

Lecture 18
Tue. 10.25.2016

Electromagnetic Lagrangian and charge-field mechanics
(Ch. 2.8 of Unit 2)

Charge mechanics in electromagnetic fields

Vector analysis for particle-in- (\mathbf{A}, Φ) -potential

Lagrangian for particle-in- (\mathbf{A}, Φ) -potential

Hamiltonian for particle-in- (\mathbf{A}, Φ) -potential

Canonical momentum in (\mathbf{A}, Φ) potential

Hamiltonian formulation

Hamilton's equations

Crossed E and B field mechanics

Classical Hall-effect and cyclotron orbit orbit equations

Vector theory vs. complex variable theory

Mechanical analog of cyclotron and FBI rule

Cycloid and epicycloid ruler&compass geometry

Cycloid geometry of flying levers

Practical poolhall application



This mechanical analog of (E_x, B_z) field mimics \mathbf{A} -field with tabletop \mathbf{v} -field

Charge mechanics in electromagnetic fields

- *Vector analysis for particle-in- (\mathbf{A}, Φ) -potential*
- Lagrangian for particle-in- (\mathbf{A}, Φ) -potential*
- Hamiltonian for particle-in- (\mathbf{A}, Φ) -potential*
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Vector analysis for particle-in-(\mathbf{A}, Φ)-potential

So-called *pondermotive* form for Newton's $F=ma$ equation for a mass m of charge e .

electronic charge:
 $e = -1.602176 \cdot 10^{-19}$ Coulombs

$$m \frac{d\mathbf{v}}{dt} = \mathbf{F} = e(\mathbf{E} + \mathbf{v} \times \mathbf{B})$$

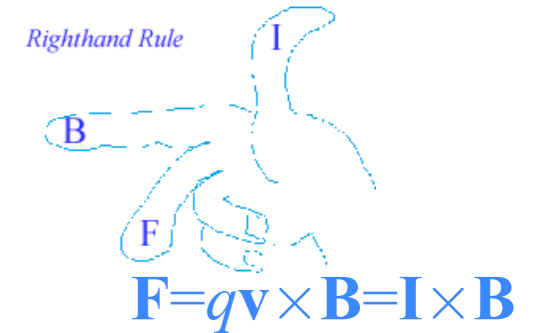
Electric field \mathbf{E} and magnetic field \mathbf{B}

scalar potential field $\Phi = \Phi(\mathbf{r}, t)$

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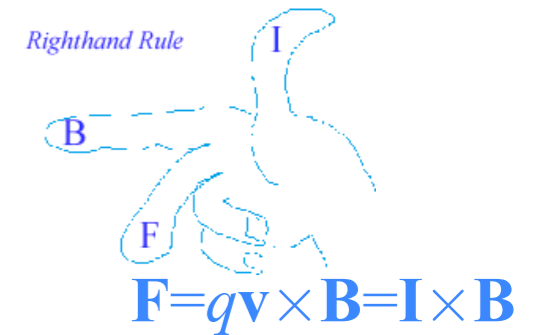
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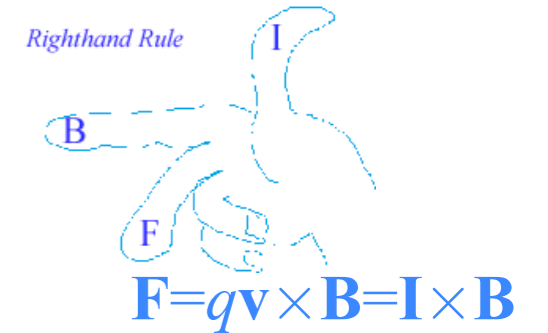
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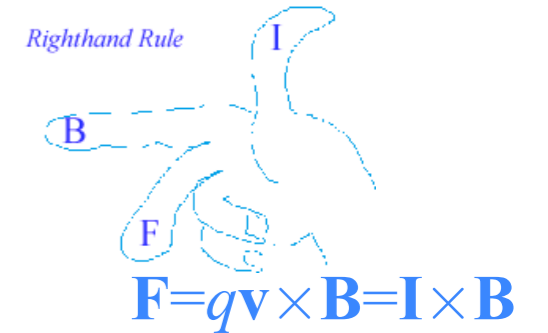
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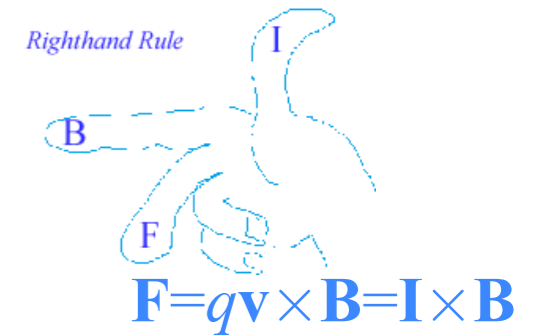
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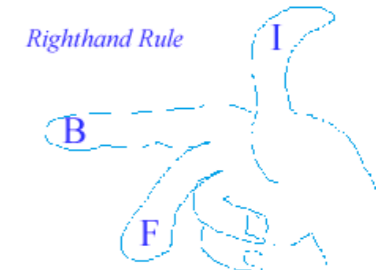
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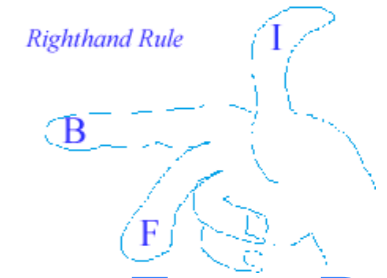
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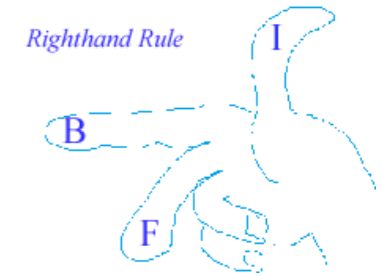
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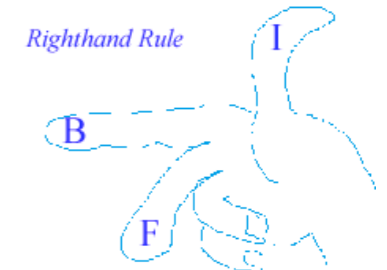
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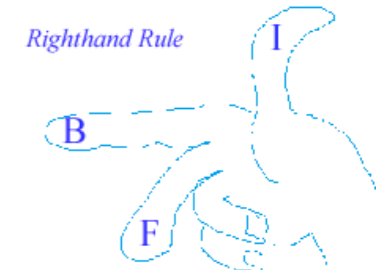
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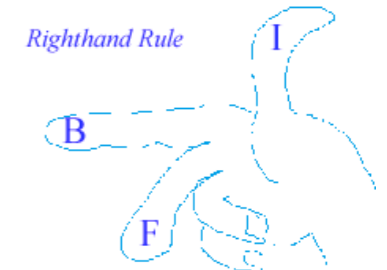
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Newtonian mechanics has *no explicit dependence* of position \mathbf{r} and velocity \mathbf{v} .

\mathbf{r} -partial derivative of \mathbf{v} (or vice-versa) is **identically zero**.

$$\partial_k v^j \equiv 0 \text{ iff : } \nabla \mathbf{v} = \frac{\partial \mathbf{v}}{\partial \mathbf{r}} = \mathbf{0}$$

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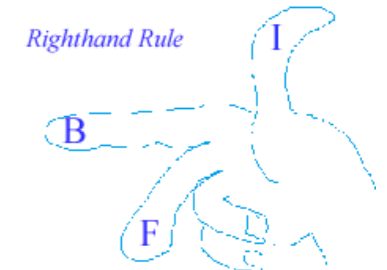
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$$\mathbf{F} = q\mathbf{v} \times \mathbf{B} = \mathbf{I} \times \mathbf{B}$$

Doing a double-cross

ϵ_{ijk} -Tensor analysis of $\mathbf{v} \times (\nabla \times \mathbf{A})$

$$[\mathbf{v} \times (\nabla \times \mathbf{A})]_k = \epsilon_{kij} v_i (\nabla \times \mathbf{A})_j$$

$$\epsilon_{ijk} = \begin{cases} +1 & \text{for even permutation of } i < j < k \\ 0 & \text{if any of } i, j, k \text{ are equal} \\ -1 & \text{for odd permutation of } i < j < k \end{cases}$$

$$= \epsilon_{kij} v_i (\epsilon_{abj} (\partial_a A_b))$$

$$= \epsilon_{kij} \epsilon_{abj} v_i (\partial_a A_b)$$

$$= (\delta_{ka} \delta_{ib} - \delta_{kb} \delta_{ia}) v_i (\partial_a A_b)$$

$$= \delta_{ka} \delta_{ib} v_i (\partial_a A_b) - \delta_{kb} \delta_{ia} v_i (\partial_a A_b)$$

$$= v_b (\partial_k A_b) - v_a (\partial_a A_k)$$

$$= (\partial_k A_b) v_b - v_a (\partial_a A_k) = (\nabla \mathbf{A}) \cdot \mathbf{v} - \mathbf{v} \cdot \nabla \mathbf{A}$$

$$= \partial_k (A_b v_b) - (\partial_k v_b) A_b - v_a (\partial_a A_k) = \nabla(\mathbf{A} \cdot \mathbf{v}) - (\nabla \mathbf{v}) \cdot \mathbf{A} - \mathbf{v} \cdot \nabla \mathbf{A}$$

Applying Levi-Civita ϵ -identity:

$$\epsilon_{kij} \epsilon_{abj} = \delta_{ka} \delta_{ib} - \delta_{kb} \delta_{ia}$$

$$\epsilon_{ijk} = \epsilon_{ikj} = \epsilon_{kij} = 1$$

$$= -\epsilon_{jik} = -\epsilon_{jki} = -\epsilon_{kji}$$

Converting back to Gibbs's **bold** notation involves *tensors* like $\nabla \mathbf{A}$ and $\nabla \mathbf{v}$.

Newtonian mechanics has *no explicit dependence* of position \mathbf{r} and velocity \mathbf{v} .

\mathbf{r} -partial derivative of \mathbf{v} (or vice-versa) is **identically zero**.

$$\partial_k v^j \equiv 0 \text{ iff : } \nabla \mathbf{v} = \frac{\partial \mathbf{v}}{\partial \mathbf{r}} = \mathbf{0}$$

$$\mathbf{v} \times (\nabla \times \mathbf{A}) = \nabla(\mathbf{A} \cdot \mathbf{v}) - \mathbf{0} - \mathbf{v} \cdot \nabla \mathbf{A} \quad \text{for particle mechanics}$$

Summary of Vector analysis for particle-in- (A, Φ) -potential

Tensor index notation helps to distinguish $(\nabla \mathbf{A}) \cdot \mathbf{v}$, $\mathbf{v} \cdot (\nabla \mathbf{A})$, and $\nabla(\mathbf{A} \cdot \mathbf{v}) = (\nabla \mathbf{A}) \cdot \mathbf{v} + (\nabla \mathbf{v}) \cdot \mathbf{A}$.

$$\begin{aligned} [(\nabla \mathbf{A}) \cdot \mathbf{v}]_k &= \frac{\partial A_j}{\partial x_k} v_j \\ &= (\partial_k A_j) v_j \end{aligned}$$

$$\begin{aligned} [\mathbf{v} \cdot (\nabla \mathbf{A})]_k &= v_j \frac{\partial A_k}{\partial x_j} \\ &= (v_j \partial_j A_k) \end{aligned}$$

$$\begin{aligned} [\nabla(\mathbf{A} \cdot \mathbf{v})]_k &= [(\nabla \mathbf{A}) \cdot \mathbf{v} + (\nabla \mathbf{v}) \cdot \mathbf{A}]_k \\ \partial_k (A_b v_b) &= (\partial_k v_b) A_b - (\partial_k v_a) A_a \end{aligned}$$

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Charge mechanics in electromagnetic fields

Vector analysis for particle-in- (\mathbf{A}, Φ) -potential

 *Lagrangian for particle-in- (\mathbf{A}, Φ) -potential*

Hamiltonian for particle-in- (\mathbf{A}, Φ) -potential

Canonical momentum in (\mathbf{A}, Φ) potential

Hamiltonian formulation

Hamilton's equations

Lagrangian for particle-in-(A, Φ)-potential

So-called *pondermotive* form for Newton's $F=ma$ equation for a mass m of charge e .

electronic charge:
 $e = -1.602176 \cdot 10^{-19}$ Coulombs

$$m \frac{d\mathbf{v}}{dt} = \mathbf{F} = e(\mathbf{E} + \mathbf{v} \times \mathbf{B})$$

Electric field \mathbf{E} and magnetic field \mathbf{B}

scalar potential field $\Phi = \Phi(\mathbf{r}, t)$

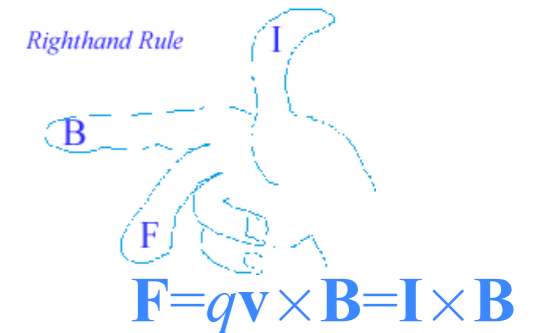
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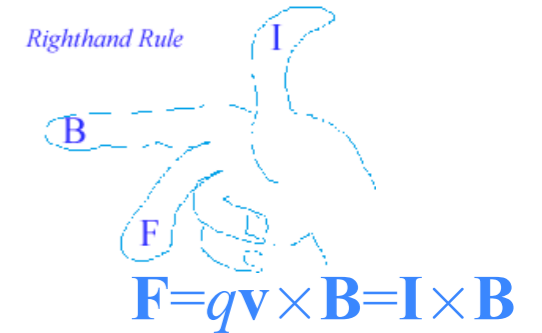
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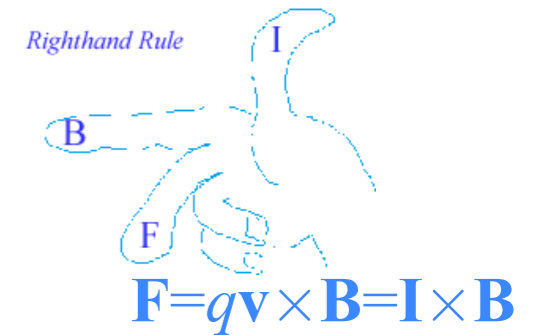
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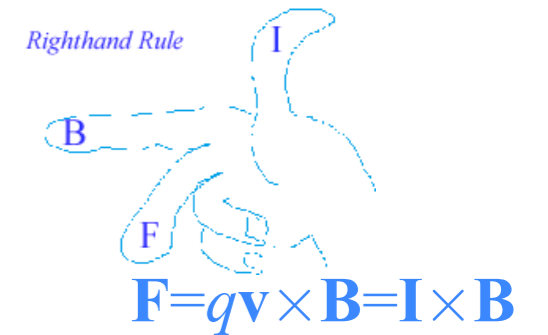
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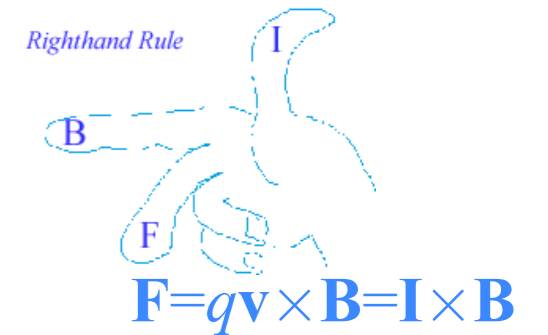
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$$-\nabla(e\Phi - \mathbf{v} \cdot e\mathbf{A})$$

$$-e \frac{d\mathbf{A}}{dt}$$

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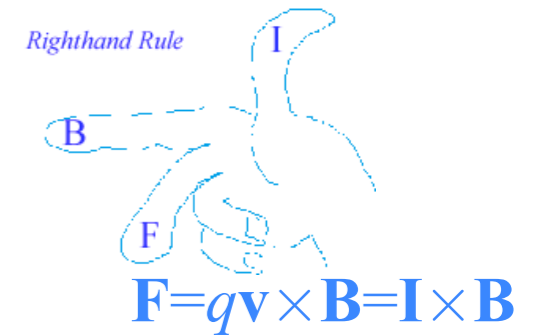
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Inserting Φ -term that $\partial_{\mathbf{v}}$ zeros :

(This step requires that : $\frac{\partial}{\partial \mathbf{v}}(e\Phi) = 0$) (and : $\frac{\partial}{\partial \mathbf{v}}(\mathbf{v} \cdot e\mathbf{A}) = e\mathbf{A}$)

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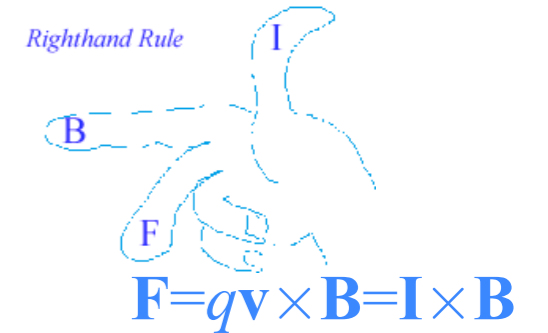
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This step requires that :

$$\nabla \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right) \equiv \frac{\partial}{\partial \mathbf{r}} \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right) = 0$$

Inserting $\mathbf{v} \cdot \mathbf{v}$ -term that $\partial_{\mathbf{r}}$ zeros :

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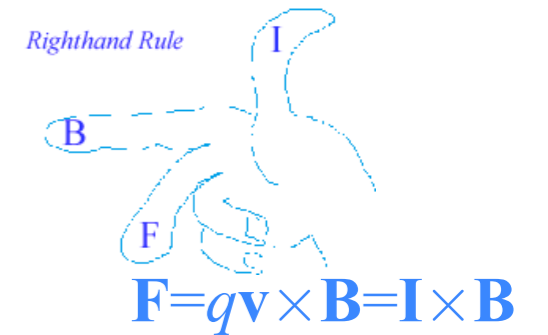
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$$\frac{\partial}{\partial \mathbf{r}} \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right) = 0$$

$$\frac{d}{dt} \frac{\partial L}{\partial \mathbf{v}} = \frac{\partial L}{\partial \mathbf{r}}$$

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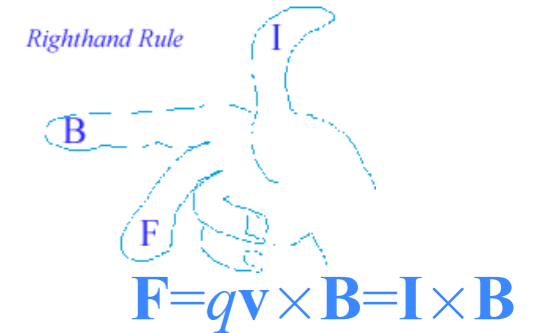
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$$m \frac{d\mathbf{v}}{dt} = e \left[-\nabla\Phi + \nabla(\mathbf{v} \cdot \mathbf{A}) - \frac{\partial\mathbf{A}}{\partial t} - (\mathbf{v} \cdot \nabla)\mathbf{A} \right] = e \left[-\nabla(\Phi - \mathbf{v} \cdot \mathbf{A}) - \frac{d\mathbf{A}}{dt} \right]$$

$$m \frac{d\mathbf{v}}{dt} = \frac{d}{dt} \frac{\partial}{\partial \mathbf{v}} \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right)$$

$$\frac{d}{dt} \frac{\partial}{\partial \mathbf{v}} \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right) = \frac{d}{dt} \frac{\partial}{\partial \mathbf{v}} (e\Phi - \mathbf{v} \cdot e\mathbf{A}) - \nabla(e\Phi - \mathbf{v} \cdot e\mathbf{A})$$

$$\frac{d}{dt} \frac{\partial}{\partial \mathbf{v}} (e\Phi - \mathbf{v} \cdot e\mathbf{A}) = -e \frac{d\mathbf{A}}{dt}$$

$$\frac{d}{dt} \frac{\partial}{\partial \mathbf{v}} \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} - (e\Phi - \mathbf{v} \cdot e\mathbf{A}) \right) = \frac{\partial}{\partial \mathbf{r}} \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} - (e\Phi - \mathbf{v} \cdot e\mathbf{A}) \right) \quad \frac{\partial}{\partial \mathbf{r}} \left(\frac{1}{2} m \mathbf{v} \cdot \mathbf{v} \right) = 0$$

$$\frac{d}{dt} \frac{\partial L}{\partial \mathbf{v}} = \frac{\partial L}{\partial \mathbf{r}}$$

Lagrangian has a *linear* velocity term $e\mathbf{v} \cdot \mathbf{A}$ in addition to the usual quadratic $KE = mv^2/2$ and $PE = e\Phi$.

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Charge mechanics in electromagnetic fields

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 *Canonical momentum in (\mathbf{A}, Φ) potential*

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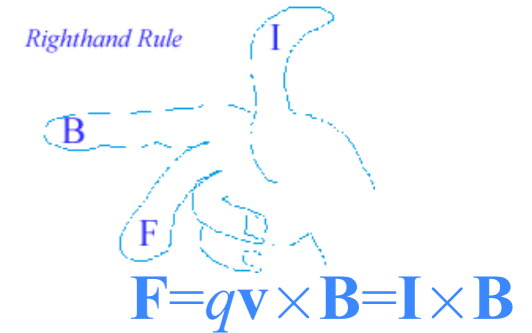
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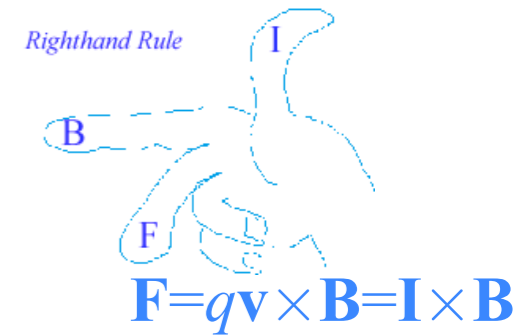
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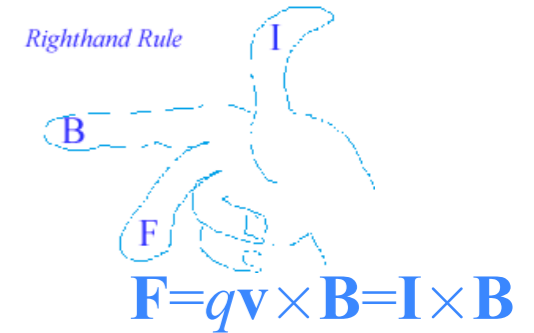


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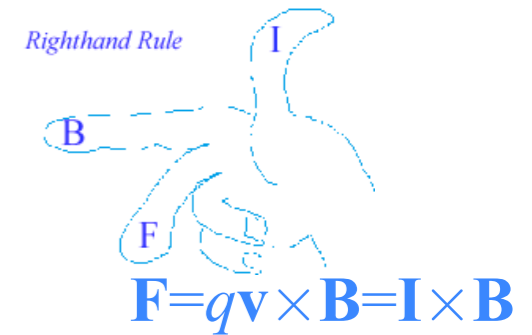
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Otherwise vector potential term $-\mathbf{v}\cdot e\mathbf{A}$ leads to an extraordinary *canonical momentum*: $\mathbf{p} = m\mathbf{v} + e\mathbf{A}(\mathbf{r}, t)$.
Particle momentum $m\mathbf{v}$ is not canonical, but related to *canonical* \mathbf{p} as follows: $m\mathbf{v} = \mathbf{p} - e\mathbf{A}(\mathbf{r}, t)$

Charge mechanics in electromagnetic fields

Vector analysis for particle-in- (\mathbf{A}, Φ) -potential

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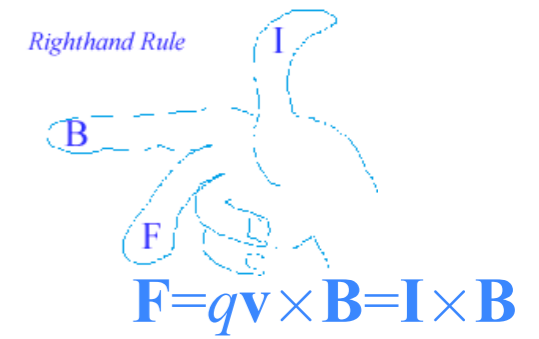
 *Hamiltonian formulation*

Hamilton's equations

Hamiltonian for charged particle in fields

The Hamiltonian function of the Legendre-Poincare form is the following.

$$H = \sum_{\mu} \dot{q}^{\mu} p_{\mu} - L = \mathbf{v} \cdot \mathbf{p} - L = \mathbf{v} \cdot (m\mathbf{v} + e\mathbf{A}(\mathbf{r}, t)) - \left(\frac{1}{2} m\mathbf{v} \cdot \mathbf{v} - (e\Phi(\mathbf{r}, t) - \mathbf{v} \cdot e\mathbf{A}(\mathbf{r}, t)) \right)$$



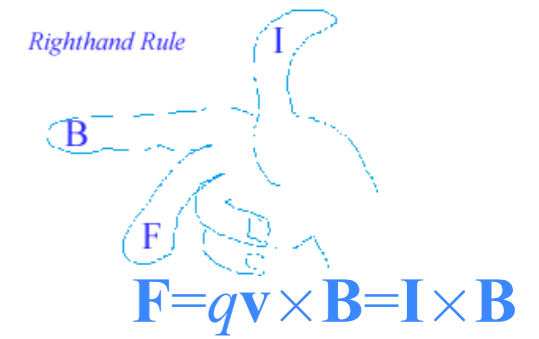
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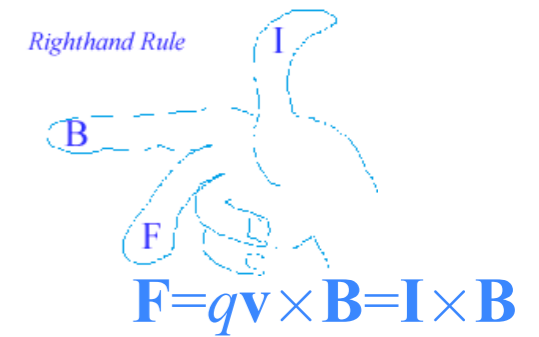
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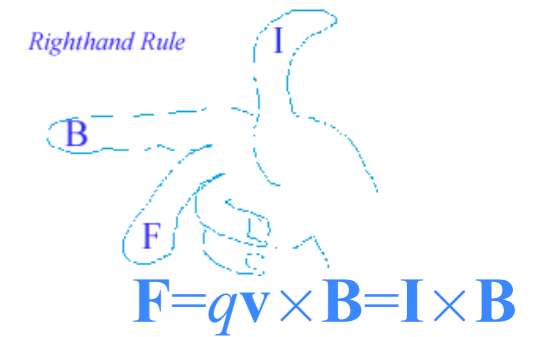
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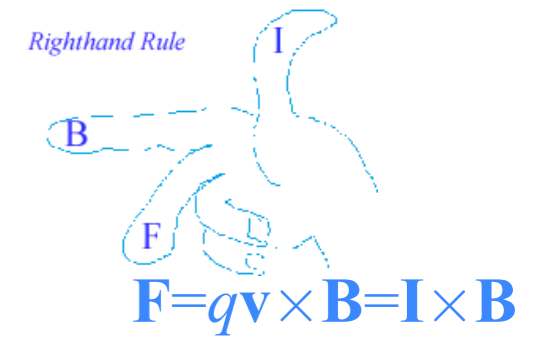
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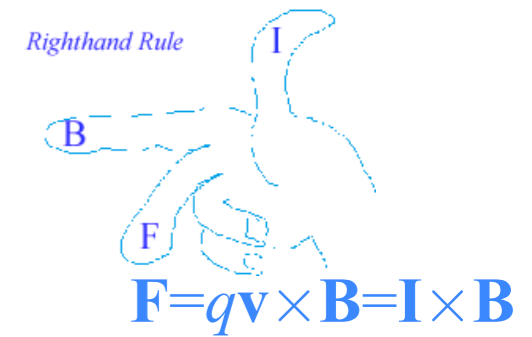
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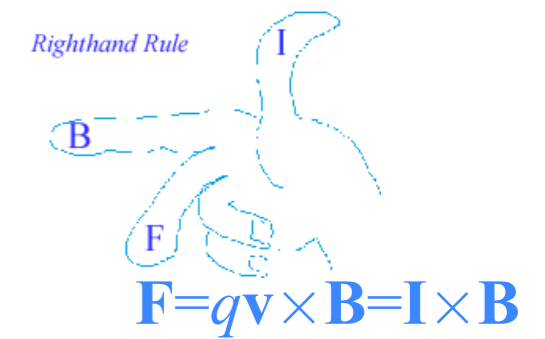


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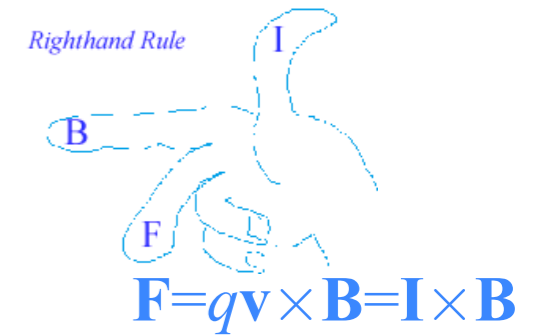
→ *Hamilton's equations*

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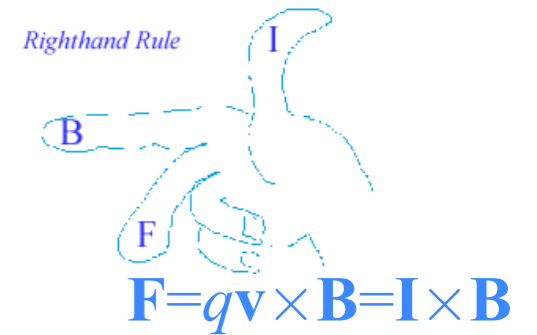
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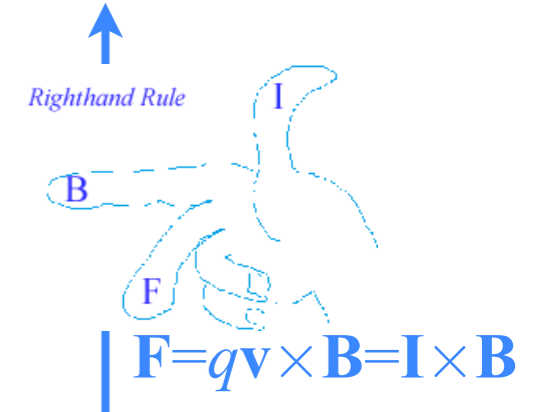
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...and now

we come back

full circle...

$$m\dot{v}_a = e \left(v_\mu \frac{\partial A_\mu}{\partial x_a} - v_\mu \frac{\partial A_a}{\partial x_\mu} + E_a \right)$$

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$$\mathbf{v} \times (\nabla \times \mathbf{A}) = \mathbf{v} \cdot (\nabla \mathbf{A}) - (\mathbf{v} \cdot \nabla)\mathbf{A} \quad \text{for particle mechanics}$$

Crossed E and B field mechanics

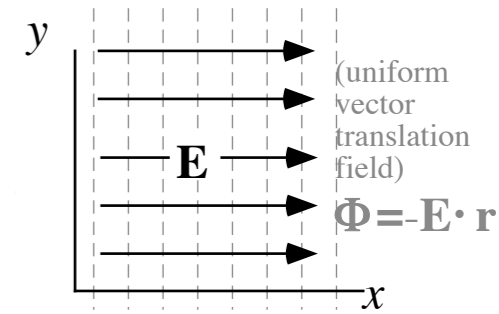
- *Classical Hall-effect and cyclotron orbit orbit equations*
- Vector theory vs. complex variable theory*
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A constant \mathbf{E} field has a scalar potential field Φ with constant gradient.

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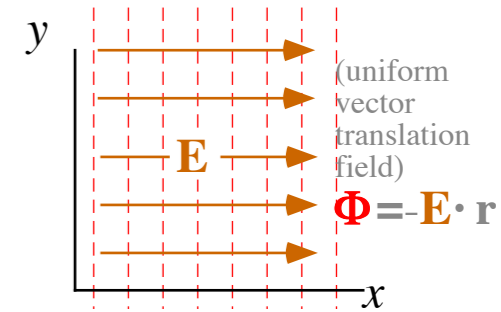
Fig. 2.4.1.



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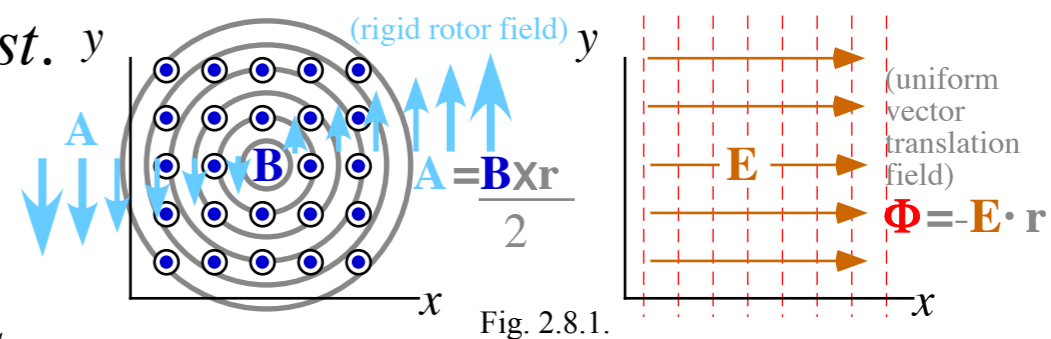
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This mechanical analog of (E_x, B_z) field mimics \mathbf{A} -field with tabletop \mathbf{v} -field



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Newtonian electromagnetic equations of motion: $m\dot{\mathbf{v}} = e(\mathbf{E} + \mathbf{v} \times \mathbf{B})$

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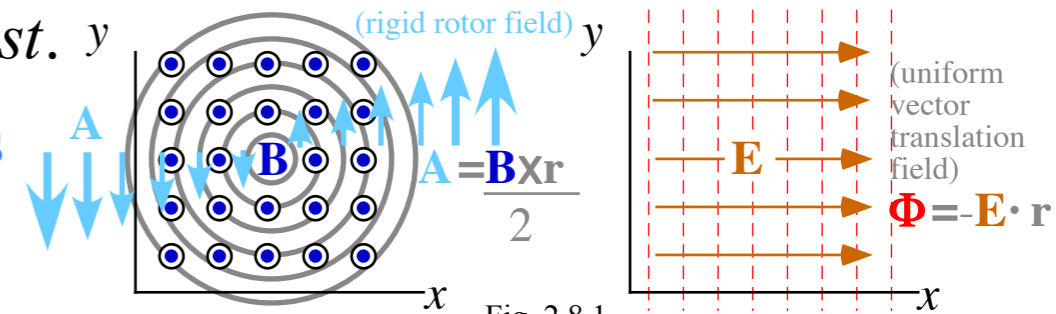
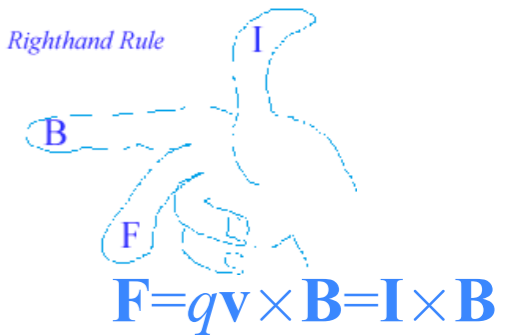


Fig. 2.8.1.

Righthand Rule



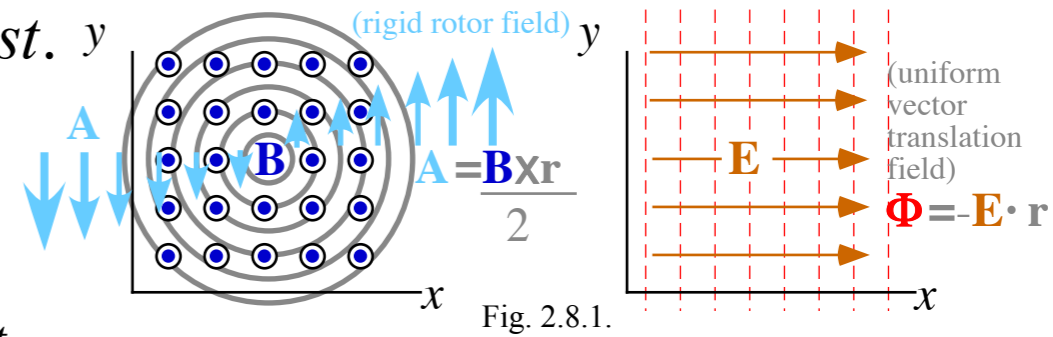
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Shorthand Labeling

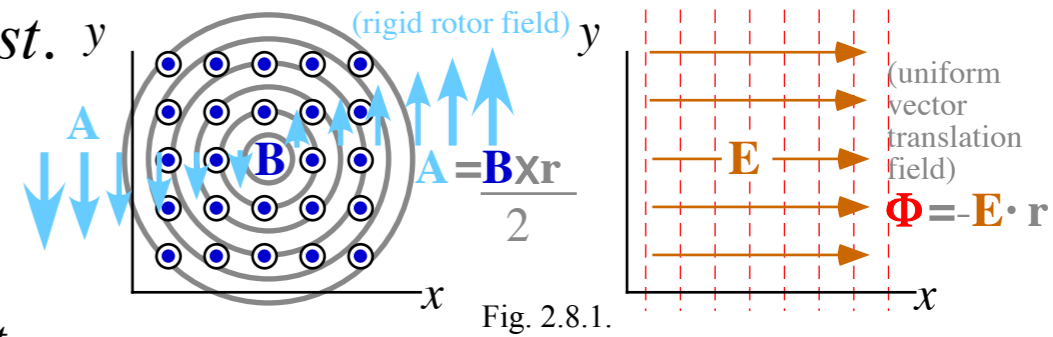
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Shorthand Labeling

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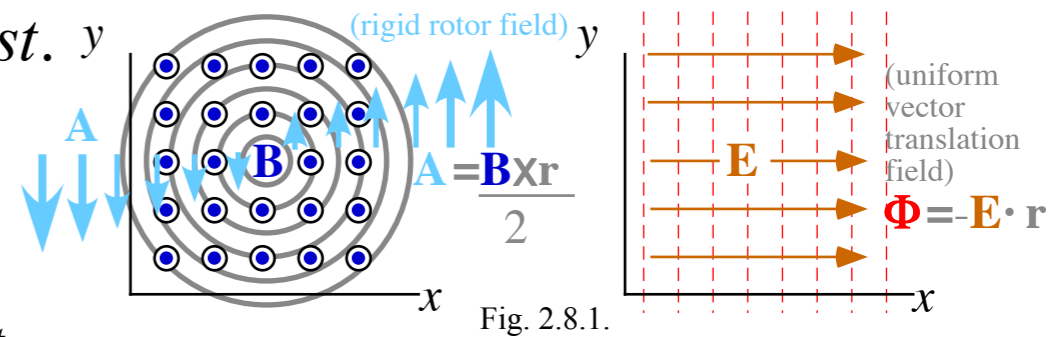


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Complex variable velocity: $v = v_x + iv_y$ and electric field: $\varepsilon = \varepsilon_x + i\varepsilon_y$

$$\dot{v}_x + i\dot{v}_y = \varepsilon_x + i\varepsilon_y - iBv_x + Bv_y = \varepsilon_x + i\varepsilon_y - iB(v_x + iv_y)$$

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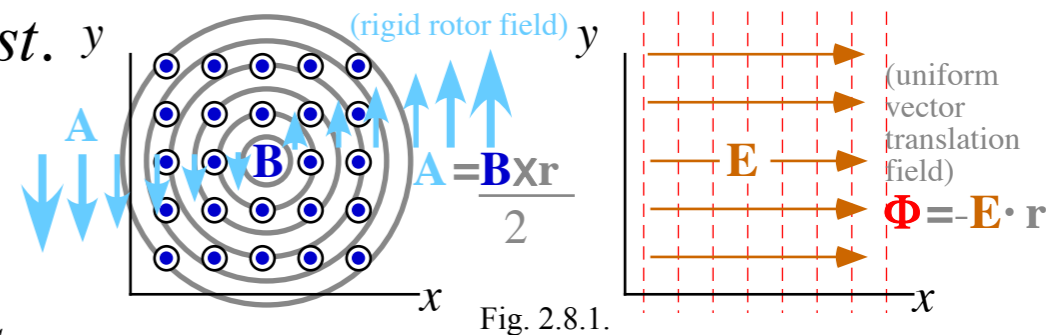
Crossed E and B field mechanics

A constant \mathbf{E} field has a scalar potential field Φ with constant gradient.

$$\Phi(\mathbf{r}) = -\mathbf{E} \cdot \mathbf{r}, \quad -\nabla\Phi(\mathbf{r}) = -\nabla(-\mathbf{E} \cdot \mathbf{r}) = \mathbf{E} = \text{const.}$$

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Newtonian electromagnetic equations of motion: $m\dot{\mathbf{v}} = e(\mathbf{E} + \mathbf{v} \times \mathbf{B})$

Gibb's notation:

$$\begin{aligned} \dot{\mathbf{v}} &= \boldsymbol{\varepsilon} + \mathbf{v} \times B\hat{\mathbf{e}}_z \\ \dot{v}_x \hat{\mathbf{e}}_x + \dot{v}_y \hat{\mathbf{e}}_y &= \varepsilon_x \hat{\mathbf{e}}_x + \varepsilon_y \hat{\mathbf{e}}_y + (v_x \hat{\mathbf{e}}_x + v_y \hat{\mathbf{e}}_y) \times B\hat{\mathbf{e}}_z \\ &= \varepsilon_x \hat{\mathbf{e}}_x + \varepsilon_y \hat{\mathbf{e}}_y - Bv_x \hat{\mathbf{e}}_y + Bv_y \hat{\mathbf{e}}_x \end{aligned}$$

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Shorthand Labeling

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Pick β so: $iB\beta = -\varepsilon$

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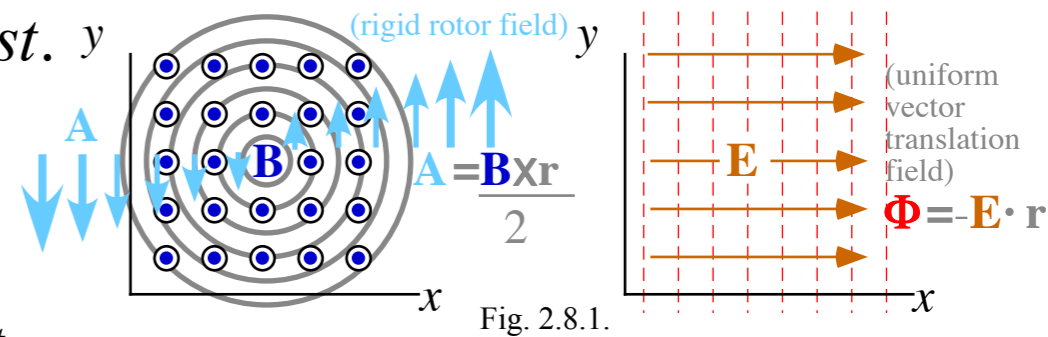
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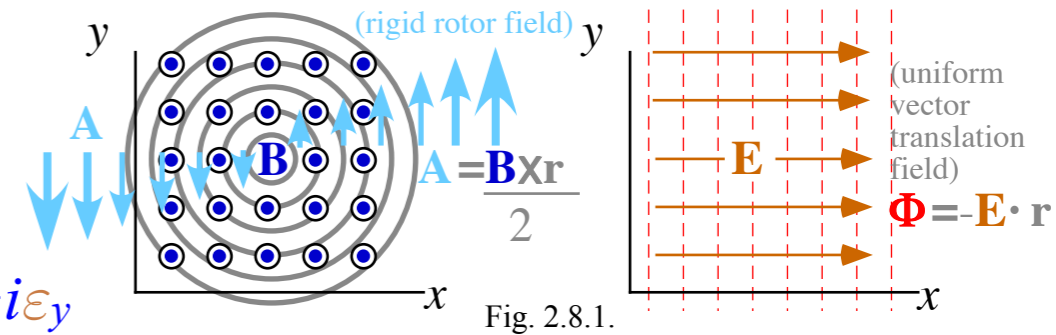
Move last part of this calculation UP↑

Crossed E and B field mechanics (Solution by complex variables)

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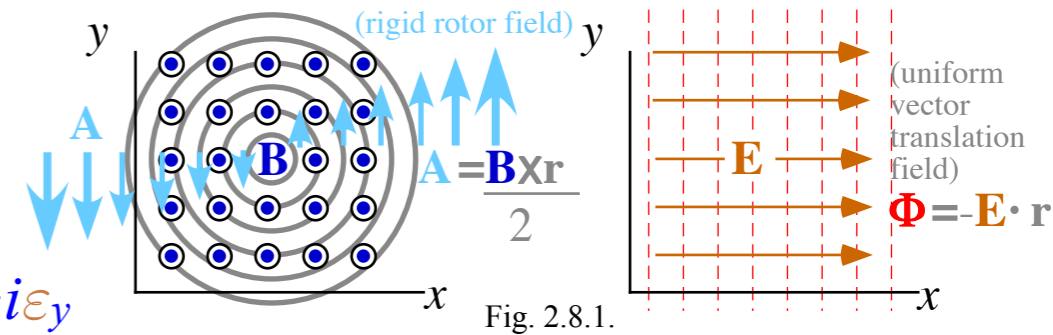
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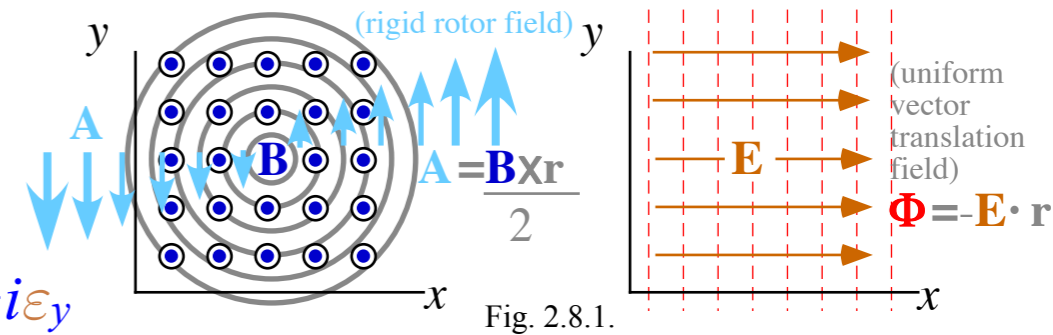
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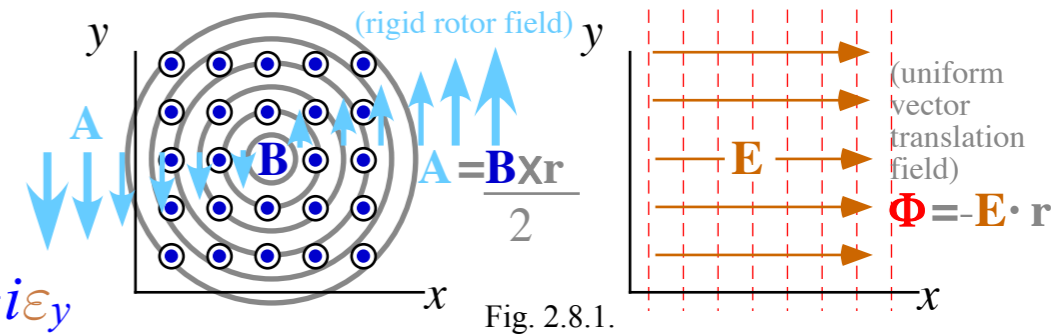
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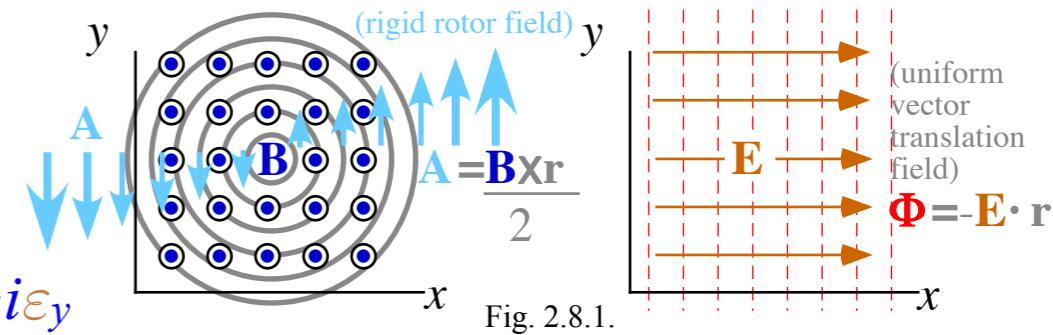
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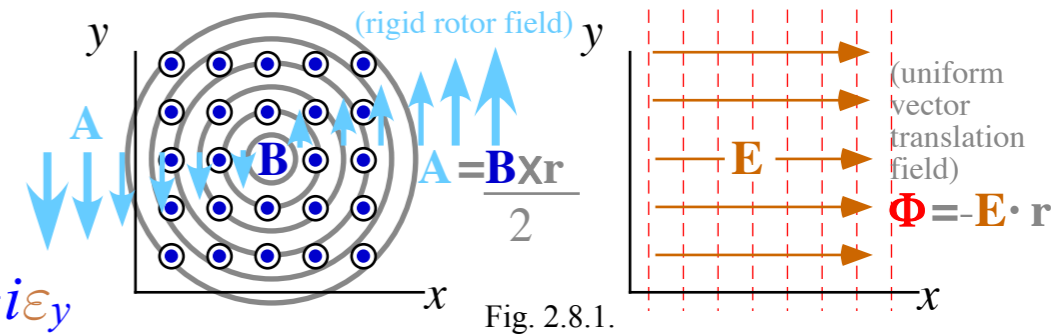
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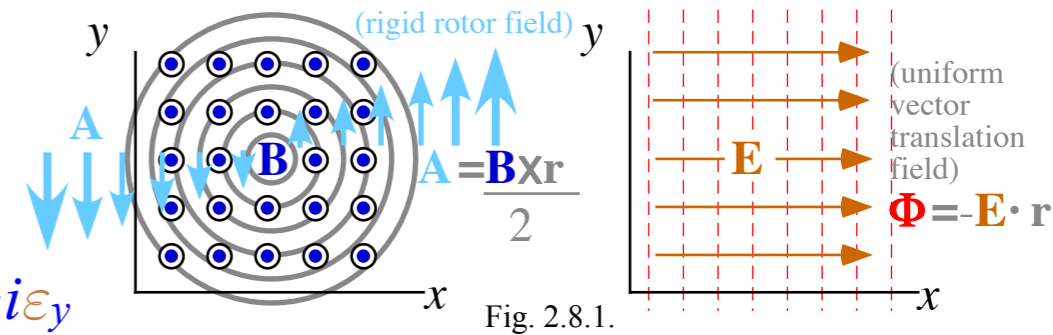
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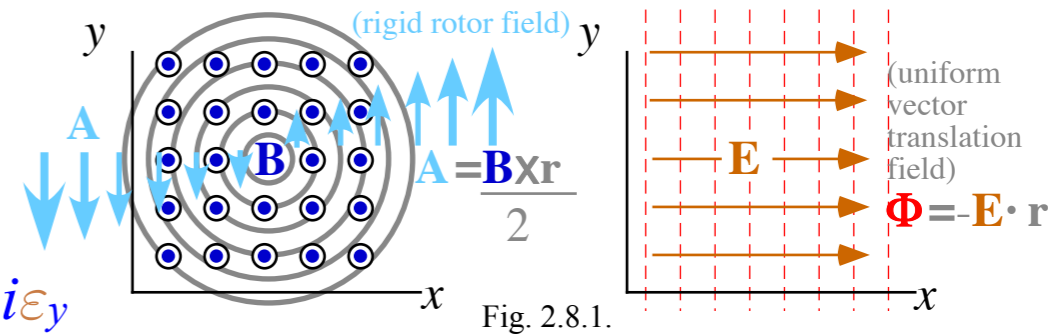
$$q(t) = \int v(t) dt = \frac{e^{-iBt}}{-iB} \left(v(0) + i\frac{\varepsilon}{B} \right) - i\frac{\varepsilon}{B} \cdot t + \text{Const.} \quad \text{where: } \text{Const.} = q(0) - \left(\frac{v(0)}{-iB} - \frac{\varepsilon}{B^2} \right) \quad \text{complex form}$$

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$$\begin{pmatrix} v_x(t) \\ v_y(t) \end{pmatrix} = \begin{pmatrix} \cos Bt & \sin Bt \\ -\sin Bt & \cos Bt \end{pmatrix} \begin{pmatrix} v_x(0) - \frac{\varepsilon_y}{B} \\ v_y(0) + \frac{\varepsilon_x}{B} \end{pmatrix} + \begin{pmatrix} \frac{\varepsilon_y}{B} \\ -\frac{\varepsilon_x}{B} \end{pmatrix}$$

vector form

Integrating $v(t)$ yields complex coordinate $q = x + iy$ affected by both ε_x and ε_y .

$$q(t) = \int v(t) dt = \frac{e^{-iBt}}{-iB} \left(v(0) + i\frac{\varepsilon}{B} \right) - i\frac{\varepsilon}{B} \cdot t + \text{Const.} \quad \text{where: } \text{Const.} = q(0) - \left(\frac{v(0)}{-iB} - \frac{\varepsilon}{B^2} \right) \quad \text{complex form}$$

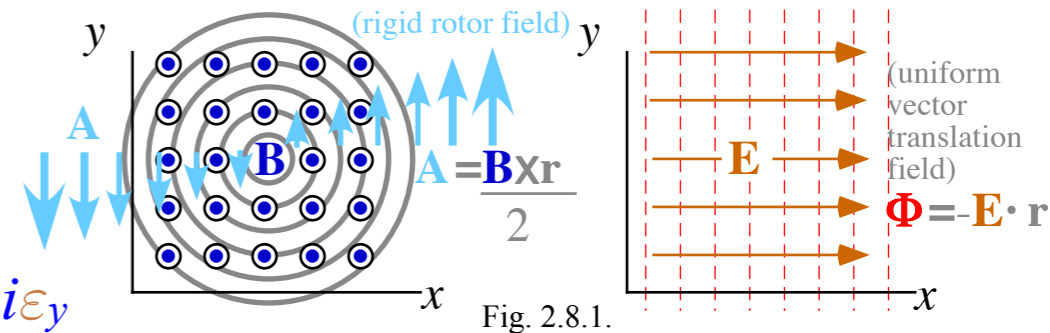
$$x(t) + iy(t) = e^{-iBt} \left(i\frac{v(0)}{B} - \frac{\varepsilon}{B^2} \right) - i\frac{\varepsilon}{B} \cdot t + x(0) + iy(0) - i\frac{v(0)}{B} + \frac{\varepsilon}{B^2}$$

Crossed E and B field mechanics (Solution by complex variables)

$$\dot{\mathbf{v}} = \frac{e}{m} \mathbf{E} + \mathbf{v} \times \frac{e}{m} \mathbf{B} = \boldsymbol{\varepsilon} + \mathbf{v} \times \frac{e}{m} B \hat{\mathbf{e}}_z$$

$$\boldsymbol{\varepsilon}_x = \frac{e}{m} E_x \quad \boldsymbol{\varepsilon}_y = \frac{e}{m} E_y \quad B = \frac{e}{m} B_z$$

Shorthand Labeling



Complex variable velocity: $v = v_x + iv_y$ and electric field: $\varepsilon = \varepsilon_x + i\varepsilon_y$

$$\dot{v}_x + i\dot{v}_y = \varepsilon_x + i\varepsilon_y - iBv_x + Bv_y = \varepsilon_x + i\varepsilon_y - iB(v_x + iv_y)$$

$$\dot{v} = \varepsilon - iBv \quad \text{with replacements : } \hat{\mathbf{e}}_x \rightarrow 1 \quad \text{and : } \hat{\mathbf{e}}_y \rightarrow i = \sqrt{-1}$$

A velocity transformation $V(t) = v(t) + \beta$ cancels constant ε -field to give an equation: $\dot{V} = (\text{const.})V$

$$\dot{V}(t) = \dot{v}(t) + \dot{\beta} = \varepsilon - iBv = \varepsilon - iB(V(t) - \beta) = -iBV(t) \quad \text{where : } \beta = -\frac{\varepsilon}{iB} = i\frac{\varepsilon}{B}$$

An exponential $V(t) = e^{-iBt}V(0)$ solution results: e^{-iBt} is a clockwise 2D rotation.

$$v(t) + \beta = V(t) = e^{-iBt}V(0) = e^{-iBt}(v(0) + \beta) \quad \text{or:} \quad v(t) = e^{-iBt}(v(0) + \beta) - \beta = e^{-iBt}(v(0) + i\frac{\varepsilon}{B}) - i\frac{\varepsilon}{B}$$

Expanding e^{-iBt} , $v = v_x + iv_y$, and $\varepsilon = \varepsilon_x + i\varepsilon_y$ reveals x (Real) and y (Imaginary) components

$$\begin{pmatrix} v_x(t) \\ v_y(t) \end{pmatrix} = \begin{pmatrix} \cos Bt & \sin Bt \\ -\sin Bt & \cos Bt \end{pmatrix} \begin{pmatrix} v_x(0) - \frac{\varepsilon_y}{B} \\ v_y(0) + \frac{\varepsilon_x}{B} \end{pmatrix} + \begin{pmatrix} \frac{\varepsilon_y}{B} \\ -\frac{\varepsilon_x}{B} \end{pmatrix}$$

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$$x(t) + iy(t) = e^{-iBt} \left(i\frac{v(0)}{B} - \frac{\varepsilon}{B^2} \right) - i\frac{\varepsilon}{B} \cdot t + x(0) + iy(0) - i\frac{v(0)}{B} + \frac{\varepsilon}{B^2}$$

Move last part of this calculation UP↑

Crossed E and B field mechanics (Solution by complex variables)

$$\dot{V}(t) = \dot{v}(t) + \dot{\beta} = \varepsilon - iBv = \varepsilon - iB(V(t) - \beta) = -iBV(t) \quad \text{where: } \beta = -\frac{\varepsilon}{iB} = i\frac{\varepsilon}{B}$$

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complex form
vector form

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$$\dot{V}(t) = \dot{v}(t) + \dot{\beta} = \varepsilon - iBv = \varepsilon - iB(V(t) - \beta) = -iBV(t) \quad \text{where: } \beta = -\frac{\varepsilon}{iB} = i\frac{\varepsilon}{B}$$

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$$x(t) + iy(t) = e^{-iBt} \left(i\frac{v(0)}{B} - \frac{\varepsilon}{B^2} \right) - i\frac{\varepsilon}{B} \cdot t + x(0) + iy(0) - i\frac{v(0)}{B} + \frac{\varepsilon}{B^2} \quad \text{complex form}$$

$$\begin{pmatrix} x(t) \\ y(t) \end{pmatrix} = \begin{pmatrix} \cos B \cdot t & \sin B \cdot t \\ -\sin B \cdot t & \cos B \cdot t \end{pmatrix} \begin{pmatrix} -\frac{v_y(0)}{B} - \frac{\varepsilon_x}{B^2} \\ \frac{v_x(0)}{B} - \frac{\varepsilon_y}{B^2} \end{pmatrix} + \begin{pmatrix} \frac{\varepsilon_y}{B} t \\ -\frac{\varepsilon_x}{B} t \end{pmatrix} + \begin{pmatrix} x(0) + \frac{v_y(0)}{B} + \frac{\varepsilon_x}{B^2} \\ y(0) - \frac{v_x(0)}{B} + \frac{\varepsilon_y}{B^2} \end{pmatrix} \quad \text{vector form}$$

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complex form

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vector form

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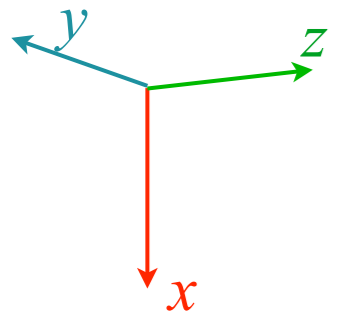
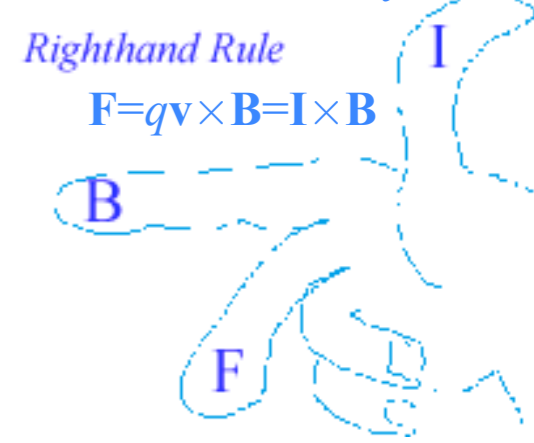
$$q(t) = \int v(t) dt = \frac{e^{-iBt}}{-iB} \left(v(0) + i\frac{\epsilon}{B} \right) - i\frac{\epsilon}{B} \cdot t + Const. \quad \text{where: } Const. = q(0) - \left(\frac{v(0)}{-iB} - \frac{\epsilon}{B^2} \right)$$

complex form

$$x(t) + iy(t) = e^{-iBt} \left(i\frac{v(0)}{B} - \frac{\epsilon}{B^2} \right) - i\frac{\epsilon}{B} \cdot t + x(0) + iy(0) - i\frac{v(0)}{B} + \frac{\epsilon}{B^2}$$

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vector form



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Integrating $v(t)$ yields complex coordinate $q = x + iy$ affected by both ϵ_x and ϵ_y .

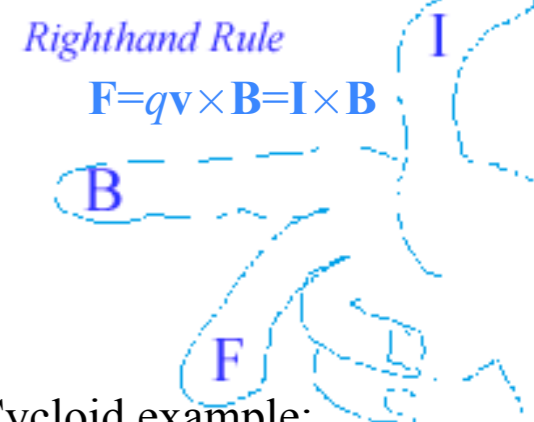
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complex form

$$x(t) + iy(t) = e^{-iBt} \left(i\frac{v(0)}{B} - \frac{\epsilon}{B^2} \right) - i\frac{\epsilon}{B} \cdot t + x(0) + iy(0) - i\frac{v(0)}{B} + \frac{\epsilon}{B^2}$$

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vector form

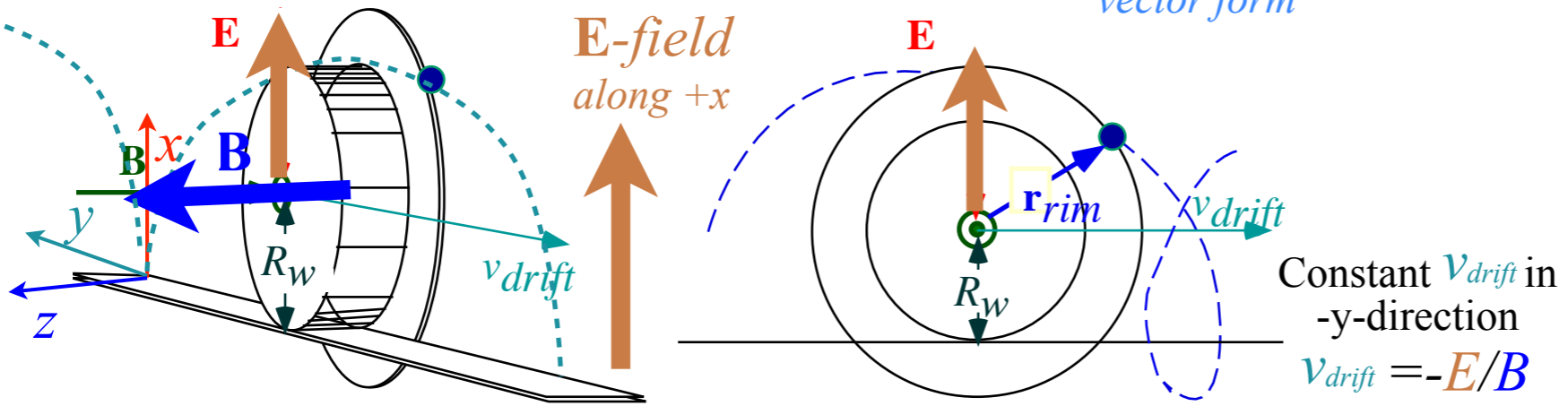


Cycloid example:
 initial $(x(0), y(0)) = (0, 0)$
 and $(v_x(0), v_y(0)) = (0, 0)$

$\begin{pmatrix} x(t) \\ y(t) \end{pmatrix}$ is on rim of a wheel of radius $R_W = E/B^2$

$$\begin{pmatrix} \cos Bt & \sin Bt \\ -\sin Bt & \cos Bt \end{pmatrix} \begin{pmatrix} -\frac{E}{B^2} \\ 0 \end{pmatrix}$$

$$+ \begin{pmatrix} 0 \\ -\frac{E}{B} t \end{pmatrix} + \begin{pmatrix} \frac{E}{B^2} \\ 0 \end{pmatrix}$$



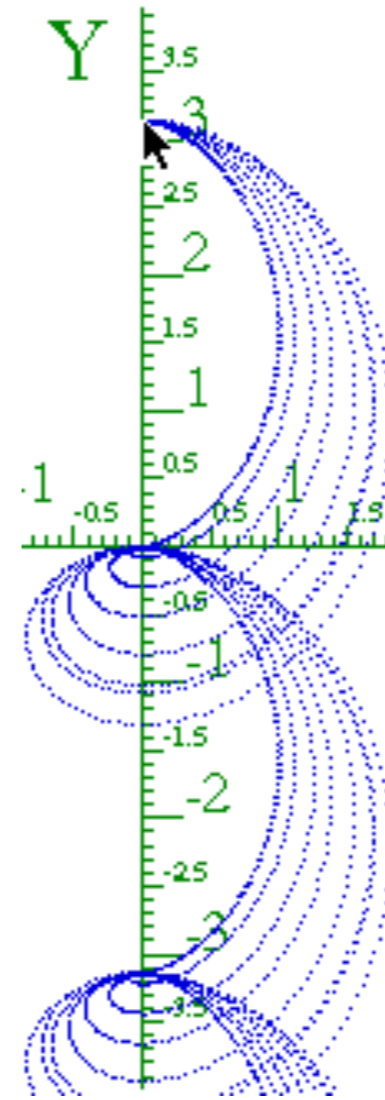
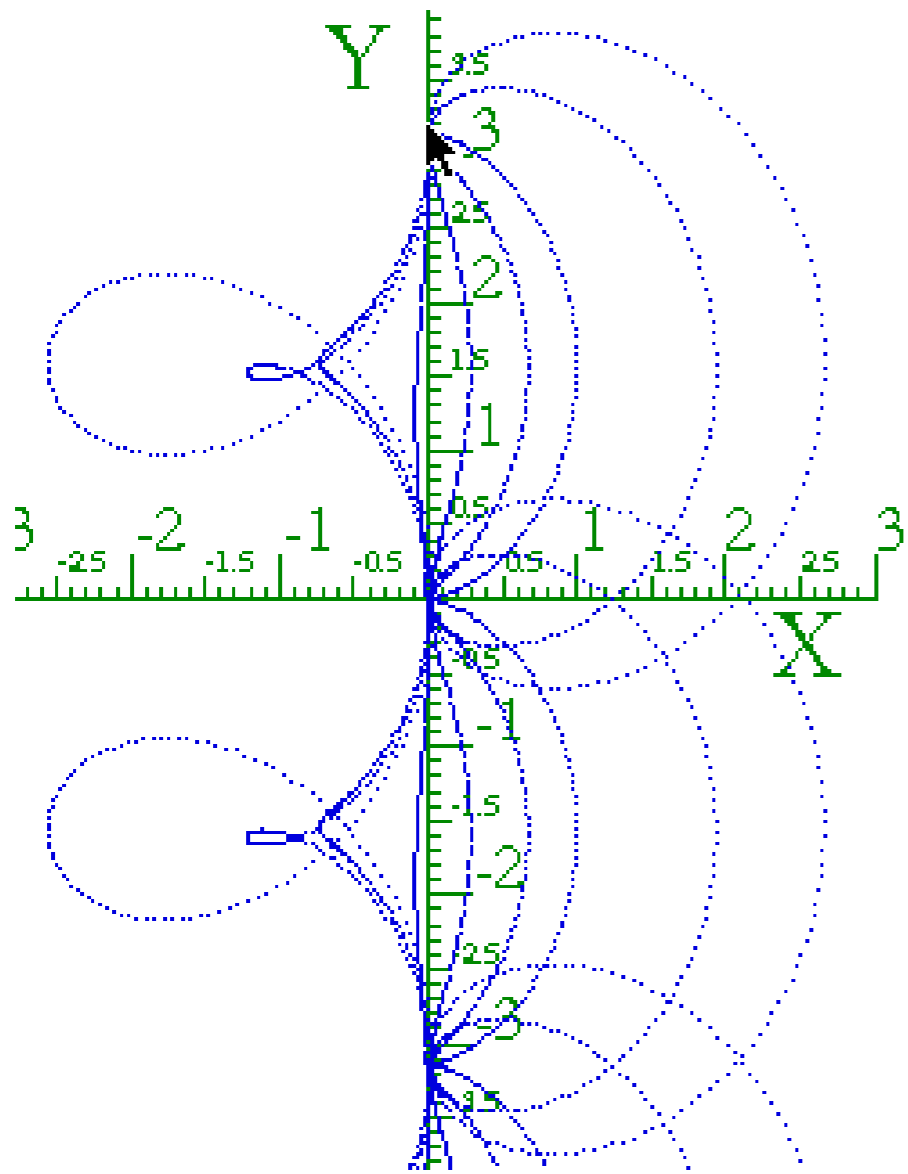
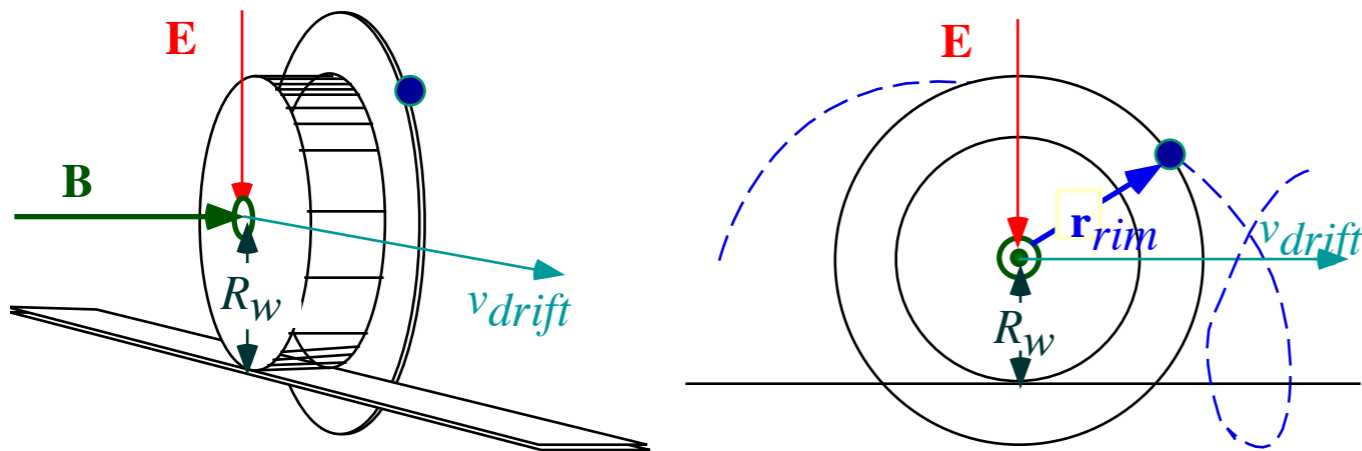
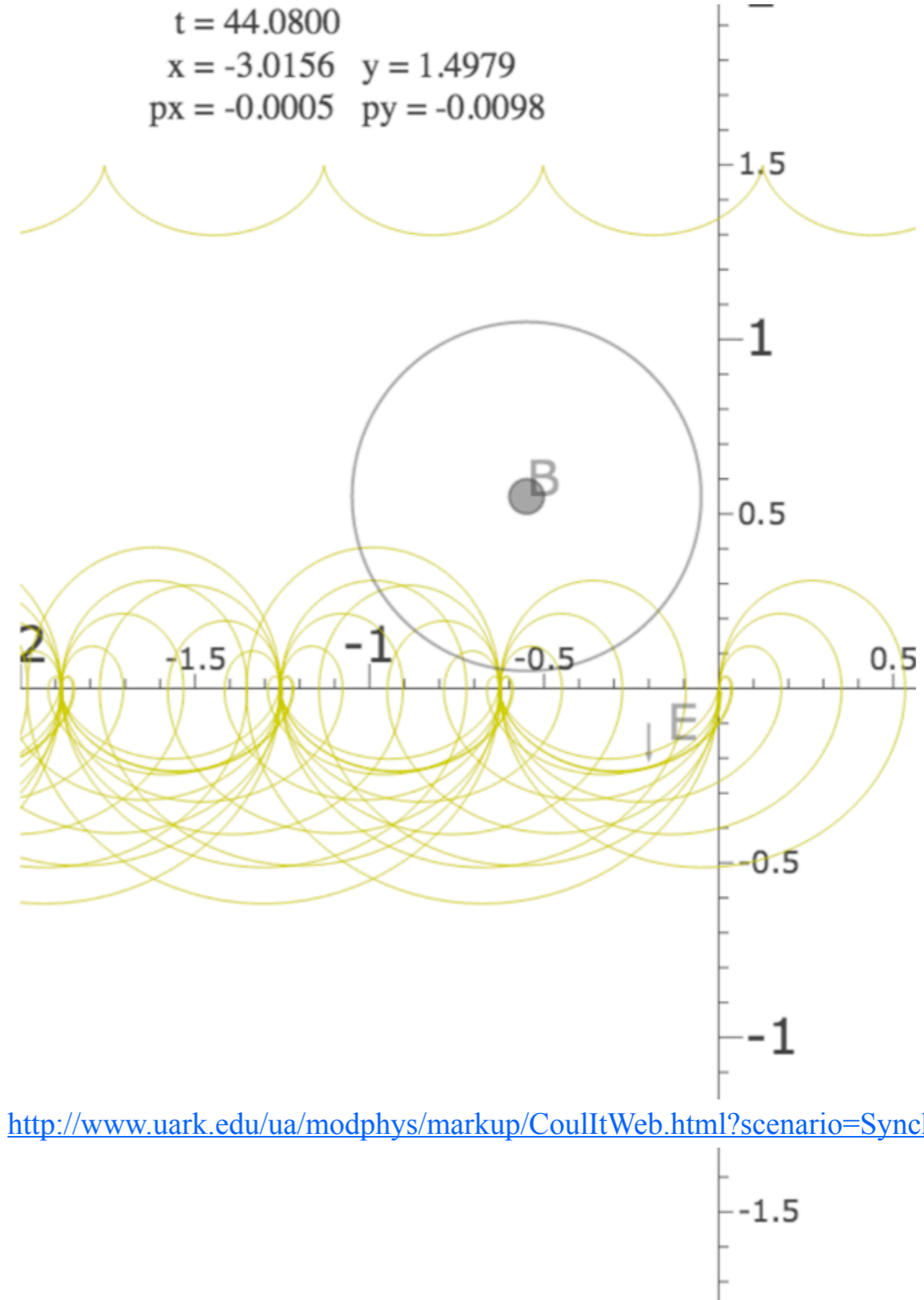


Fig. 2.8.2 Trajectories of unit charge and mass in magnetic and electric fields ($E=1/2$, $B=1$)

Fig. 2.8.3 Rolling railroad wheel and rim analogy for cyclotron orbits



- Initial position $x(0)$ =
- Initial position $y(0)$ =
- Initial momentum $p_x(0)$ =
- Initial momentum $p_y(0)$ =
- Terminal time $t(\text{off})$ =
- Maximum step size dt =
- Charge of Nucleus 1 =
- Charge of Nucleus 2 =
- Coulomb (k_{12}) =
- Core thickness r =
- x-Stark field E_x =
- y-Stark field E_y =
- Zeeman field B_z =
- Diamagnetic strength k =
- Plank constant \hbar =
- Color quantization hues =
- Color quantization bands =
- Fractional Error (e^{-x}), x =
- Particle Size =
- Fix $r(0)$ Fix $p(0)$ Do swarm Beam
- Plot $r(t)$ Plot $p(t)$
- Color action No stops Field vectors Info
- Draw masses Axes Coordinates Lenz
- Set p by ϕ Elastic 2 Free
- Save to GIF



<http://www.uark.edu/ua/modphys/markup/CoulItWeb.html?scenario=SynchrotronMotion>

Initial position $x(0) = -0.0021$

Initial position $y(0) = -0.0064$

Initial momentum $p_x(0) = -0.5016$

Initial momentum $p_y(0) = 0$

Terminal time $t(\text{off}) = 6.28318$

Maximum step size $dt = 0.08$

Charge of Nucleus 1 = 0

Charge of Nucleus 2 = 0

Coulomb (k_{12}) = 0

Core thickness $r = 0.00000$

x-Stark field $E_x = 0$

y-Stark field $E_y = -0.1$

Zeeman field $B_z = 1$

Diamagnetic strength $k = 0$

Plank constant $\hbar = 1.57079$

Color quantization hues = 64

Color quantization bands = 2

Fractional Error (e^{-x}), $x = 8$

Particle Size = 8

Fix $r(0)$ Fix $p(0)$ Do swarm Beam

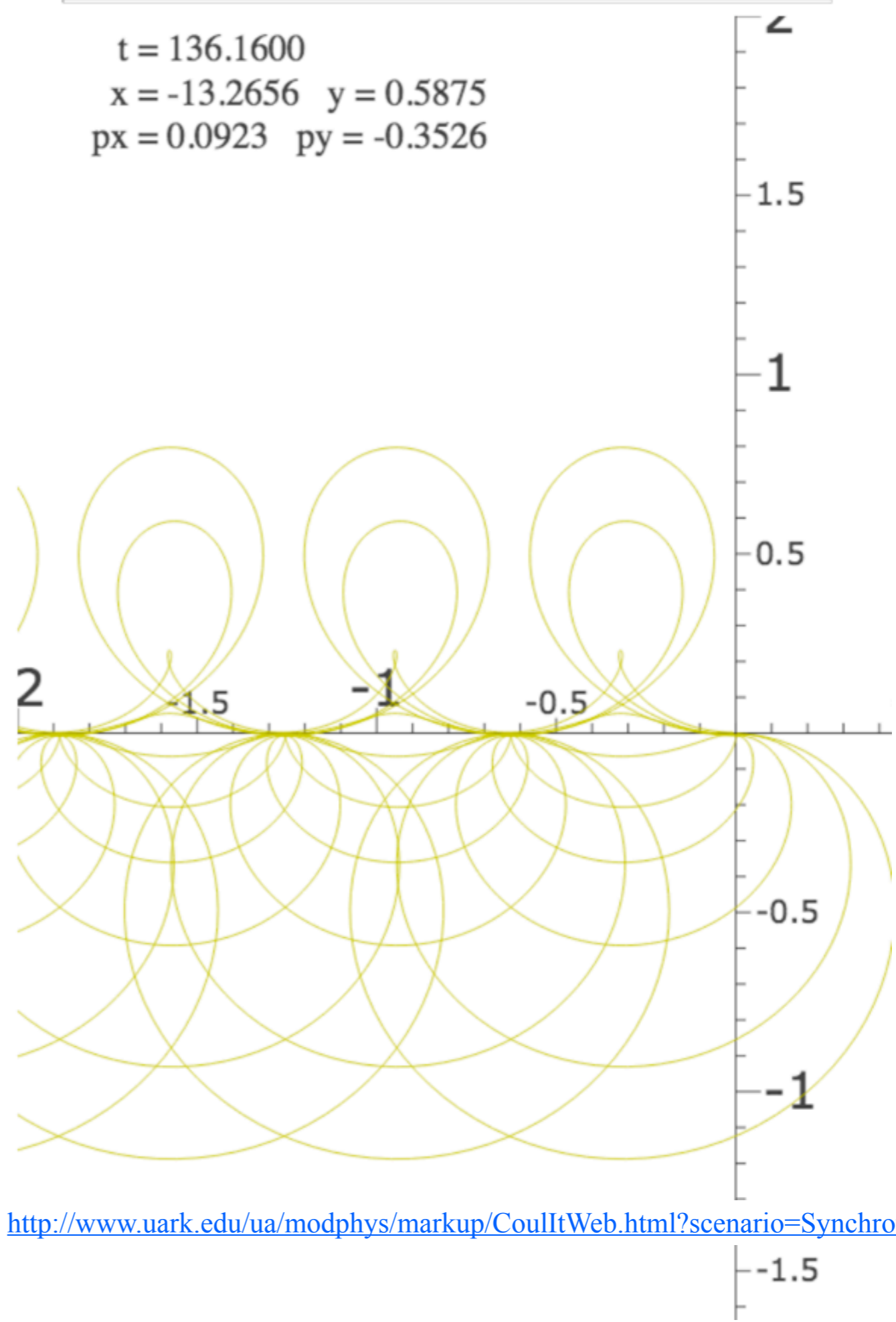
Plot $r(t)$ Plot $p(t)$

Color action No stops Field vectors Info

Draw masses Axes Coordinates Lenz

Set p by ϕ Elastic 2 Free

$t = 136.1600$
 $x = -13.2656$ $y = 0.5875$
 $p_x = 0.0923$ $p_y = -0.3526$



<http://www.uark.edu/ua/modphys/markup/CoulItWeb.html?scenario=SynchrotronMotion2>

Crossed E and B field mechanics

Classical Hall-effect and cyclotron orbit orbit equations

Vector theory vs. complex variable theory

 *Mechanical analog of cyclotron and FBI rule*

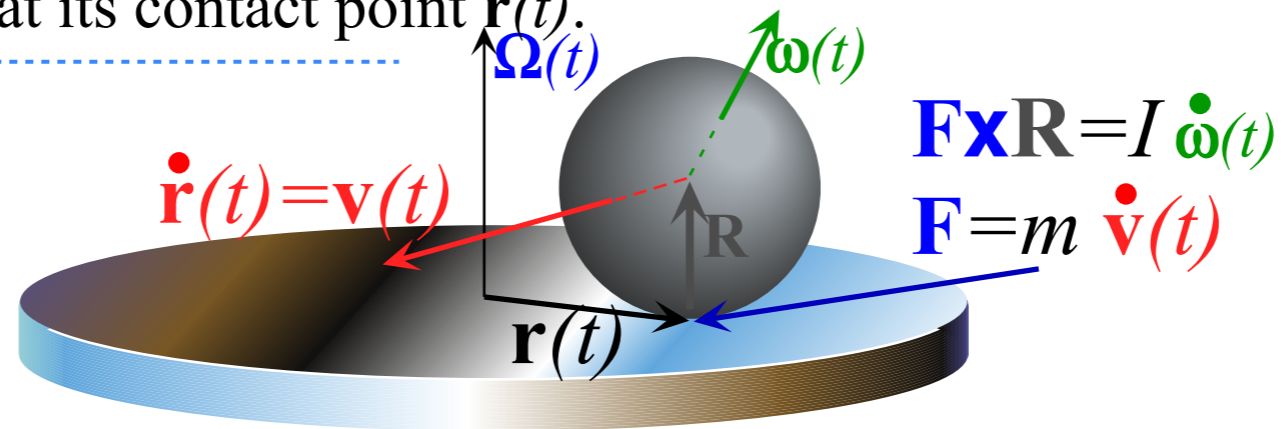
Cycloid and epicycloid ruler&compass geometry

Cycloid geometry of flying levers

Practical poolhall application

Mechanical analog of cyclotron and FBI rule

Velocity vector of the ball contact point ($\mathbf{v}(t) - \boldsymbol{\omega}(t) \times \mathbf{R}$) equals
table surface velocity $\boldsymbol{\Omega} \times \mathbf{r}(t)$ at its contact point $\mathbf{r}(t)$.



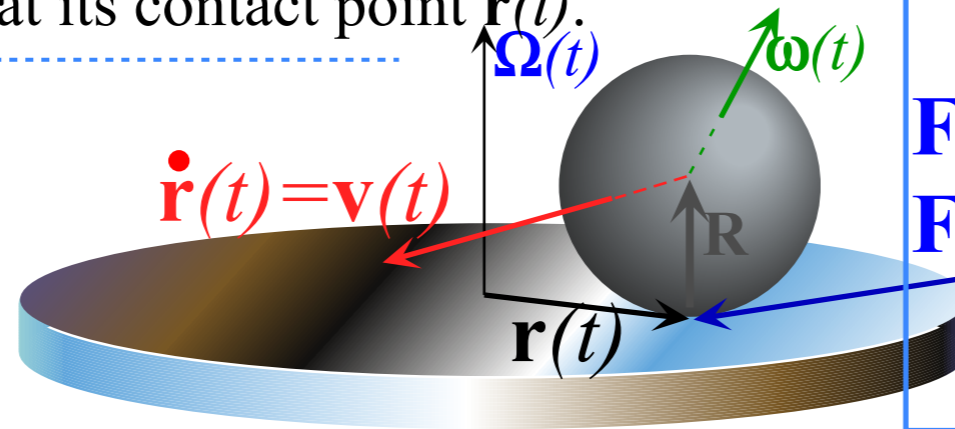
Turntable turning at constant angular velocity $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}$.



[YouTube Video of Analog to Synchrotron Motion](#)

Mechanical analog of cyclotron and FBI rule

Velocity vector of the ball contact point $(\mathbf{v}(t) - \boldsymbol{\omega}(t) \times \mathbf{R})$ equals table surface velocity $\boldsymbol{\Omega} \times \mathbf{r}(t)$ at its contact point $\mathbf{r}(t)$.



Equations of Motion:

rotation *Torque* = $\mathbf{F} \times \mathbf{R} = I \dot{\boldsymbol{\omega}}$

$$\mathbf{F} \times \mathbf{R} = I \dot{\boldsymbol{\omega}}(t)$$

$$\mathbf{F} = m \dot{\mathbf{v}}(t)$$

translation *Force* = $\mathbf{F} = m \dot{\mathbf{v}}$

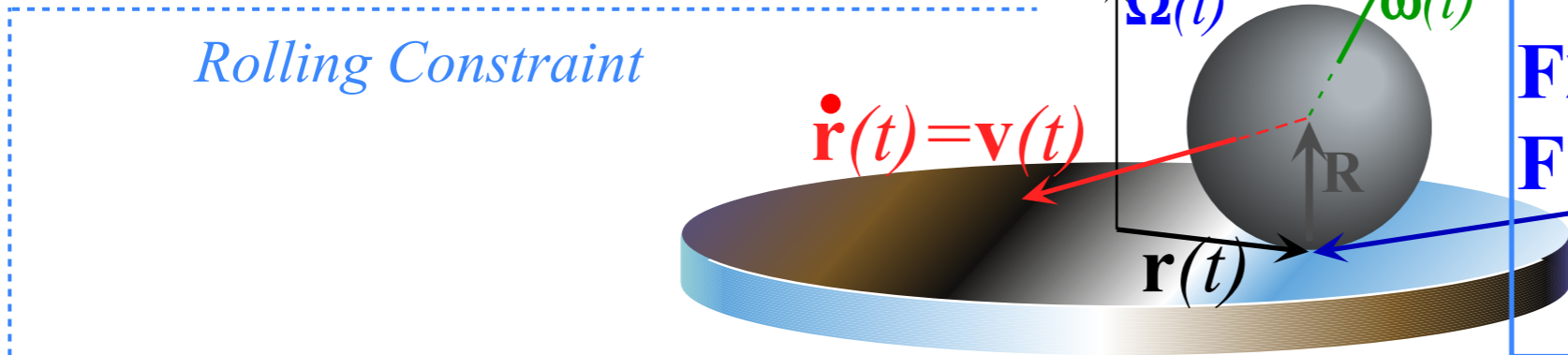
Turntable turning at constant angular velocity $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}$.

*Torque-and-F=ma
equations of motion:*

$$\begin{aligned} I \dot{\boldsymbol{\omega}}(t) &= \mathbf{F}(t) \times \mathbf{R} \\ &= m \dot{\mathbf{v}}(t) \times \mathbf{R} \\ &= m \dot{\mathbf{v}}(t) \times \hat{\mathbf{z}} R \end{aligned}$$

Mechanical analog of cyclotron and FBI rule

Velocity vector of the ball contact point $(\mathbf{v}(t) - \boldsymbol{\omega}(t) \times \mathbf{R})$ equals table surface velocity $\boldsymbol{\Omega} \times \mathbf{r}(t)$ at its contact point $\mathbf{r}(t)$.



Rolling Constraint

Equations of Motion:

rotation *Torque* = $\mathbf{F} \times \mathbf{R} = I \dot{\boldsymbol{\omega}}$

$$\mathbf{F} \times \mathbf{R} = I \dot{\boldsymbol{\omega}}(t)$$

$$\mathbf{F} = m \dot{\mathbf{v}}(t)$$

translation *Force* = $\mathbf{F} = m \dot{\mathbf{v}}$

Turntable turning at constant angular velocity $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}$.

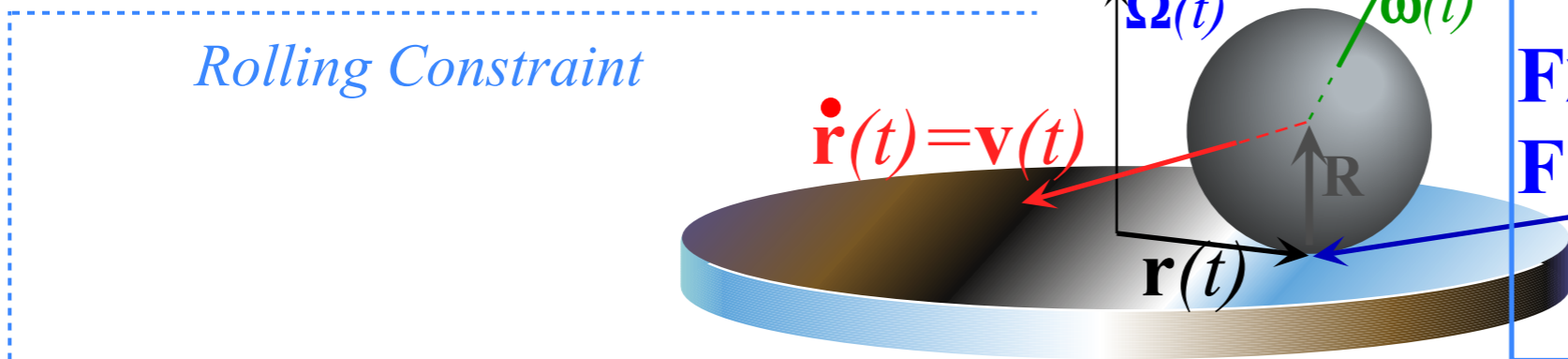
No-slipping: $\mathbf{v}(t) - \boldsymbol{\omega}(t) \times \mathbf{R} = \boldsymbol{\Omega} \times \mathbf{r}(t)$ (where: $\mathbf{R} = R \hat{\mathbf{z}}$ and $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}$ are constant.)

*Torque-and-F=ma
equations of motion:*

$$\begin{aligned} I \dot{\boldsymbol{\omega}}(t) &= \mathbf{F}(t) \times \mathbf{R} \\ &= m \dot{\mathbf{v}}(t) \times \mathbf{R} \\ &= m \dot{\mathbf{v}}(t) \times \hat{\mathbf{z}} R \end{aligned}$$

Mechanical analog of cyclotron and FBI rule

Velocity vector of the ball contact point ($\mathbf{v}(t) - \boldsymbol{\omega}(t) \times \mathbf{R}$) equals table surface velocity $\boldsymbol{\Omega} \times \mathbf{r}(t)$ at its contact point $\mathbf{r}(t)$.



Equations of Motion:

rotation *Torque* = $\mathbf{F} \times \mathbf{R} = I \dot{\boldsymbol{\omega}}$

$$\mathbf{F} \times \mathbf{R} = I \dot{\boldsymbol{\omega}}(t)$$

$$\mathbf{F} = m \dot{\mathbf{v}}(t)$$

translation *Force* = $\mathbf{F} = m \dot{\mathbf{v}}$

Turntable turning at constant angular velocity $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}$.

No-slipping: $\mathbf{v}(t) - \boldsymbol{\omega}(t) \times \mathbf{R} = \boldsymbol{\Omega} \times \mathbf{r}(t)$ (where: $\mathbf{R} = R \hat{\mathbf{z}}$ and $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}$ are constant.)

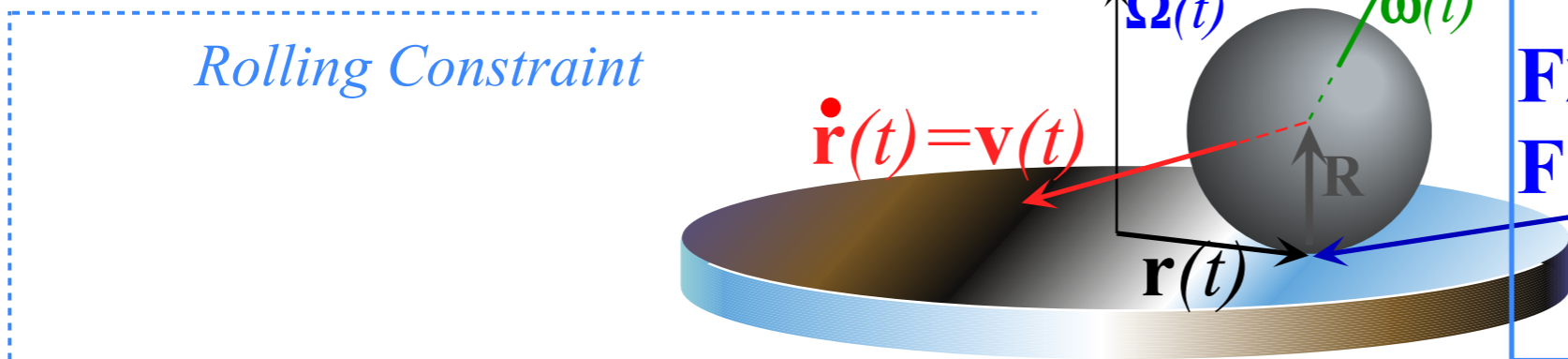
$$\mathbf{v}(t) = \boldsymbol{\Omega} \times \mathbf{r}(t) + \boldsymbol{\omega}(t) \times \mathbf{R} = \boldsymbol{\Omega} \times \mathbf{r}(t) + \boldsymbol{\omega}(t) \times \hat{\mathbf{z}} R$$

Torque-and-F=ma equations of motion:

$$\begin{aligned} I \dot{\boldsymbol{\omega}}(t) &= \mathbf{F}(t) \times \mathbf{R} \\ &= m \dot{\mathbf{v}}(t) \times \mathbf{R} \\ &= m \dot{\mathbf{v}}(t) \times \hat{\mathbf{z}} R \end{aligned}$$

Mechanical analog of cyclotron and FBI rule

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Rolling Constraint

Equations of Motion:

rotation *Torque* = $\mathbf{F} \times \mathbf{R} = I \dot{\boldsymbol{\omega}}$

$$\mathbf{F} \times \mathbf{R} = I \dot{\boldsymbol{\omega}}(t)$$

$$\mathbf{F} = m \dot{\mathbf{v}}(t)$$

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Turntable turning at constant angular velocity $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}$.

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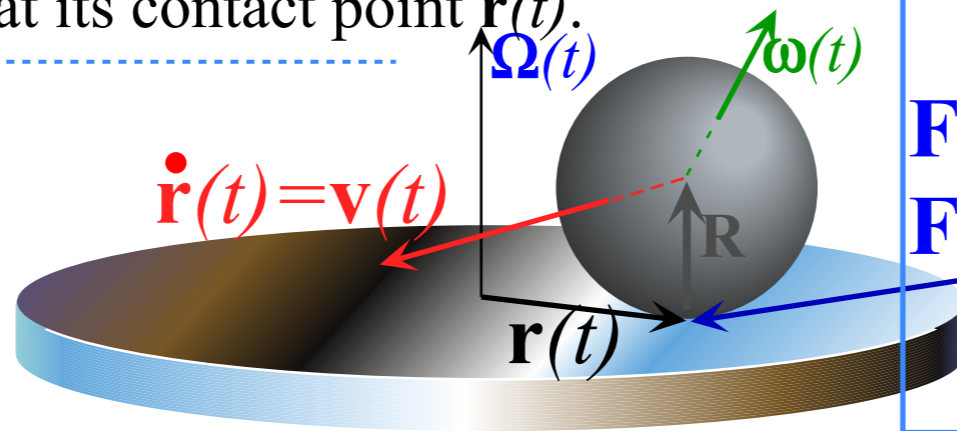
$$\dot{\mathbf{v}}(t) = \boldsymbol{\Omega} \times \dot{\mathbf{r}}(t) + \dot{\boldsymbol{\omega}}(t) \times \hat{\mathbf{z}} R = \boldsymbol{\Omega} \times \mathbf{v}(t) + \dot{\boldsymbol{\omega}}(t) \times \hat{\mathbf{z}} R$$

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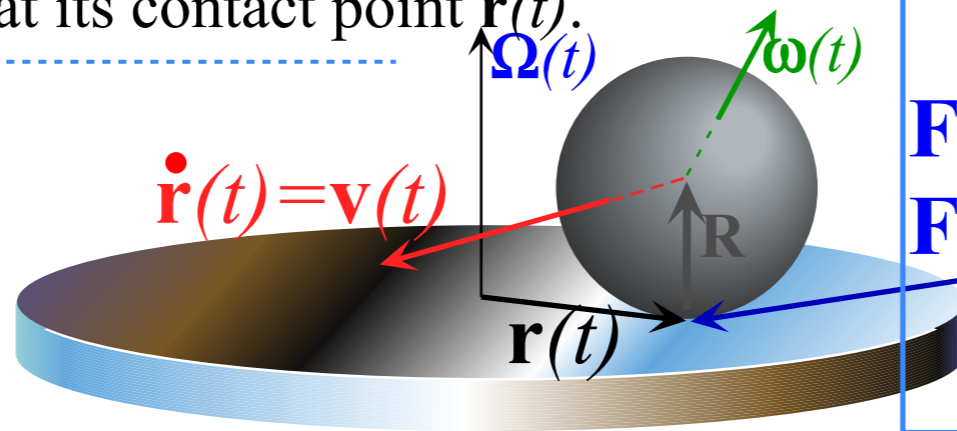
use:
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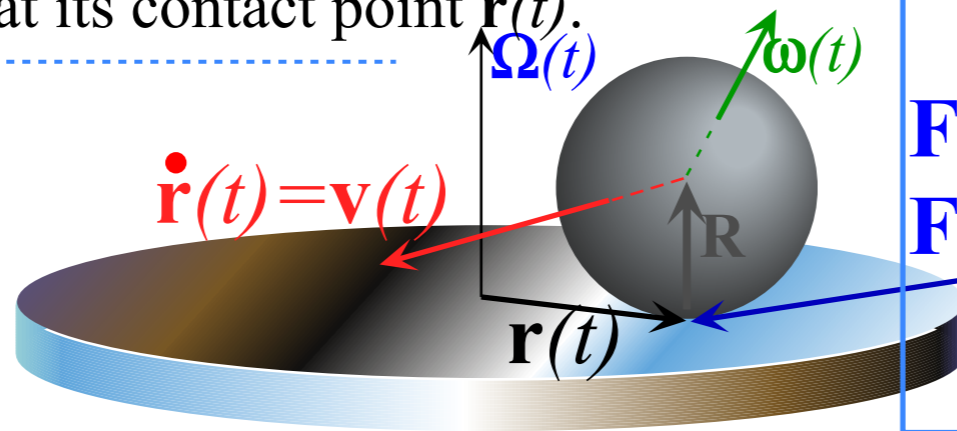
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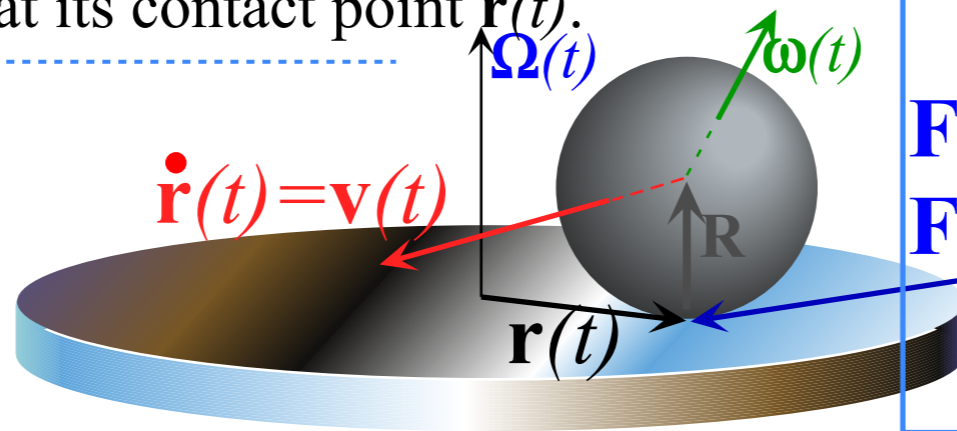
$$\dot{\mathbf{v}}(t) = \boldsymbol{\Omega} \times \mathbf{v}(t) + \frac{m \dot{\mathbf{v}}(t) \cdot \hat{\mathbf{z}}R}{I} \hat{\mathbf{z}}R - \frac{mR^2}{I} \dot{\mathbf{v}}(t)$$

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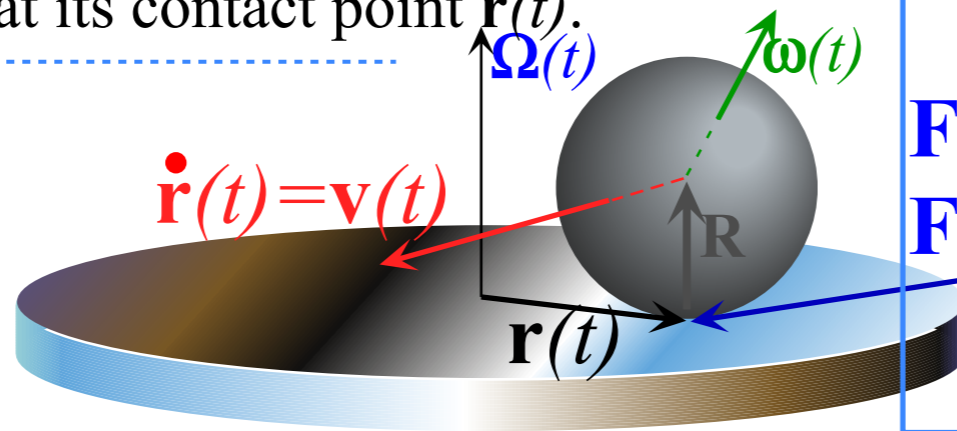
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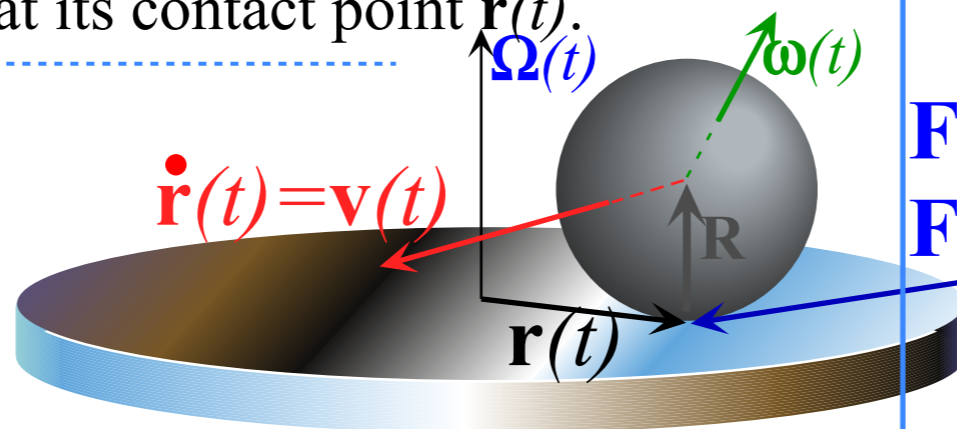
$$\left(1 + \frac{mR^2}{I}\right) \dot{\mathbf{v}}(t) = \boldsymbol{\Omega} \times \mathbf{v}(t)$$

$\mathbf{F} = \mathbf{B} \times \mathbf{v}$ mechanical analog:

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Mechanical analog cyclotron frequency

$$\omega = \frac{e}{m} B = \frac{\boldsymbol{\Omega}}{1 + \frac{m R^2}{I}}$$

$$\omega = \frac{2}{7} \boldsymbol{\Omega} \text{ for: } \frac{I}{m R^2} = \frac{2}{5} \quad \text{●}$$

$$= \frac{2}{5} \boldsymbol{\Omega} \text{ for: } \frac{I}{m R^2} = \frac{2}{3} \quad \text{○}$$



[YouTube Video of Analog to Synchrotron Motion](#)

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*Solid ball has 2 orbits
as table turns 7 rotations*

*Mechanical analog
cyclotron frequency*

$$\omega = \frac{e}{m} B = \frac{\Omega}{1 + \frac{mR^2}{I}}$$

$\omega = \frac{2}{7} \Omega$ for: $\frac{I}{mR^2} = \frac{2}{5}$

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Crossed E and B field mechanics

Classical Hall-effect and cyclotron orbit orbit equations

Vector theory vs. complex variable theory

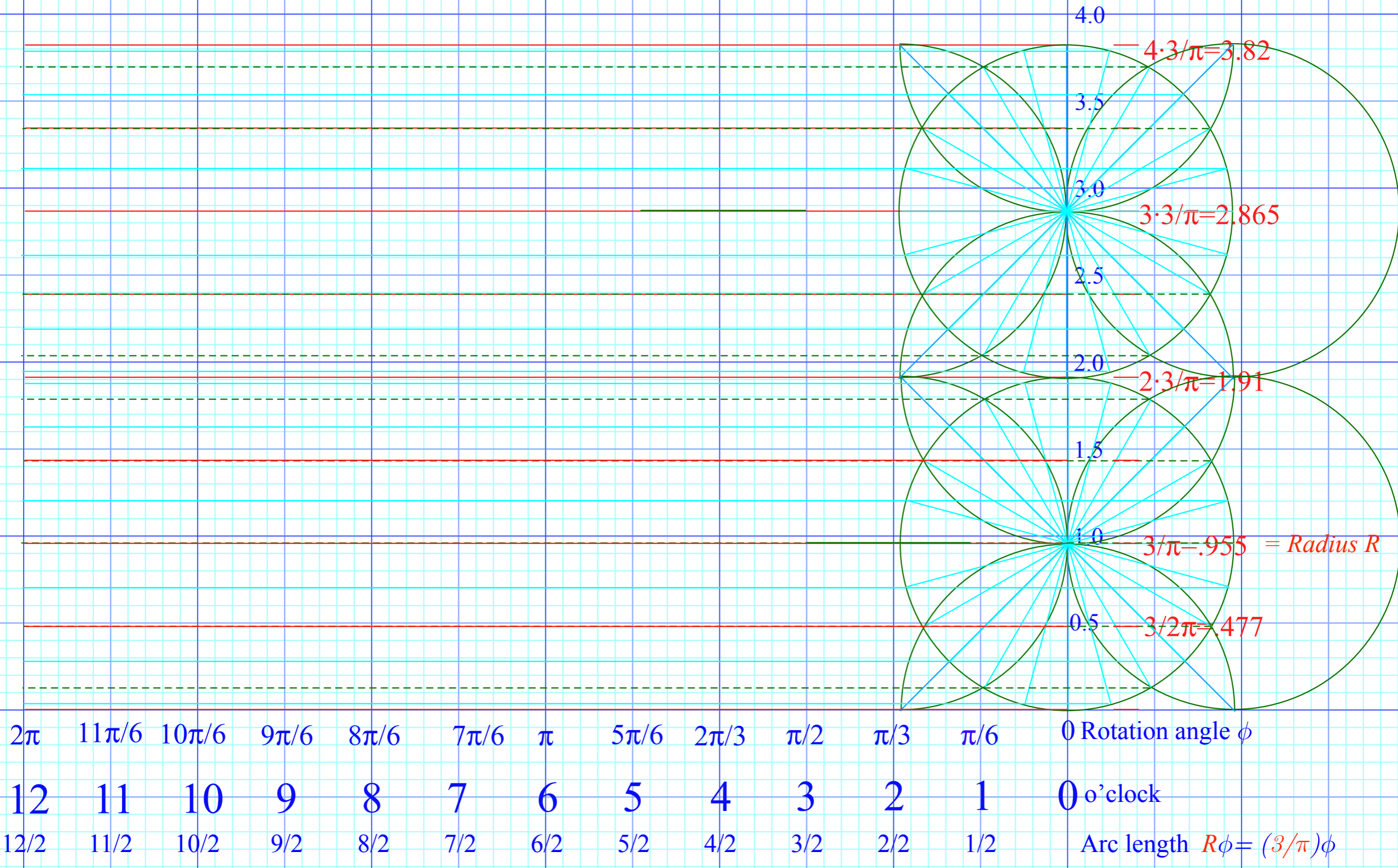
Mechanical analog of cyclotron and FBI rule

 *Cycloid and epicycloid ruler&compass geometry*

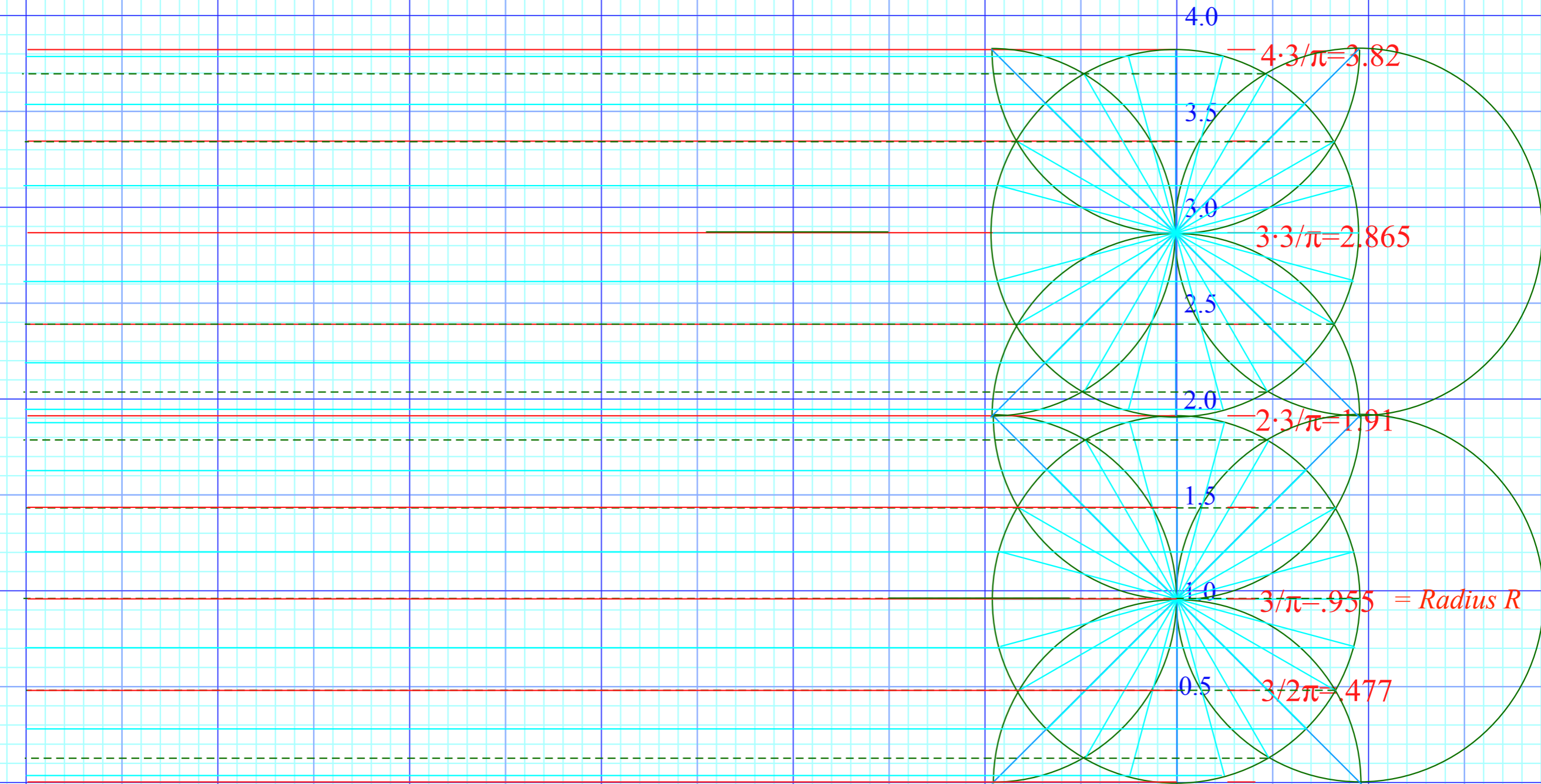
Cycloid geometry of flying levers

Practical poolhall application

Here the radius is plotted as an irrational $R=3/\pi=0.955$ length so rolling by rational angle $\phi = m\pi/n$ is a rational length of rolled-out circumference $R\phi = (3/\pi)m\pi/n = 3m/n$.



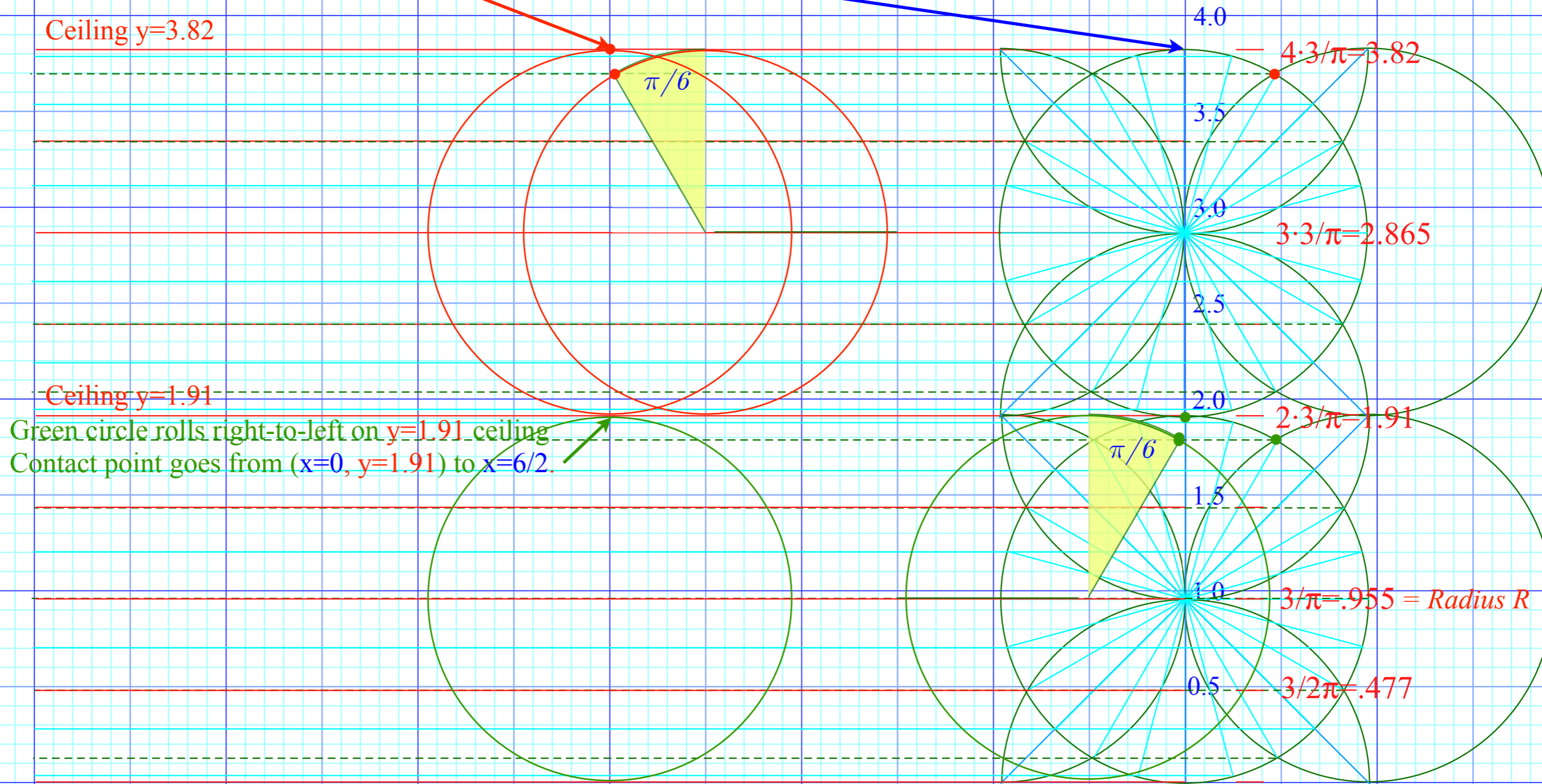
Here the radius is plotted as an irrational $R=3/\pi=0.955$ length so rolling by rational angle $\phi = m\pi/n$ is a rational length of rolled-out circumference $R\phi = (3/\pi)m\pi/n = 3m/n$. Diameter is $2R=6/\pi=1.91$



2π	$11\pi/6$	$10\pi/6$	$9\pi/6$	$8\pi/6$	$7\pi/6$	π	$5\pi/6$	$2\pi/3$	$\pi/2$	$\pi/3$	$\pi/6$	0	Rotation angle ϕ
12	11	10	9	8	7	6	5	4	3	2	1	0	o'clock
$12/2$	$11/2$	$10/2$	$9/2$	$8/2$	$7/2$	$6/2$	$5/2$	$4/2$	$3/2$	$2/2$	$1/2$		Arc length $R\phi = (3/\pi)\phi$

Here the radius is plotted as an irrational $R=3/\pi=0.955$ length so rolling by rational angle $\phi = m\pi/n$ is a rational length of rolled-out circumference $R\phi = (3/\pi)m\pi/n = 3m/n$. Diameter is $2R=6/\pi=1.91$

Red circle rolls left-to-right on $y=3.82$ ceiling
 Contact point goes from $(x=6/2, y=3.82)$ to $x=0$.

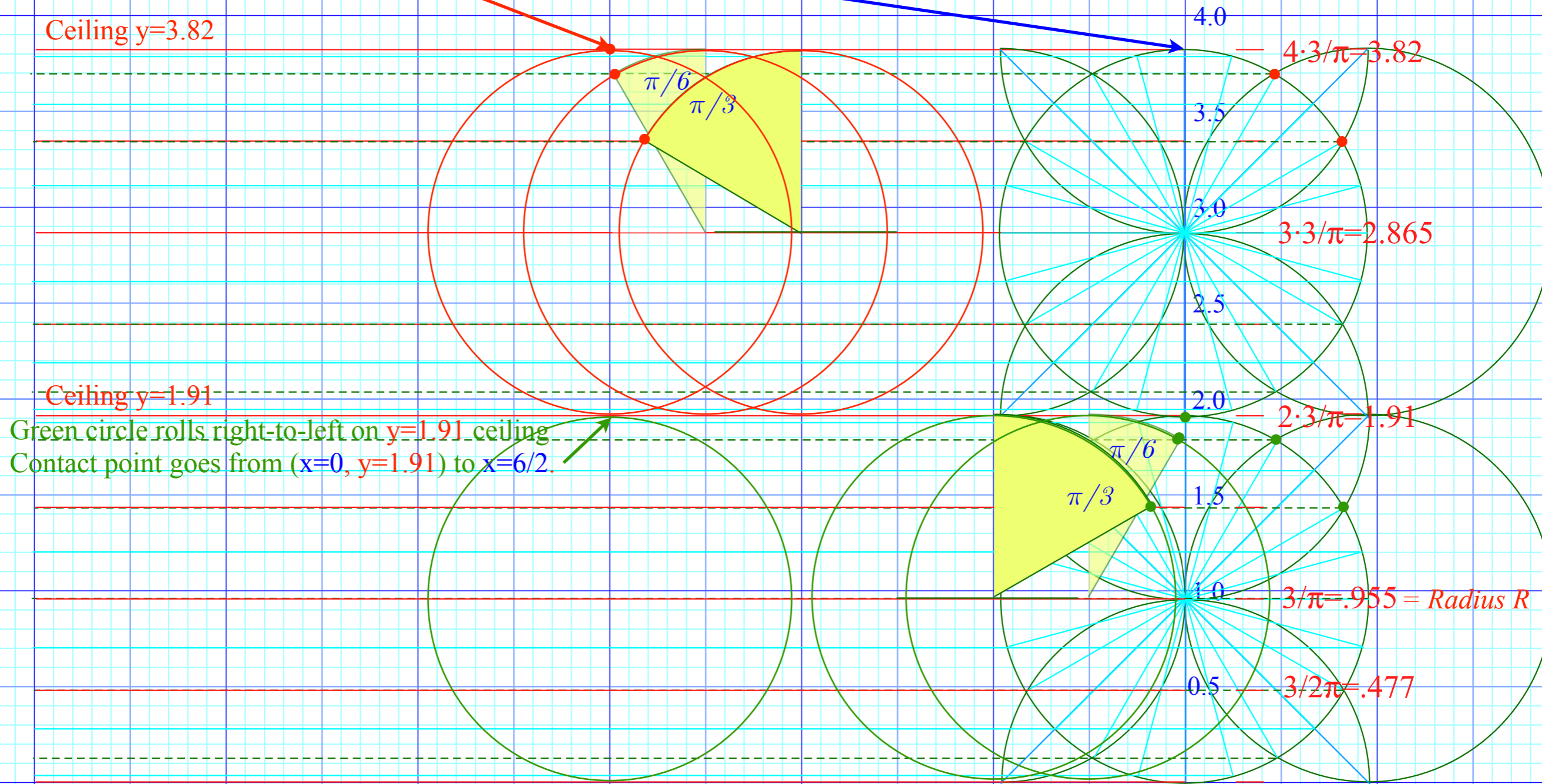


Green circle rolls right-to-left on $y=1.91$ ceiling
 Contact point goes from $(x=0, y=1.91)$ to $x=6/2$.

2π	$11\pi/6$	$10\pi/6$	$9\pi/6$	$8\pi/6$	$7\pi/6$	π	$5\pi/6$	$2\pi/3$	$\pi/2$	$\pi/3$	$\pi/6$	Rotation angle ϕ
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$12/2$	$11/2$	$10/2$	$9/2$	$8/2$	$7/2$	$6/2$	$5/2$	$4/2$	$3/2$	$2/2$	$1/2$	Arc length $R\phi = (3/\pi)\phi$

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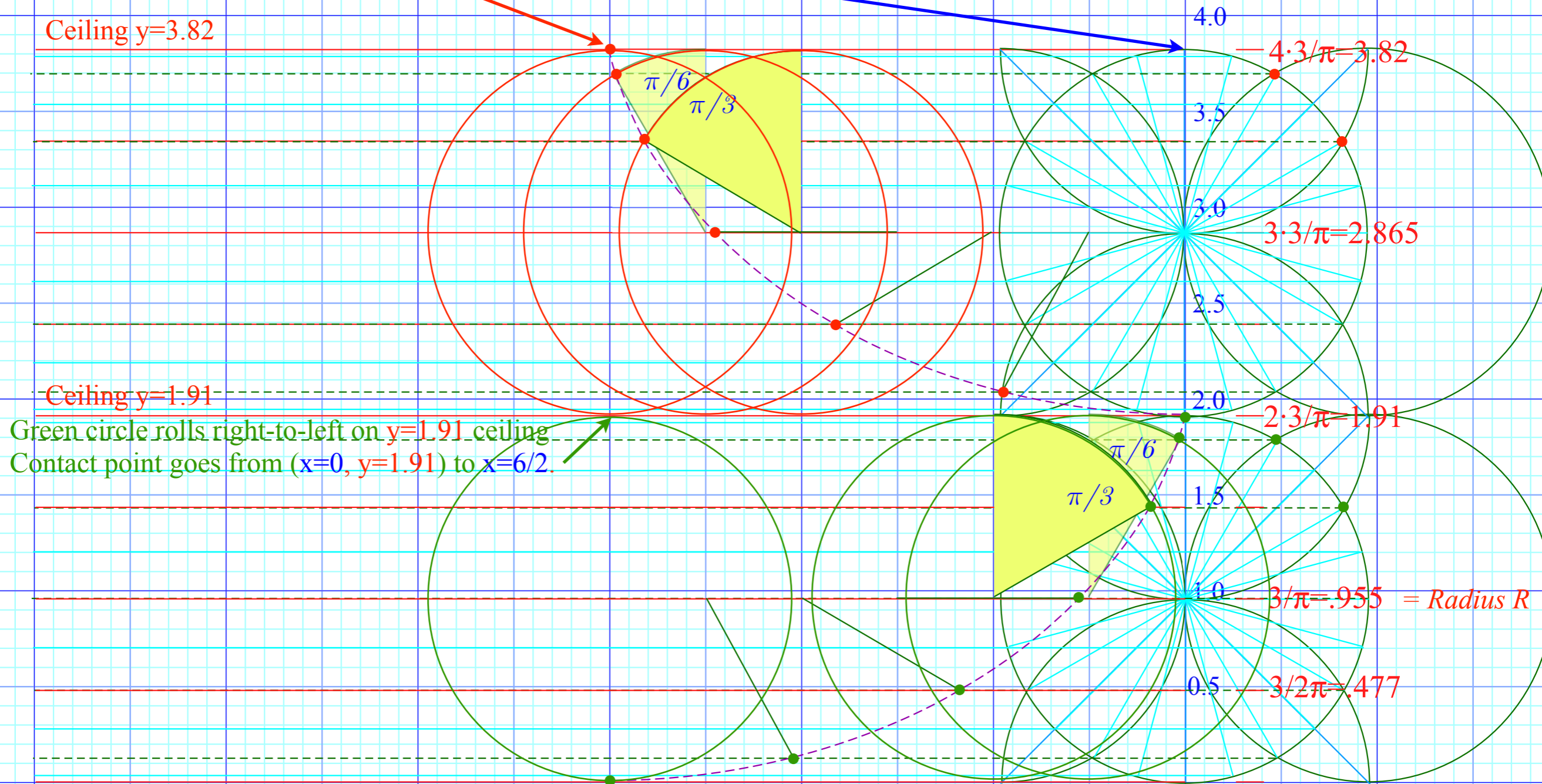
Red circle rolls left-to-right on $y=3.82$ ceiling
 Contact point goes from $(x=6/2, y=3.82)$ to $x=0$.



2π	$11\pi/6$	$10\pi/6$	$9\pi/6$	$8\pi/6$	$7\pi/6$	π	$5\pi/6$	$2\pi/3$	$\pi/2$	$\pi/3$	$\pi/6$	Rotation angle ϕ
12	11	10	9	8	7	6	5	4	3	2	1	0 o'clock
$12/2$	$11/2$	$10/2$	$9/2$	$8/2$	$7/2$	$6/2$	$5/2$	$4/2$	$3/2$	$2/2$	$1/2$	Arc length $R\phi = (3/\pi)\phi$

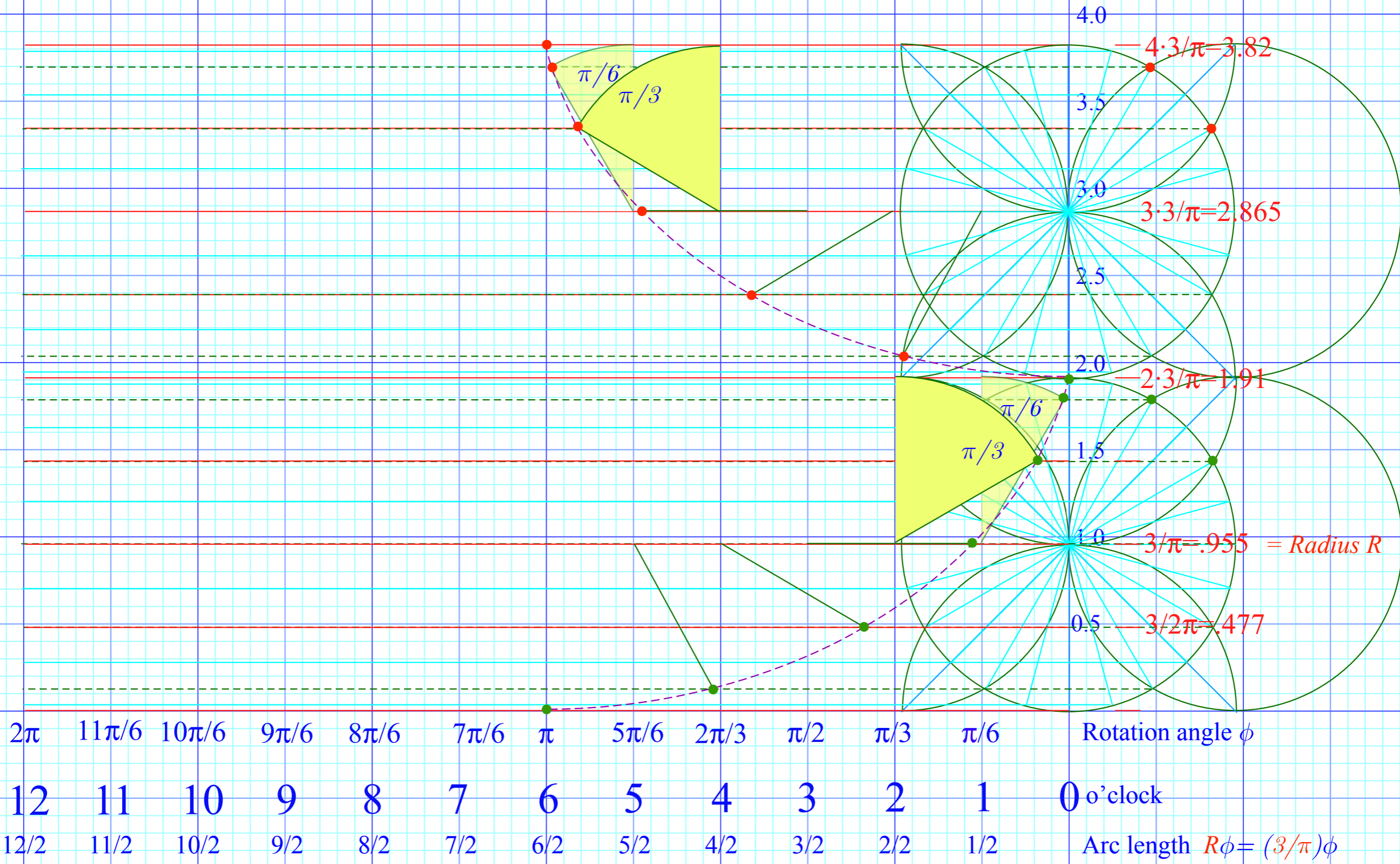
Here the radius is plotted as an irrational $R=3/\pi=0.955$ length so rolling by rational angle $\phi = m\pi/n$ is a rational length of rolled-out circumference $R\phi = (3/\pi)m\pi/n = 3m/n$. Diameter is $2R=6/\pi=1.91$

Red circle rolls left-to-right on $y=3.82$ ceiling
 Contact point goes from $(x=6/2, y=3.82)$ to $x=0$.

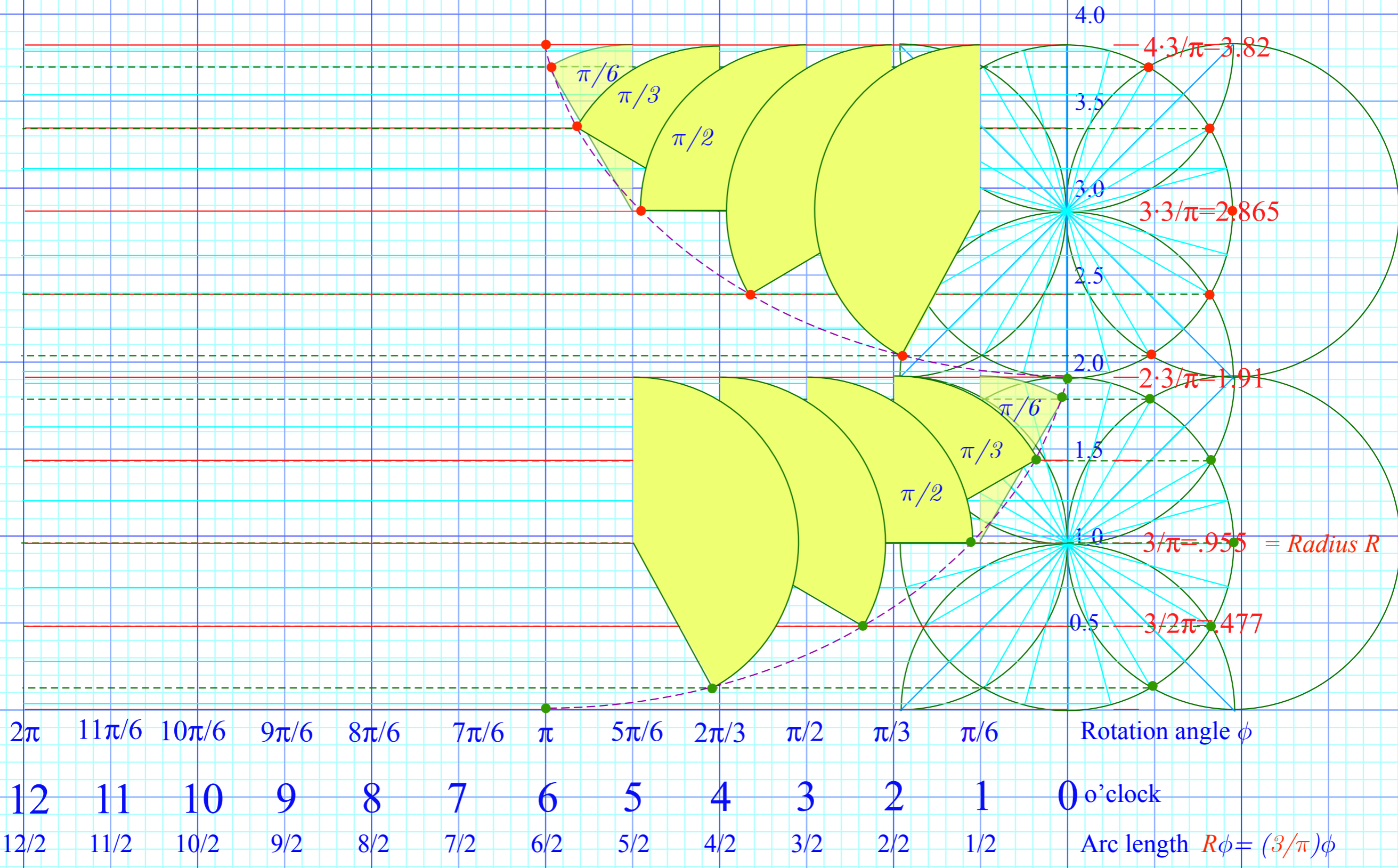


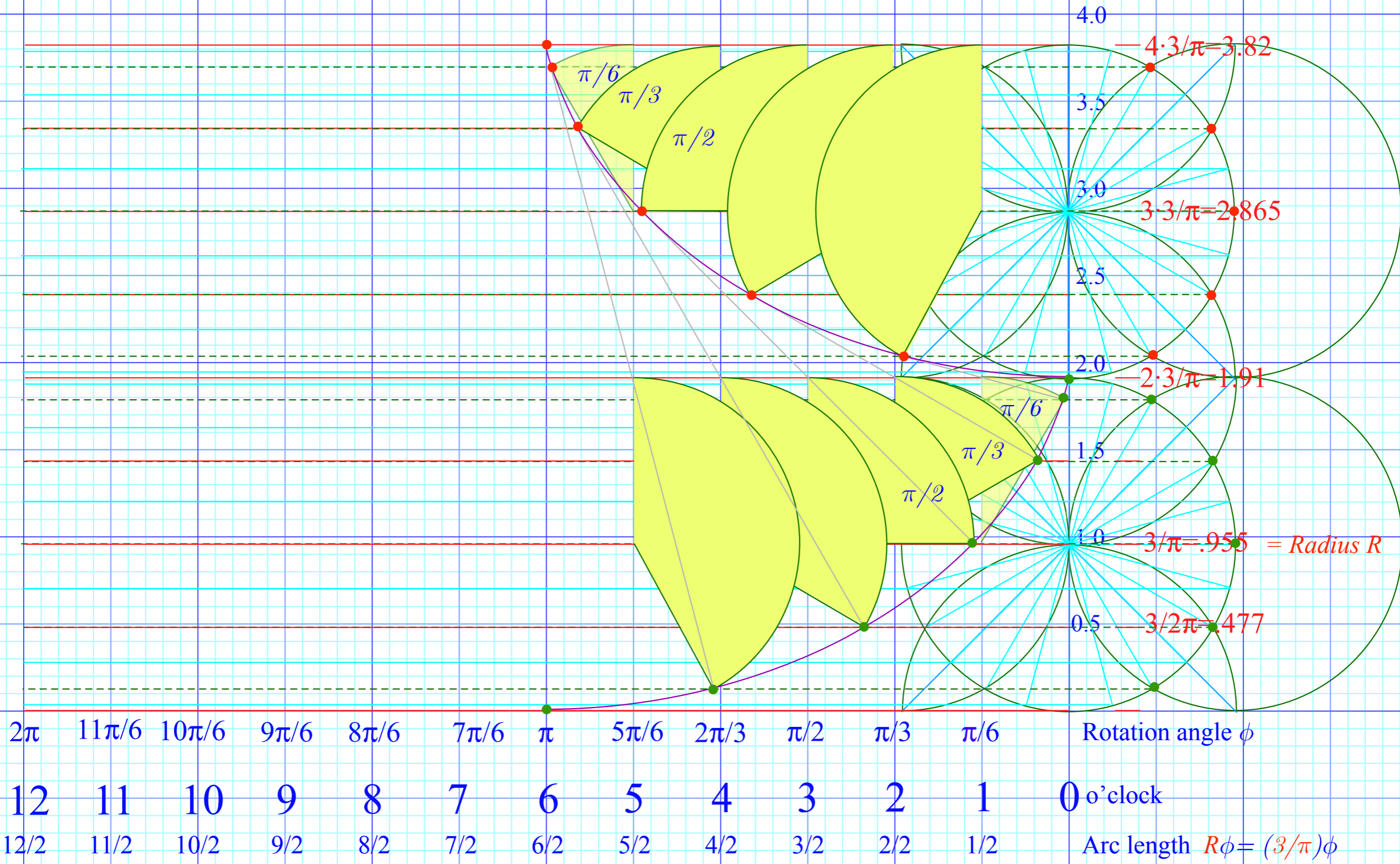
2π	$11\pi/6$	$10\pi/6$	$9\pi/6$	$8\pi/6$	$7\pi/6$	π	$5\pi/6$	$2\pi/3$	$\pi/2$	$\pi/3$	$\pi/6$	Rotation angle ϕ
12	11	10	9	8	7	6	5	4	3	2	1	0 o'clock
$12/2$	$11/2$	$10/2$	$9/2$	$8/2$	$7/2$	$6/2$	$5/2$	$4/2$	$3/2$	$2/2$	$1/2$	Arc length $R\phi = (3/\pi)\phi$

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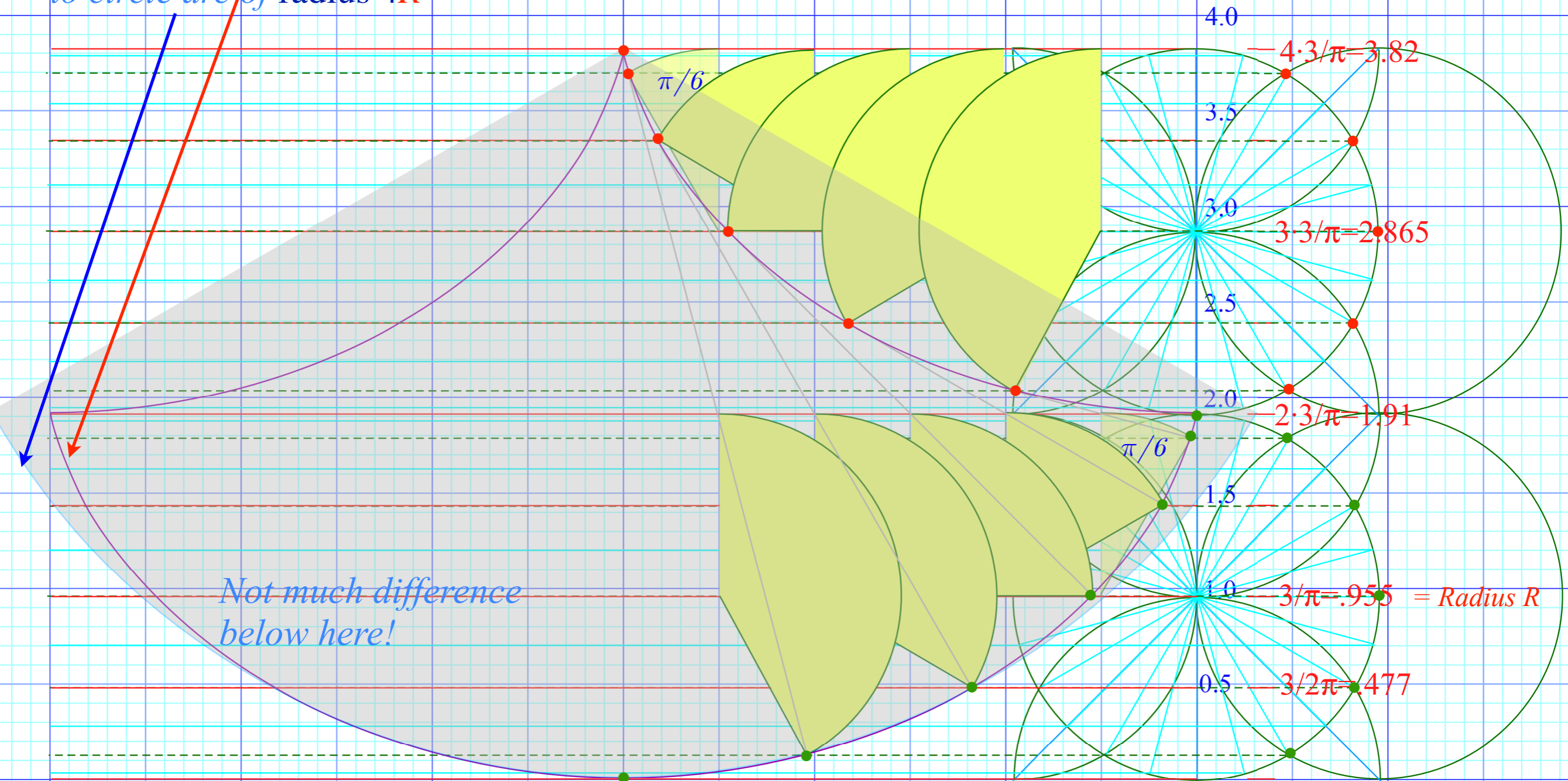
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Compare cycloid of y-diameter $2R$ and x-diameter $2\pi R$ to circle arc of radius $4R$



Not much difference below here!

2π	$11\pi/6$	$10\pi/6$	$9\pi/6$	$8\pi/6$	$7\pi/6$	π	$5\pi/6$	$2\pi/3$	$\pi/2$	$\pi/3$	$\pi/6$	Rotation angle ϕ
12	11	10	9	8	7	6	5	4	3	2	1	0 o'clock
$12/2$	$11/2$	$10/2$	$9/2$	$8/2$	$7/2$	$6/2$	$5/2$	$4/2$	$3/2$	$2/2$	$1/2$	Arc length $R\phi = (3/\pi)\phi$

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→ Cycloid and epicycloid geometry ←

Cycloid geometry of flying levers

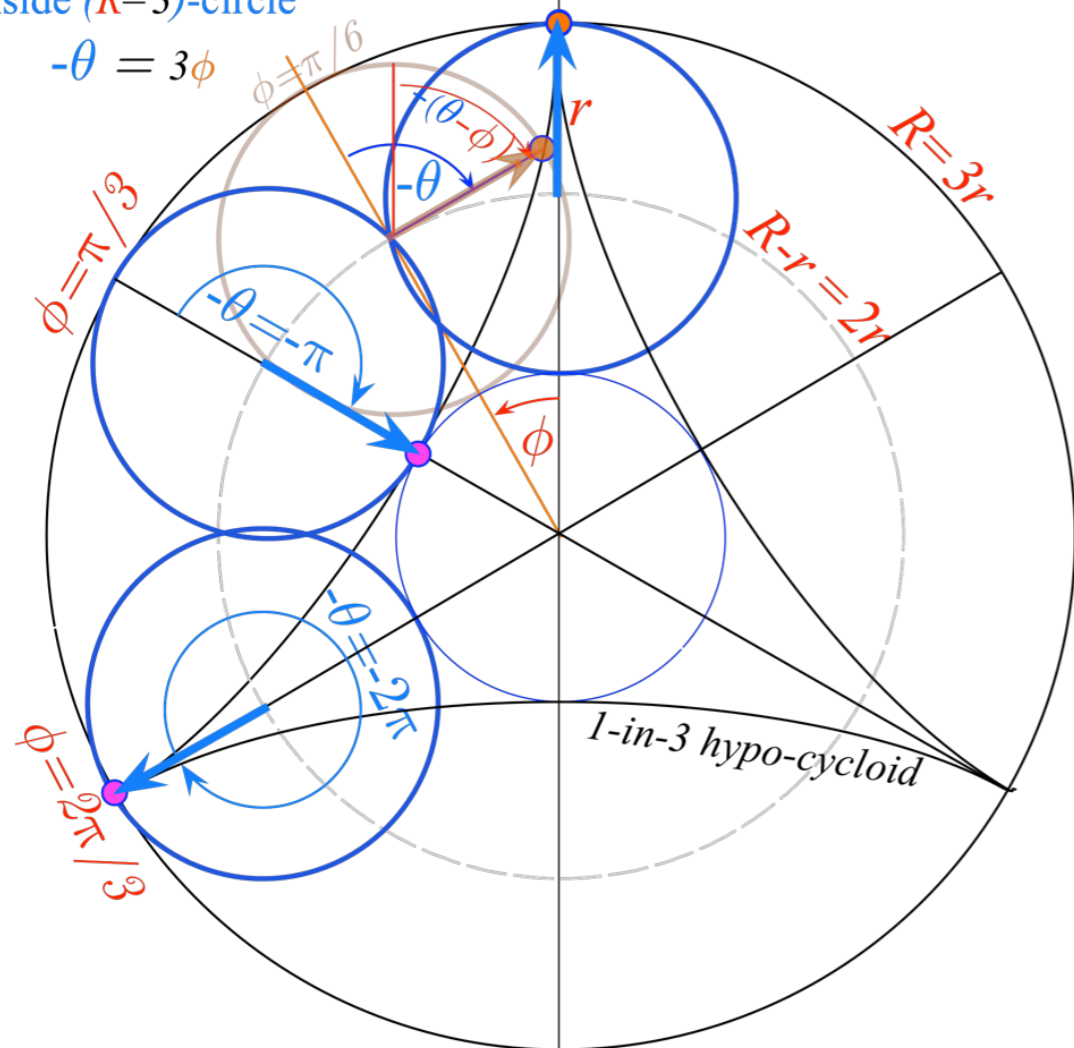
Practical poolhall application

Angular constraint

$$-\theta \cdot r = \phi \cdot R$$

($r=1$)-circle rolling
inside ($R=3$)-circle

$$-\theta = 3\phi$$



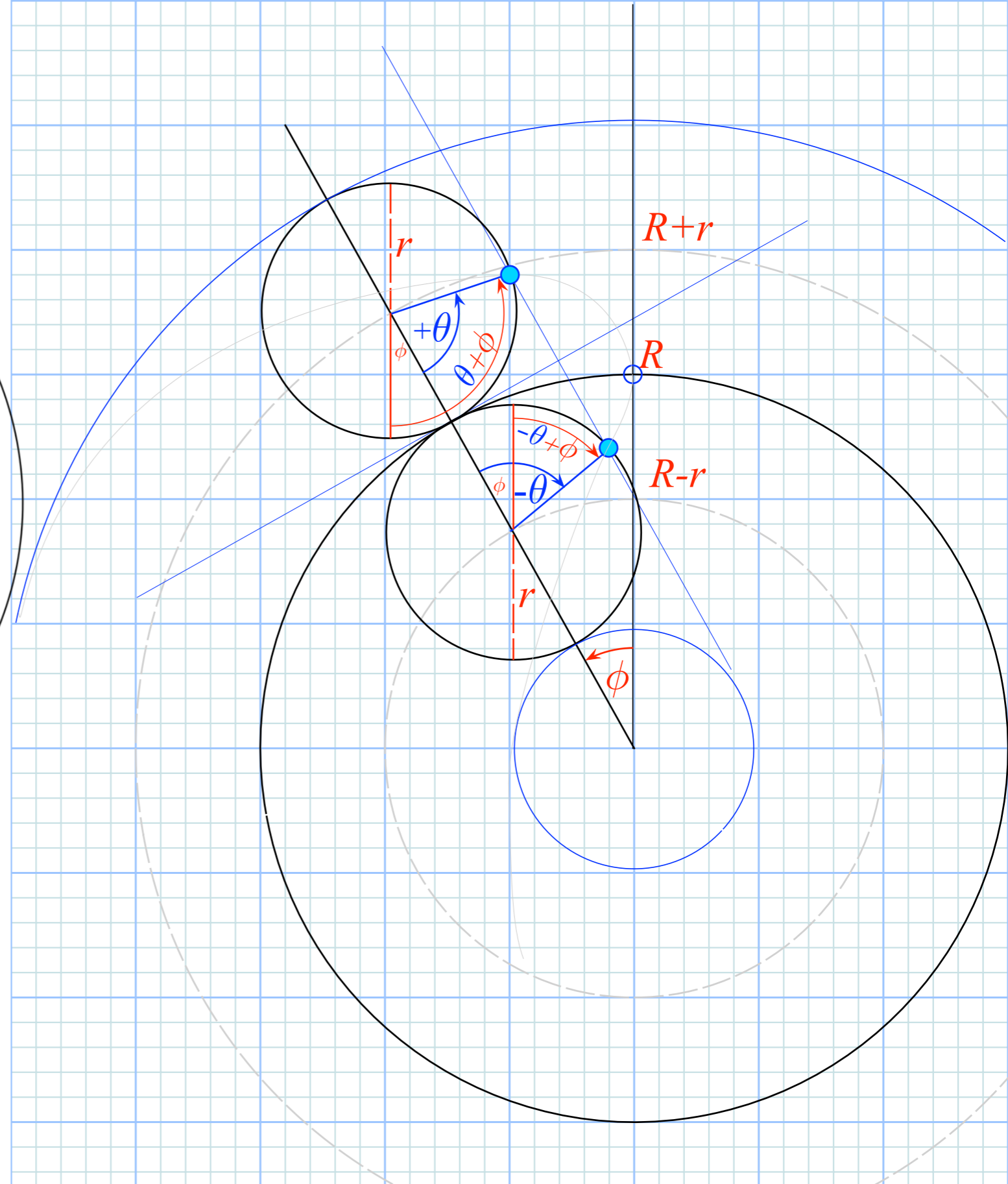
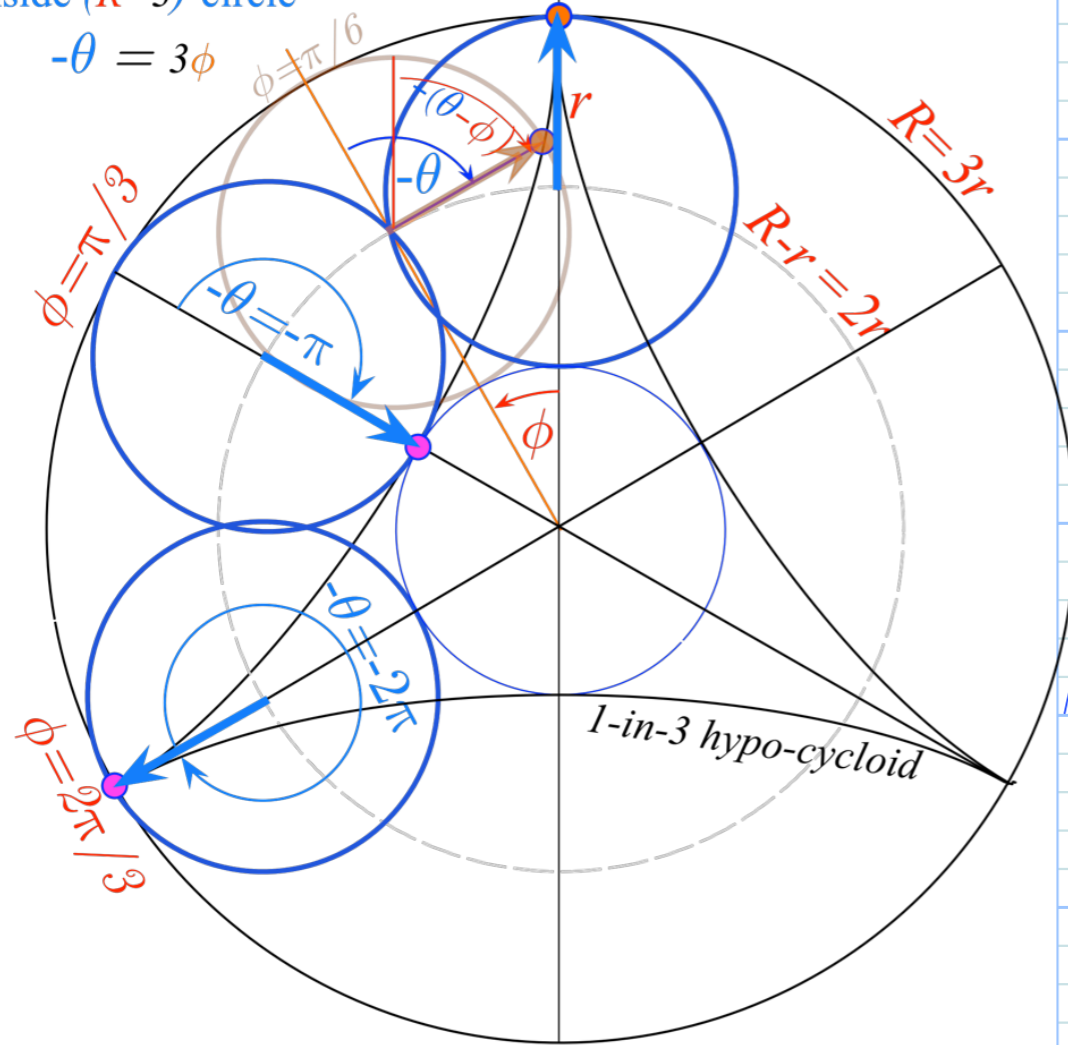
Hyper-and-Hypo-Cycloidal coordinate geometry and dynamics

Angular constraint

$$-\theta \cdot r = \phi \cdot R$$

($r=1$)-circle rolling
inside ($R=3$)-circle

$$-\theta = 3\phi$$



Hyper-and-Hypo-Cycloidal coordinate geometry and dynamics

Hyper-cycloid constrained by: $\theta r = R\phi$ or: $\theta = \frac{R}{r}\phi$

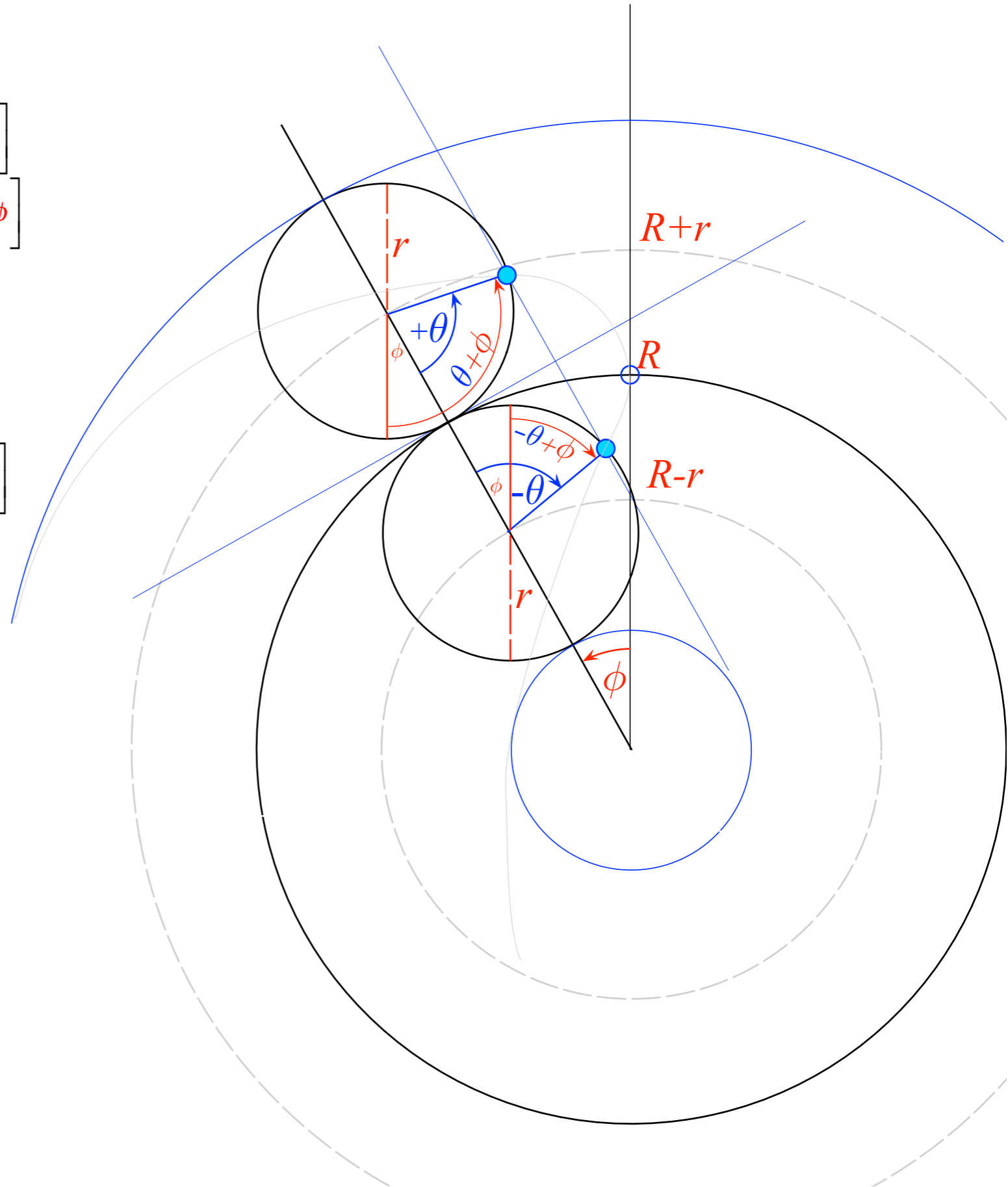
$$x = -(R+r)\sin\phi + r\sin(\theta + \phi) = r \left[-\left(\frac{R}{r}+1\right)\sin\phi + \sin\left(\frac{R}{r}+1\right)\phi \right]$$

$$y = (R+r)\cos\phi - r\cos(\theta + \phi) = r \left[\left(\frac{R}{r}+1\right)\cos\phi - \cos\left(\frac{R}{r}+1\right)\phi \right]$$

Hypo-cycloid constrained by: $-\theta r = -R\phi$ or: $\theta = \frac{R}{r}\phi$

$$x = -(R-r)\sin\phi + r\sin(\theta - \phi) = r \left[-\left(\frac{R}{r}-1\right)\sin\phi + \sin\left(\frac{R}{r}-1\right)\phi \right]$$

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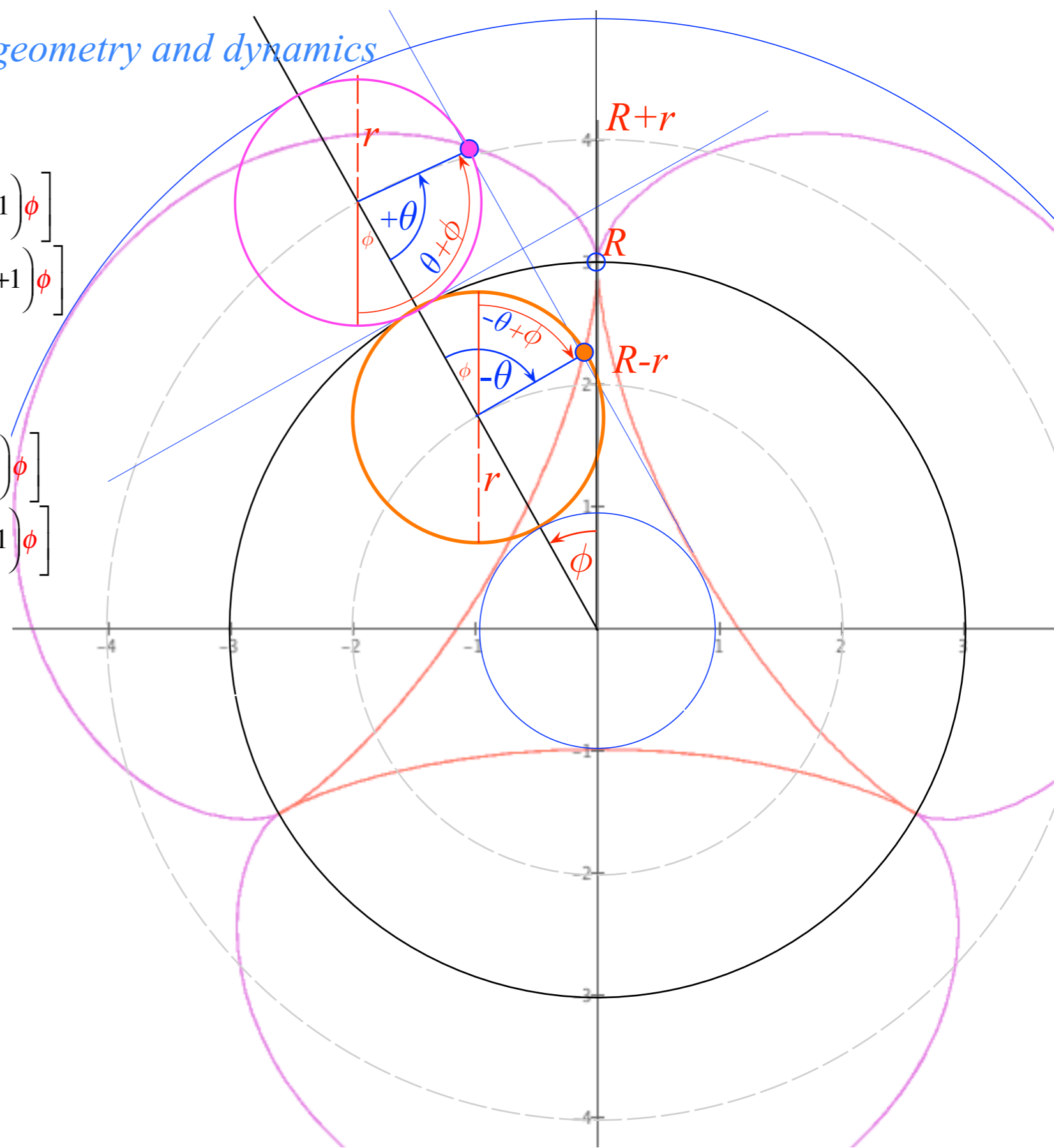
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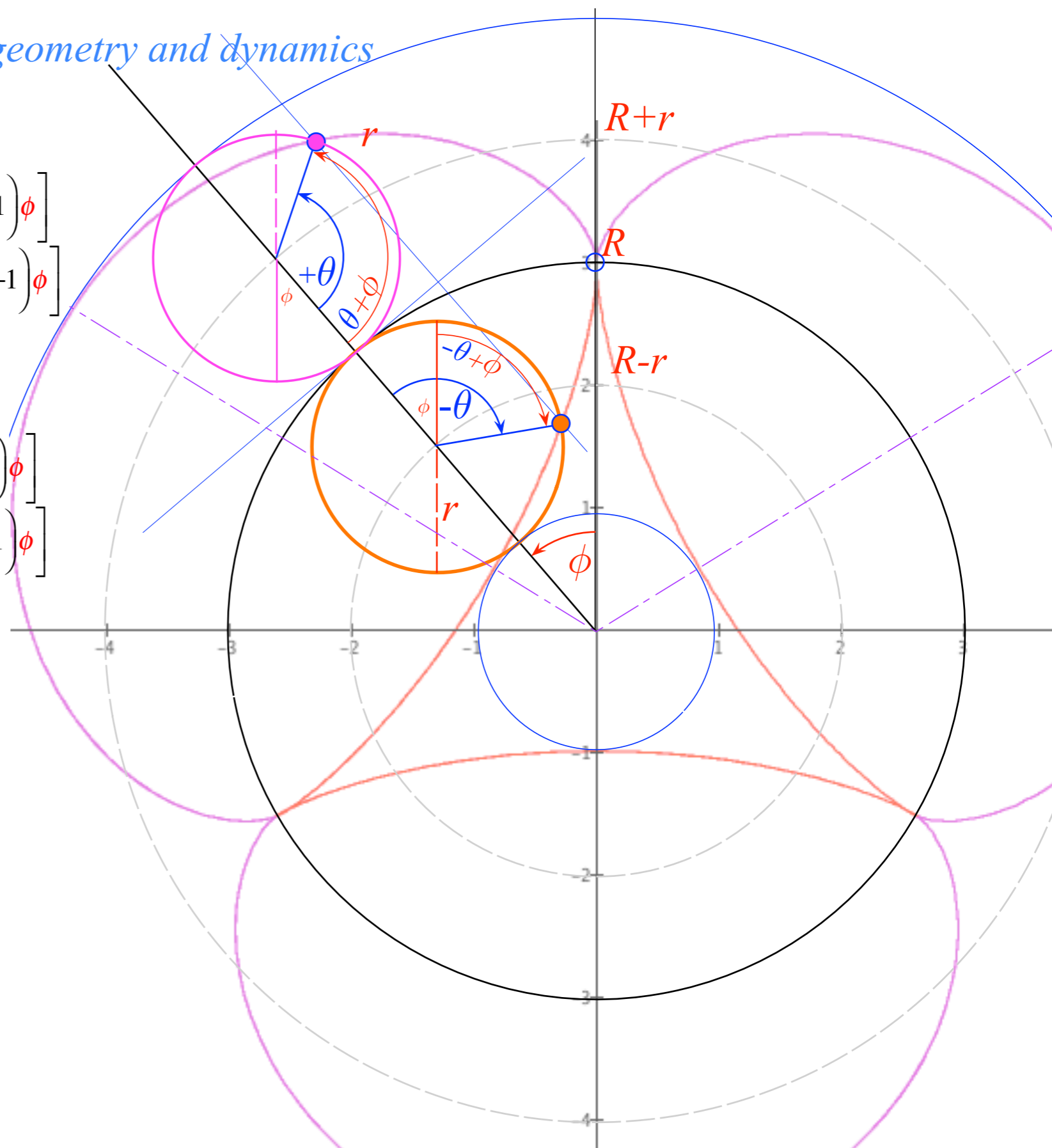
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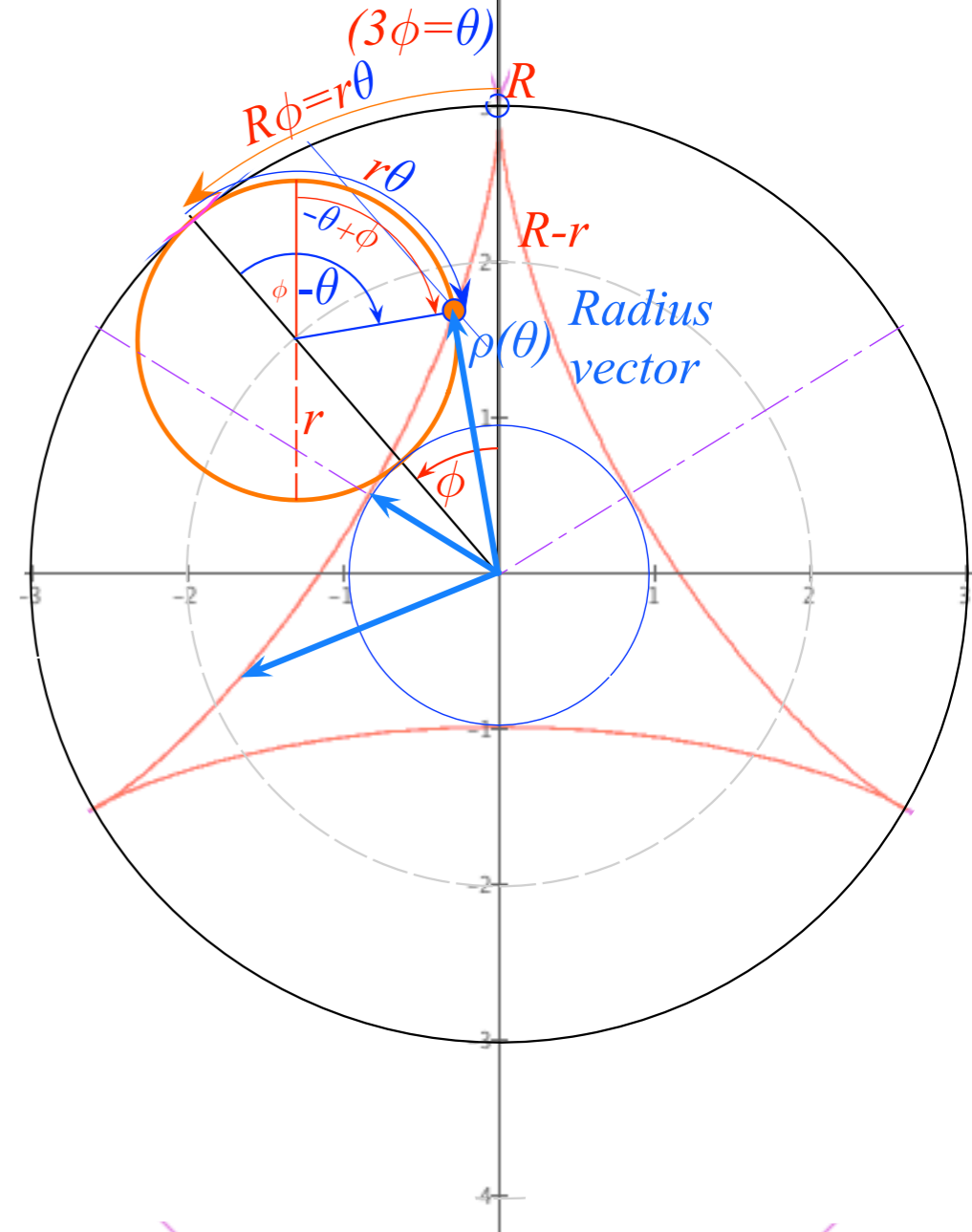
Hypo-cycloid trajectory radius ρ for: $r = 1$

$$x = -(R-1)\sin\phi + \sin(R-1)\phi \quad x^2 = (R-1)^2 \sin^2\phi - 2(R-1)\sin\phi\sin(R-1)\phi + \sin^2(R-1)\phi$$

$$y = (R-1)\cos\phi + \cos(R-1)\phi \quad y^2 = (R-1)^2 \cos^2\phi + 2(R-1)\cos\phi\cos(R-1)\phi + \cos^2(R-1)\phi$$

$$\rho^2 = x^2 + y^2 = (R-1)^2 + 2(R-1)[\cos\phi\cos(R-1)\phi - \sin\phi\sin(R-1)\phi] + 1$$

$$\rho^2 = x^2 + y^2 = (R-1)^2 + 2(R-1)\cos(R\phi) + 1$$



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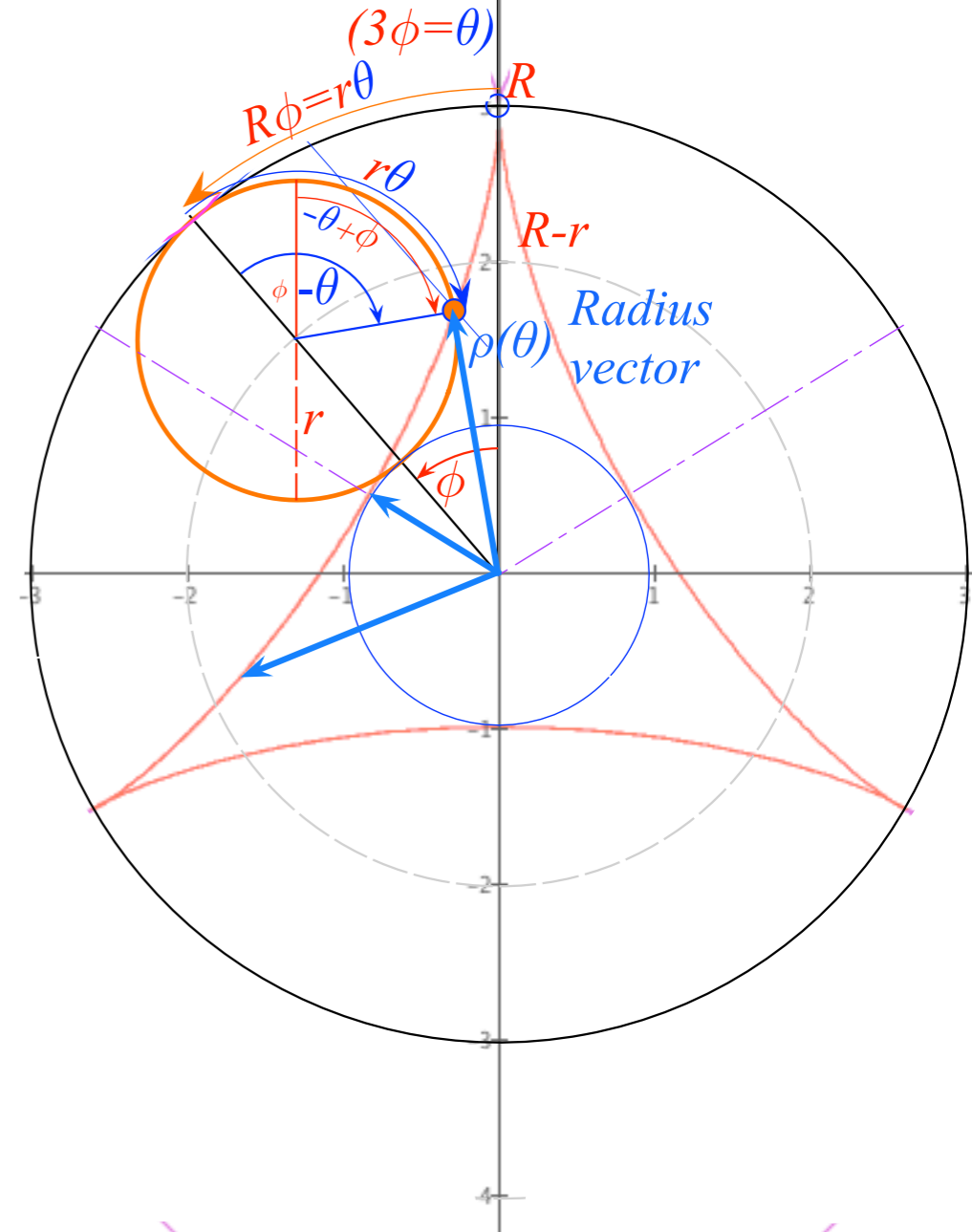
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$$\rho^2 = x^2 + y^2 = (R-1)^2 + 2(R-1)\cos(R\phi) + 1 = R^2 - 4(R-1)\sin^2\frac{R\phi}{2}$$



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Practical poolhall application

If you hammer a stick at a point h meters from its center
 you give it some linear momentum Π
 and some angular momentum $\Lambda = h \cdot \Pi$

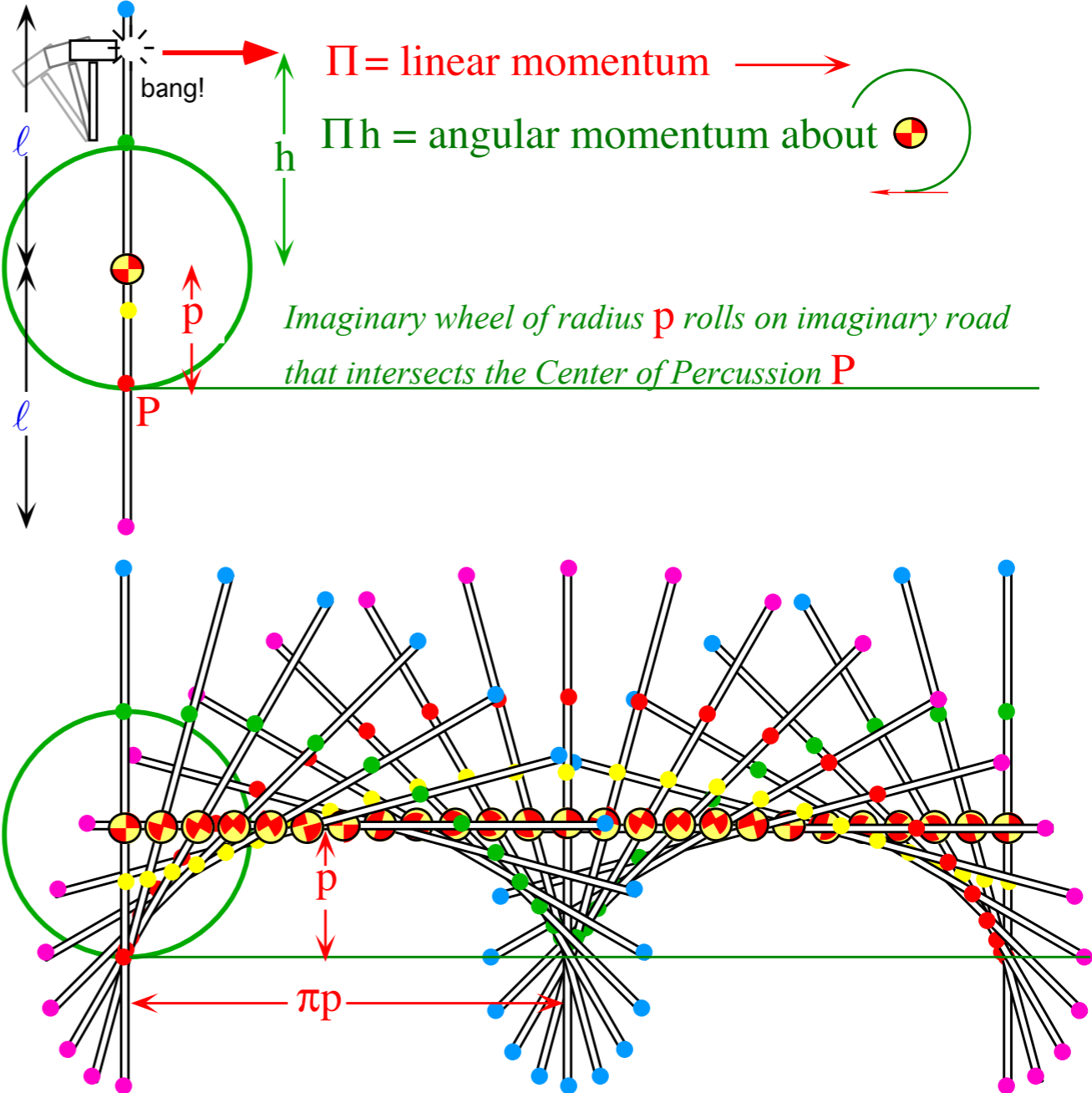


Fig. 2.A.1 Cycloidic paths due to hitting a stationary stick.

If you hammer a stick at a point h meters from its center
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Resulting angular velocity ω about the center
 is angular momentum Λ divided by
 moment of inertia $I = M \ell^2/3$ of the stick.

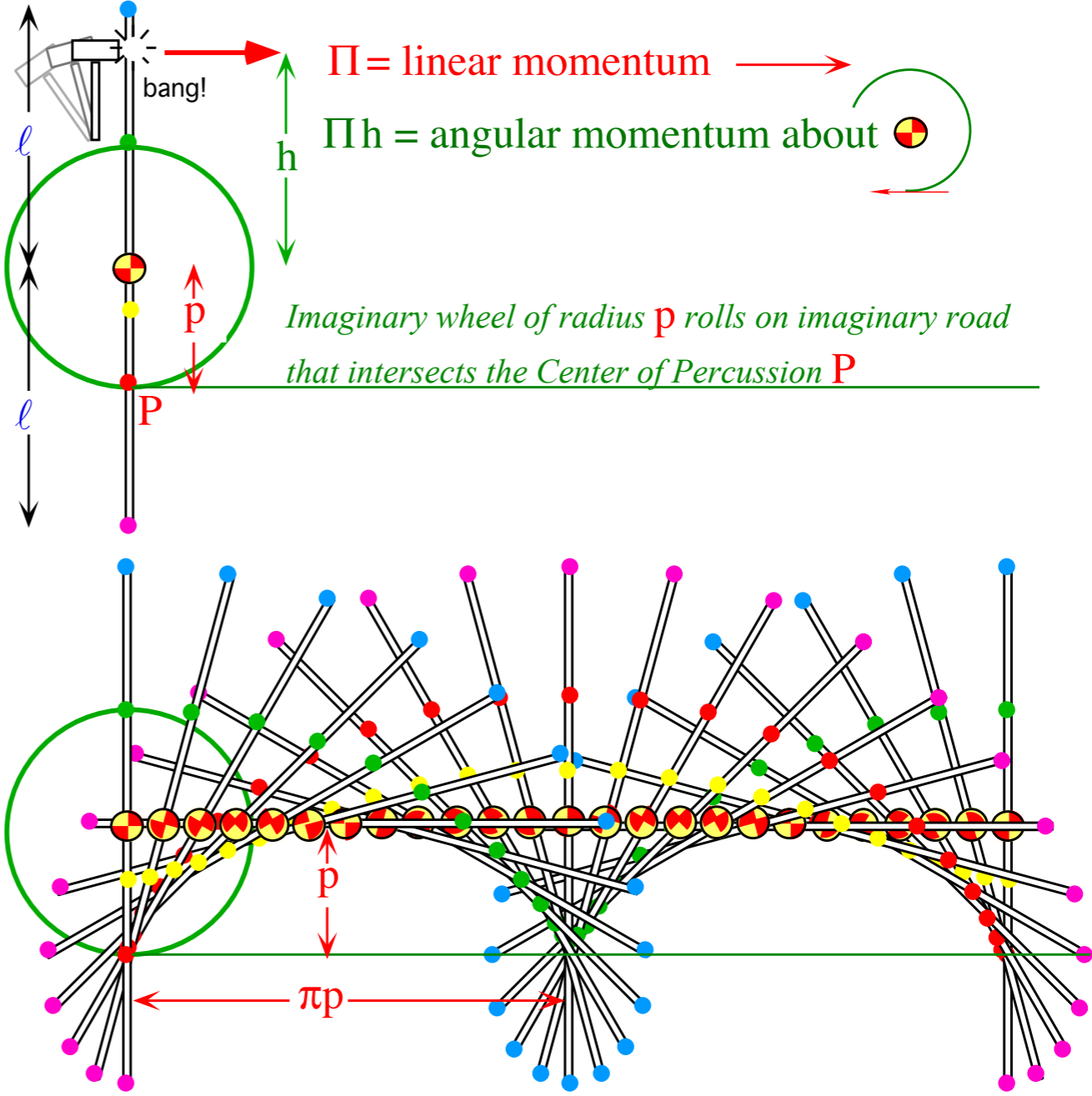


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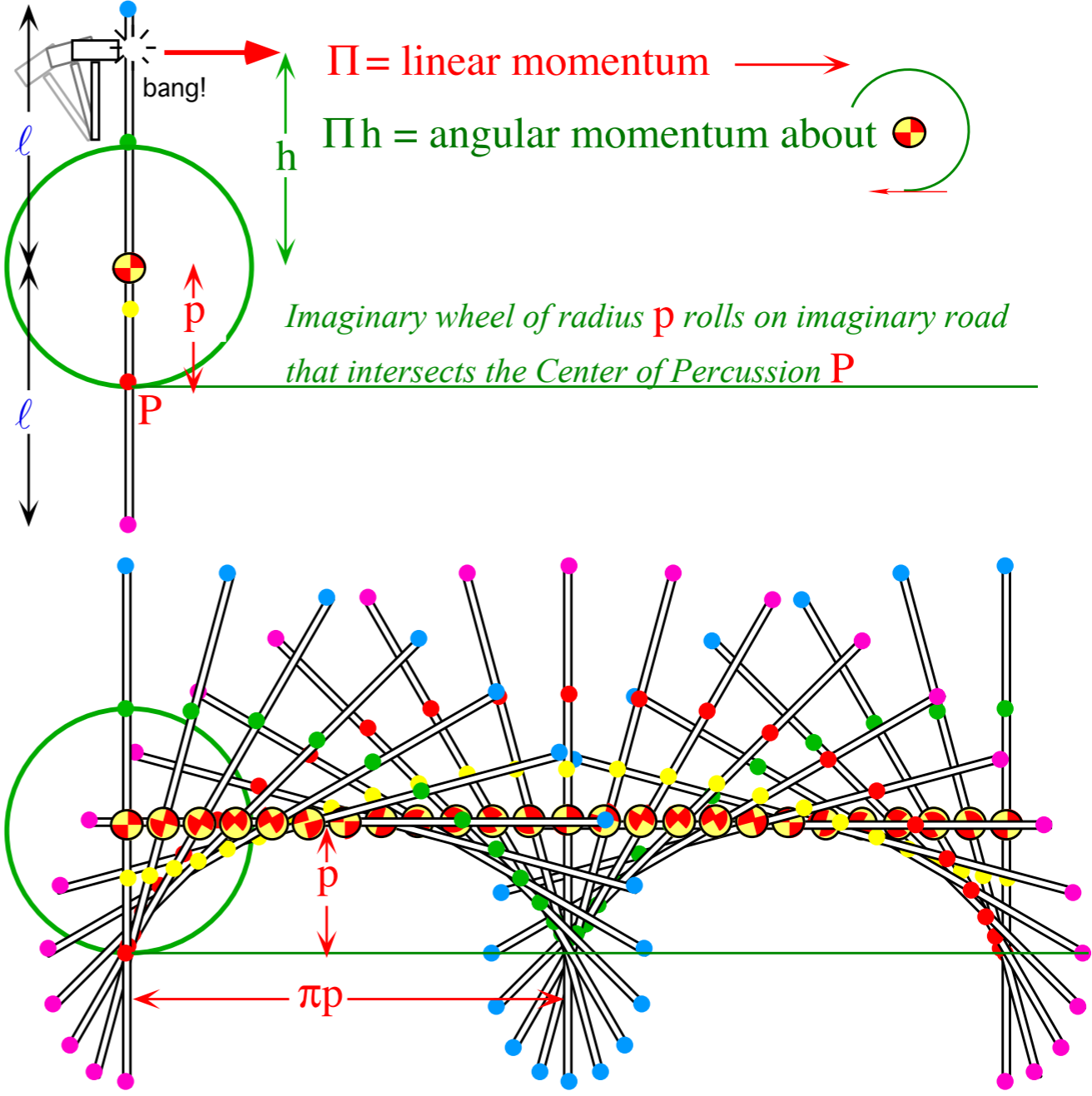


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One point P , or *center of percussion (CoP)*, is
 on the wheel where speed $p\omega$ due to rotation
 just cancels translational speed V_{Center} of stick.

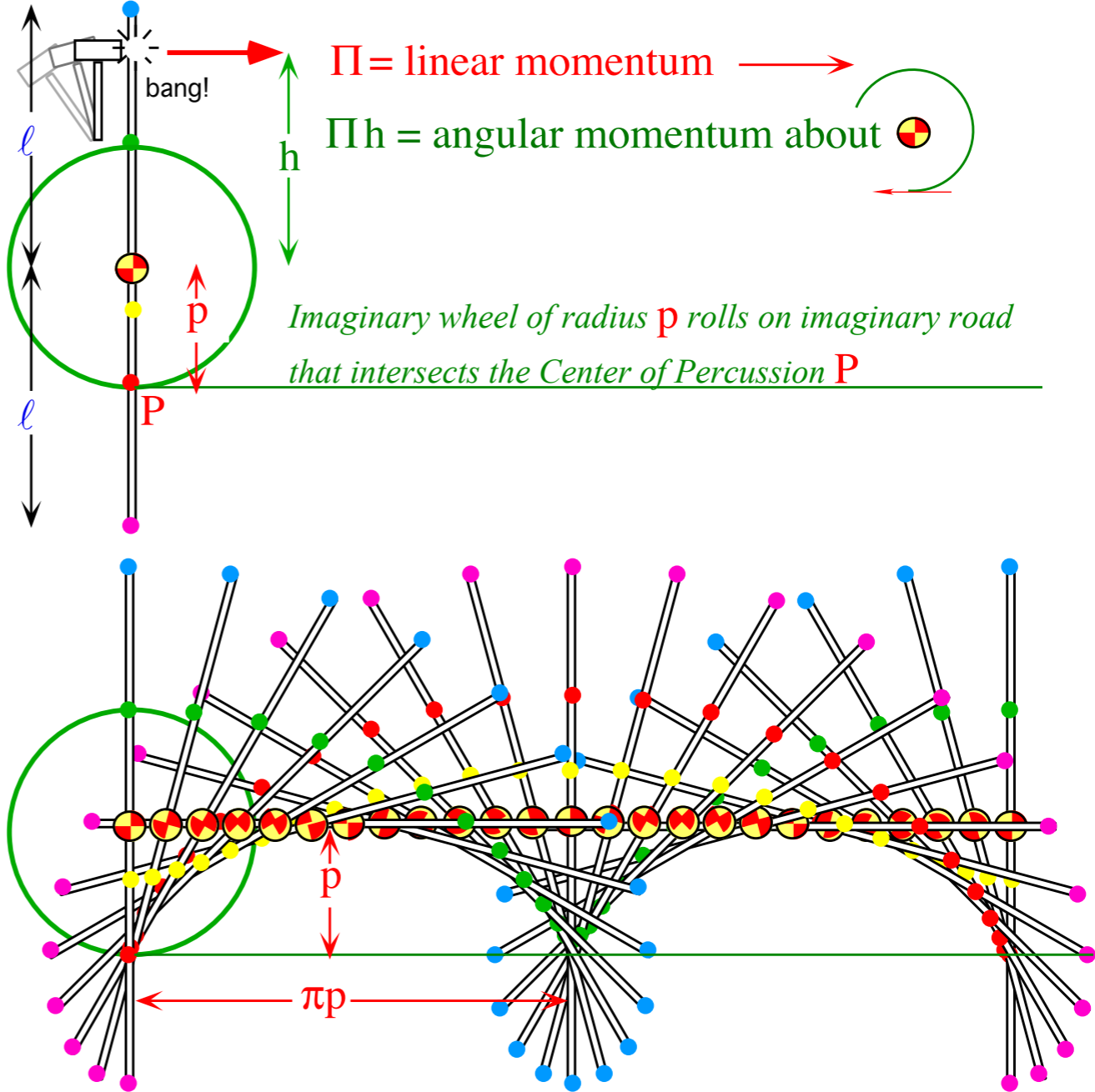


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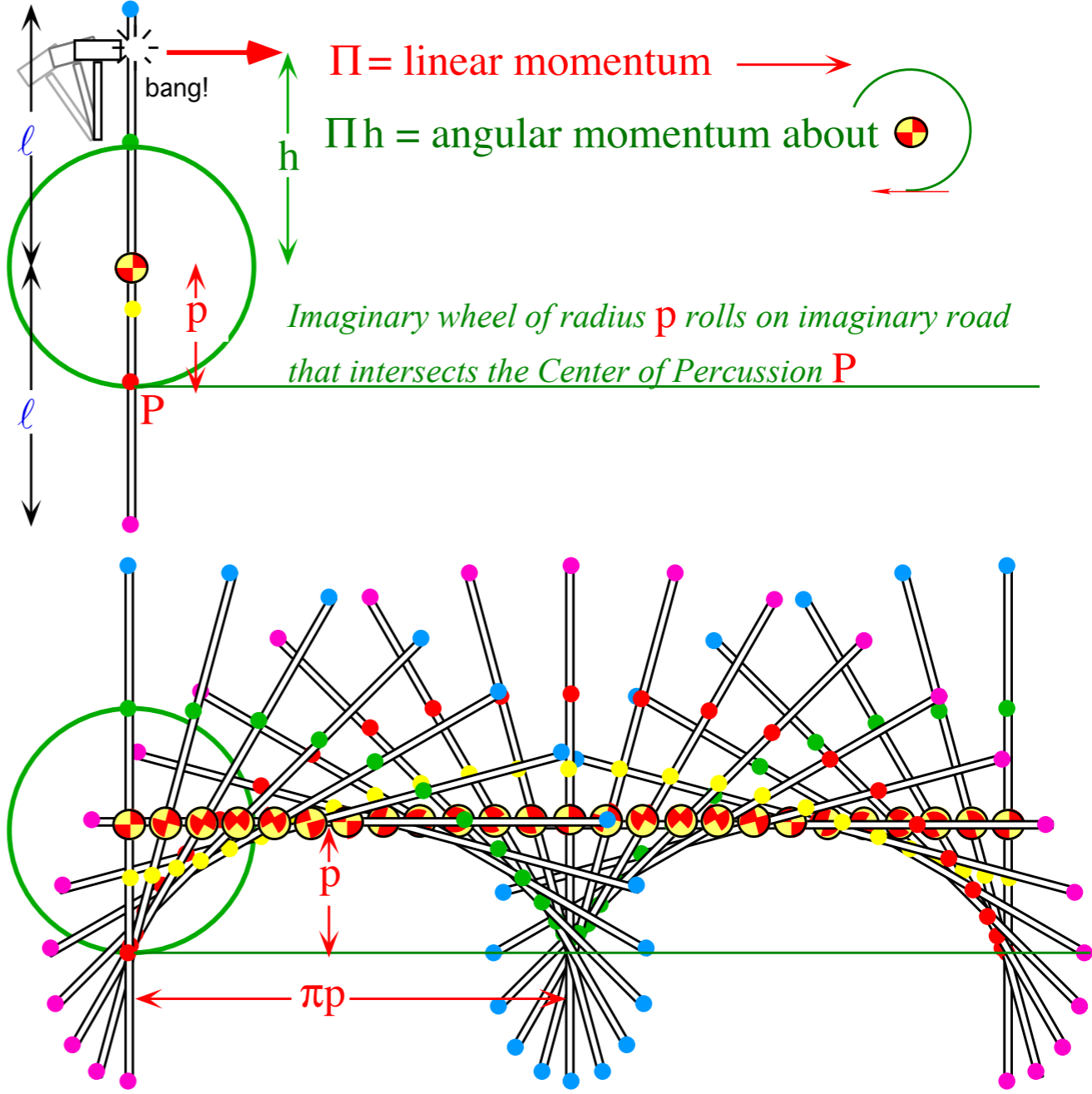


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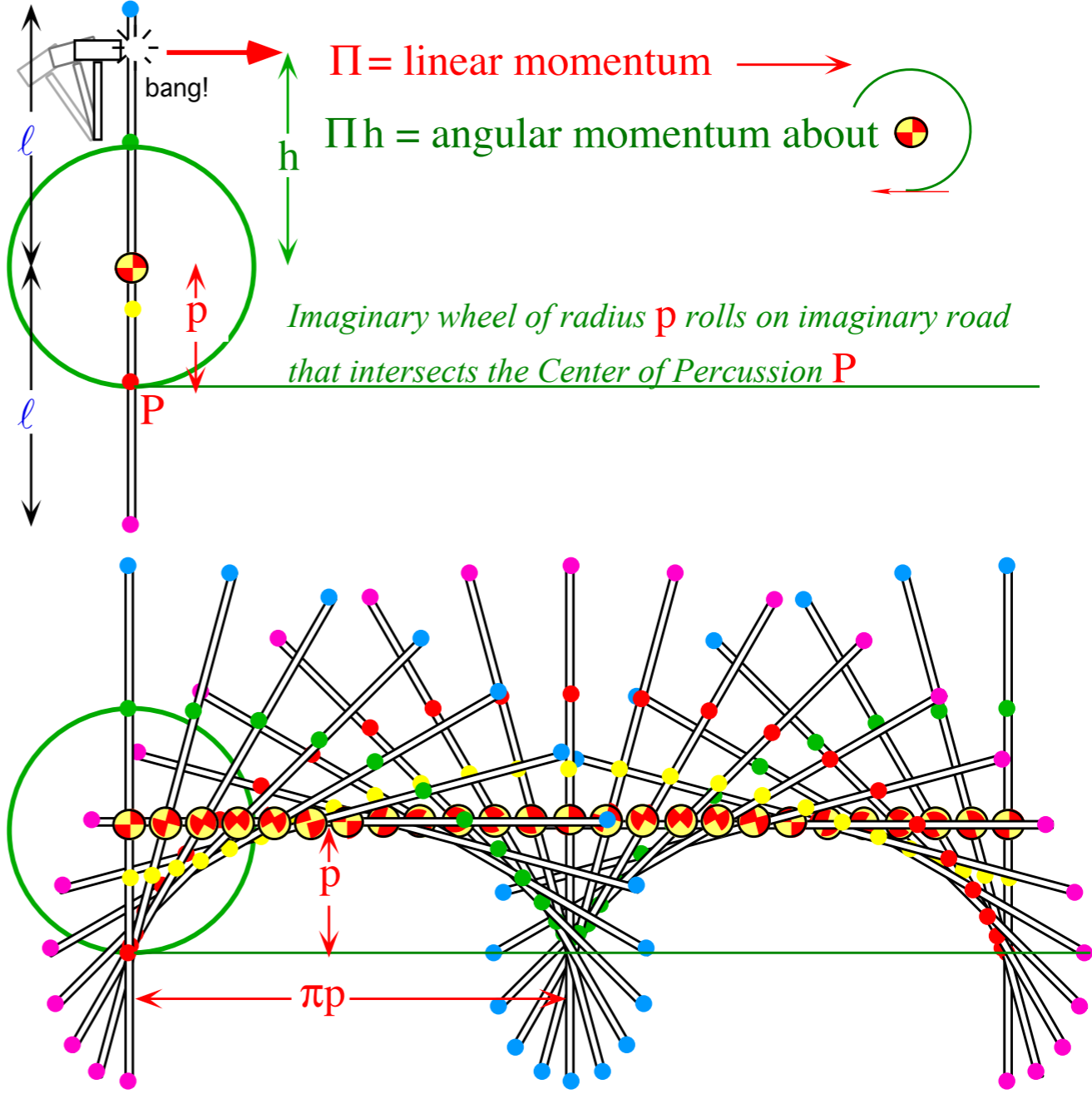


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$$I / M = \quad = \quad = p \cdot h \quad \text{or: } p = I / (Mh)$$

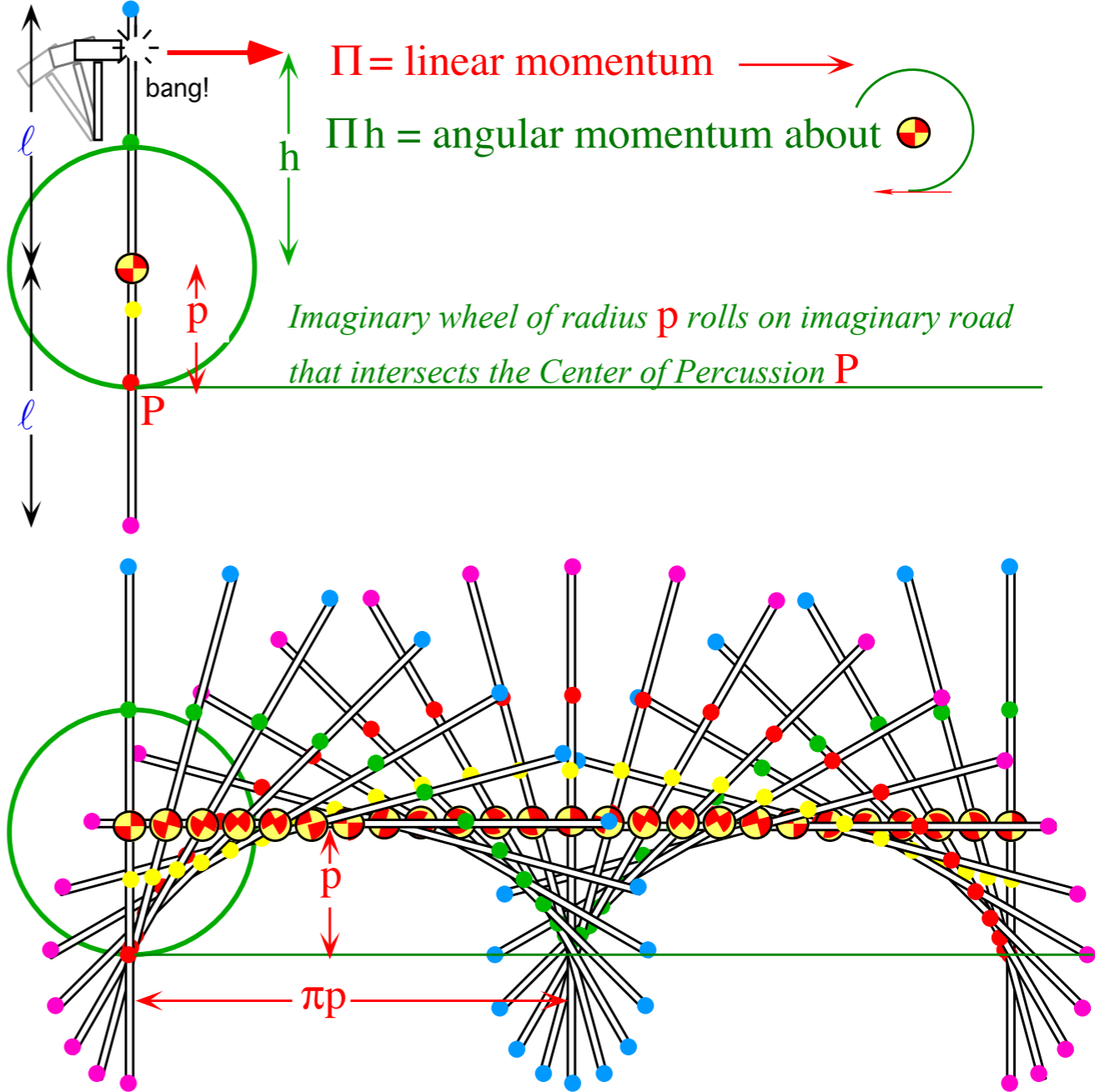


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P follows a normal cycloid made by a circle
 of radius $p = I / (Mh)$ rolling on an imaginary road
 thru point P in direction of Π .

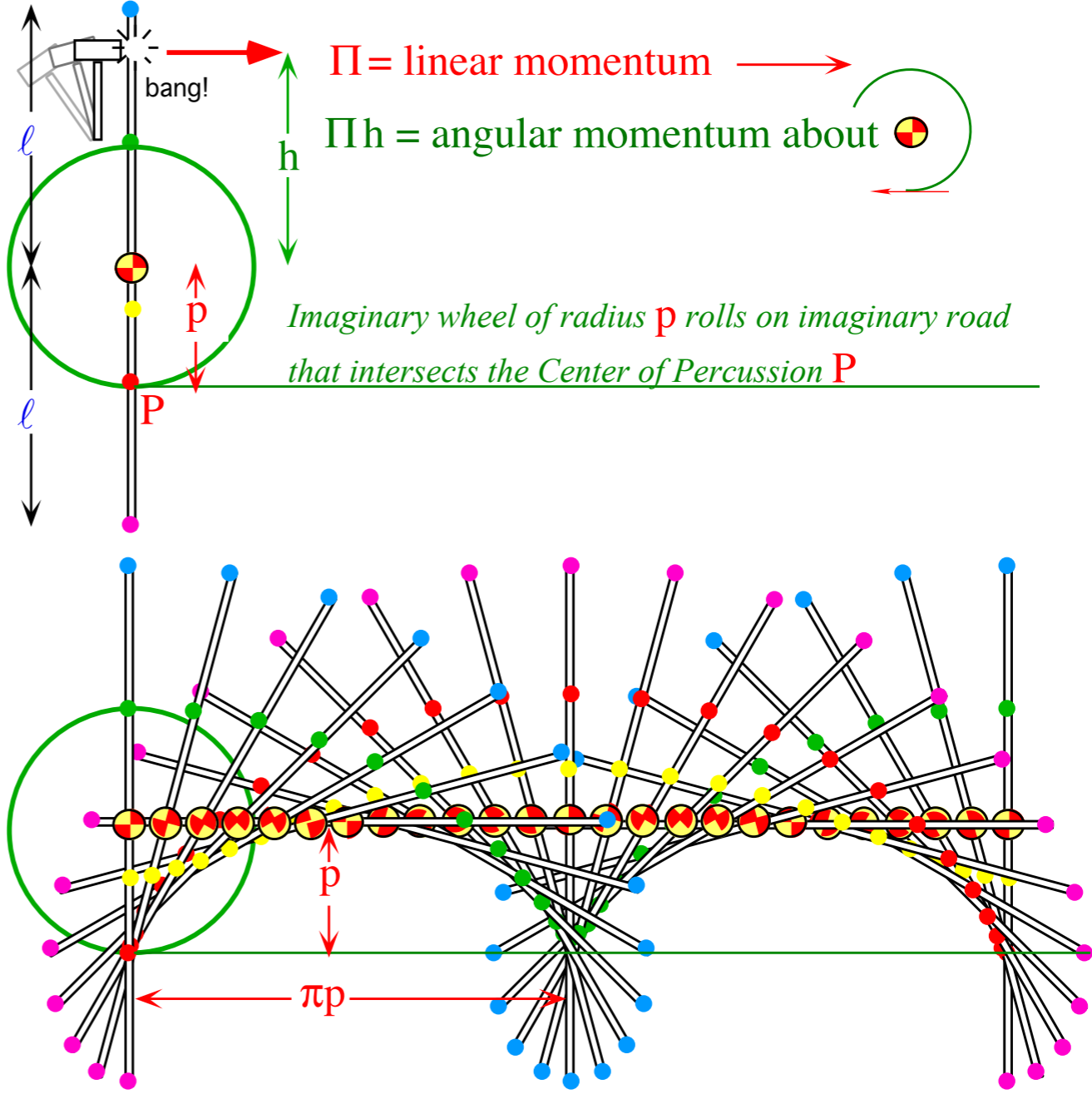


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P follows a normal cycloid made by a circle of radius $p = I / (Mh)$ rolling on an imaginary road thru point P in direction of Π .

The *percussion radius* $p = \ell^2/3h$ is of the **CoP** point that has no velocity just after hammer hits at h .

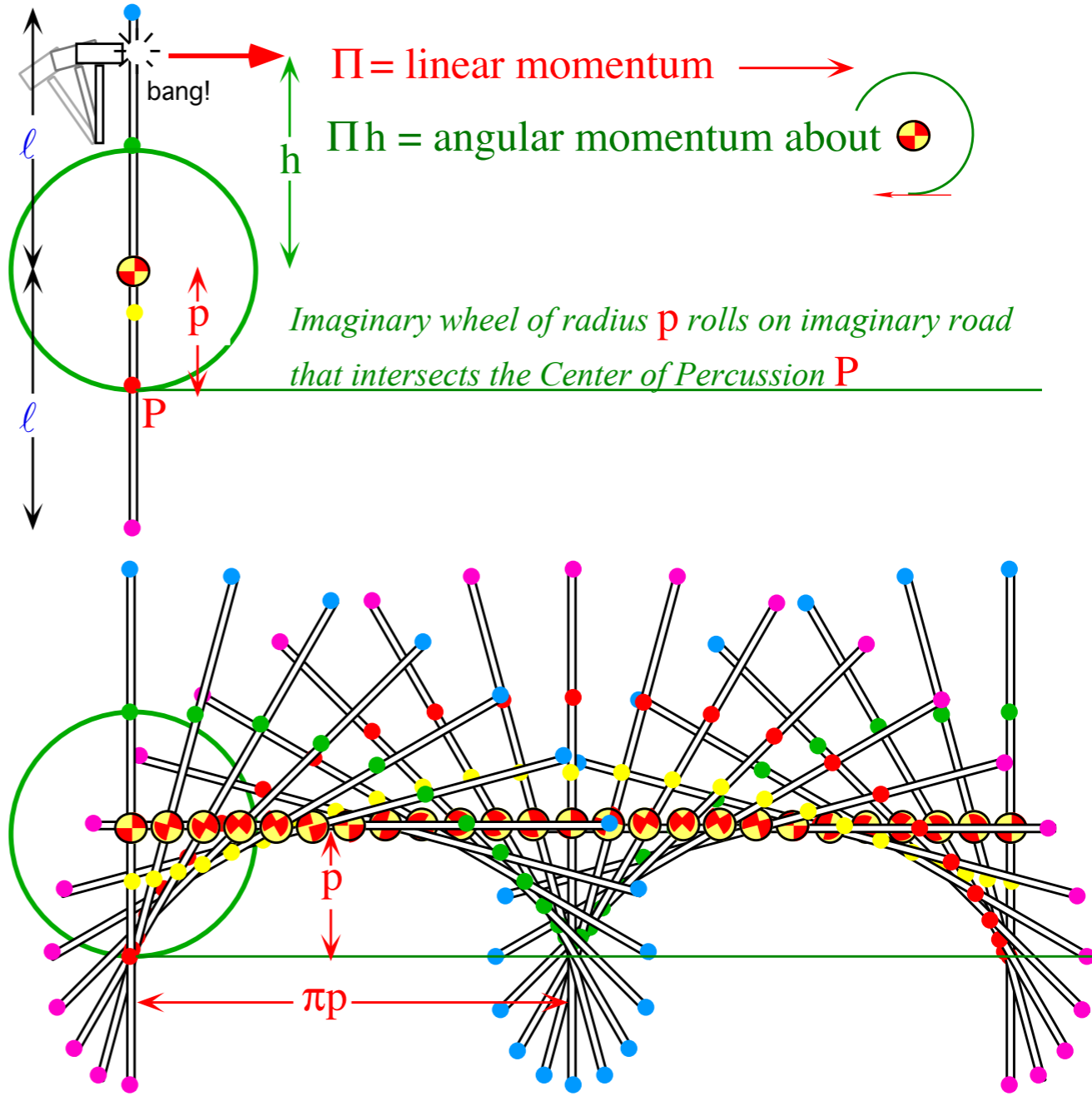


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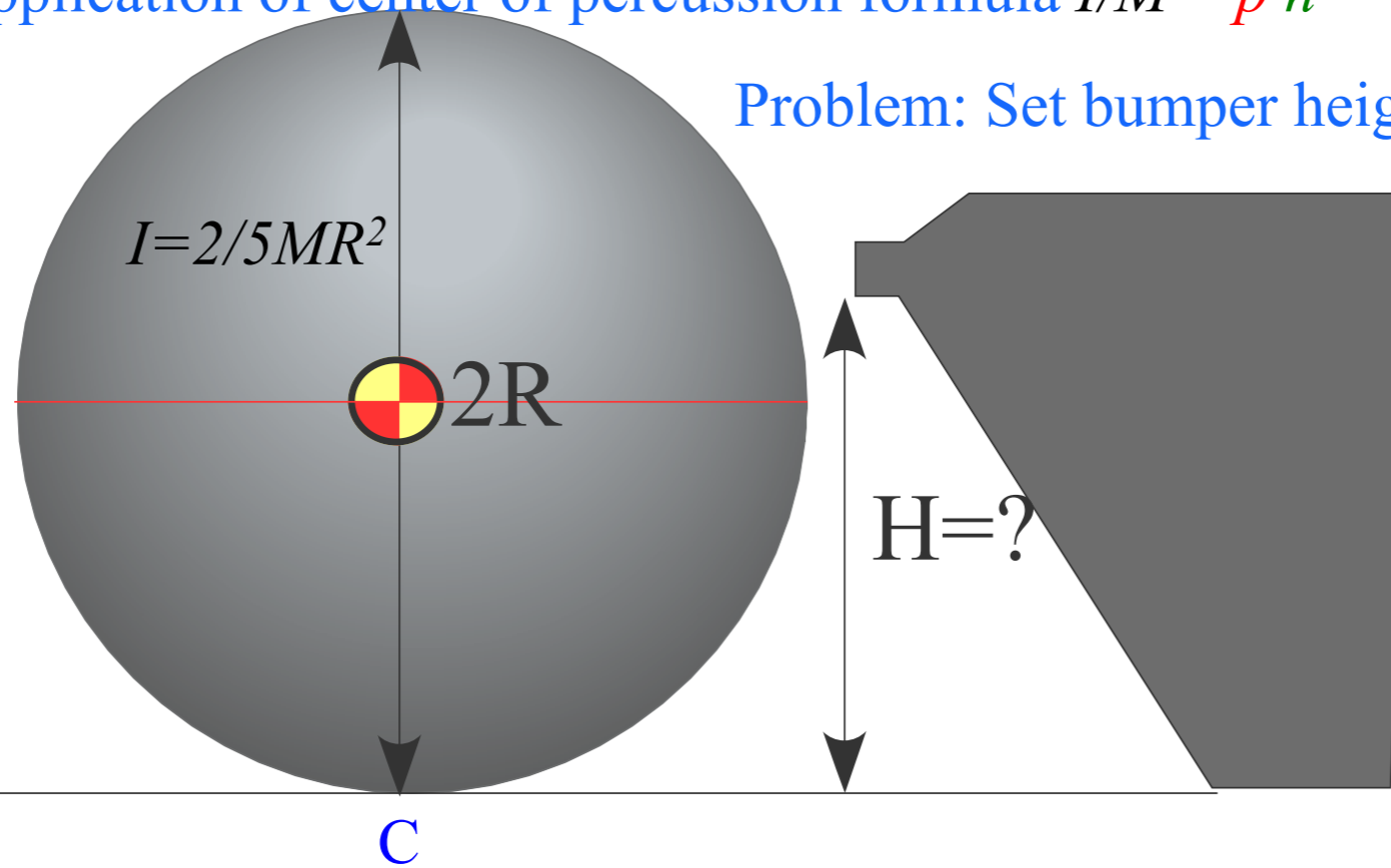
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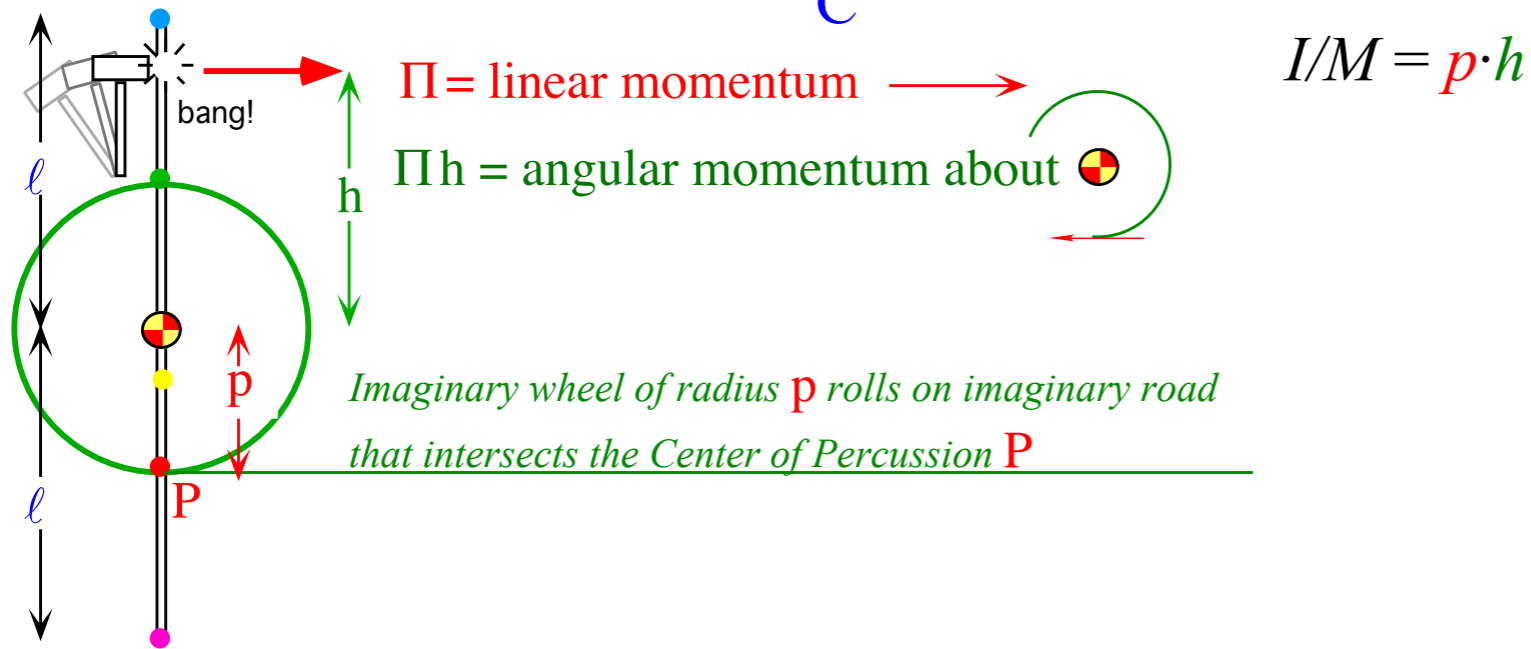
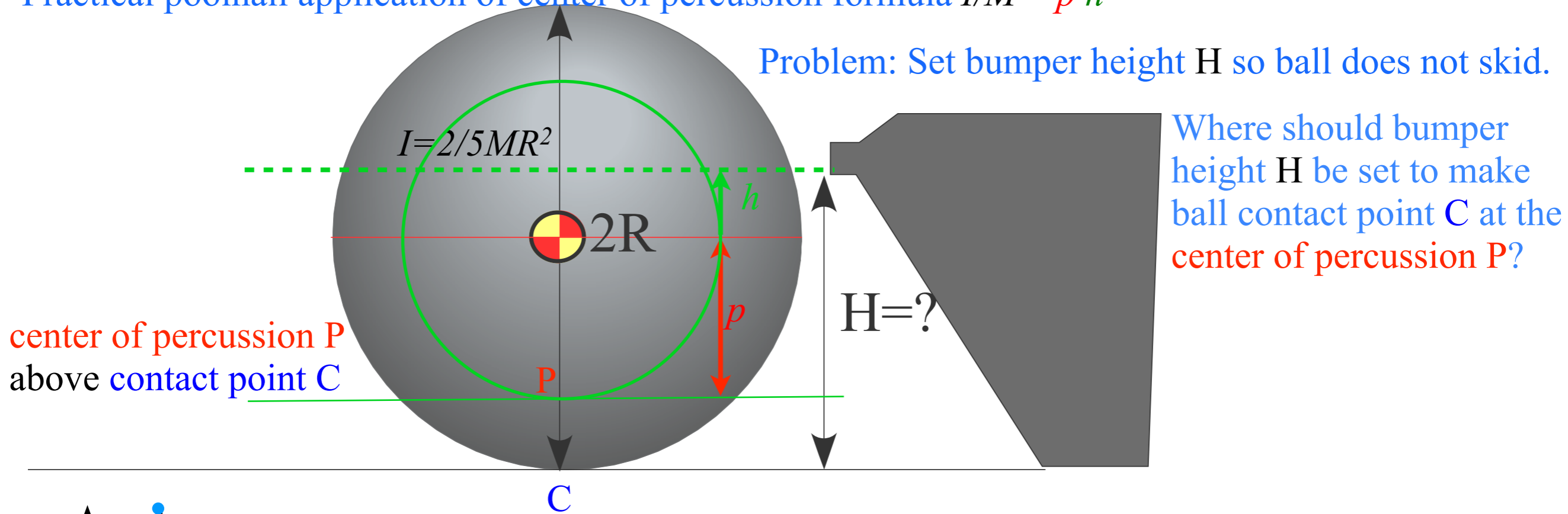
 *Practical poolhall application*

Practical poolhall application of center of percussion formula $I/M = p \cdot h$

Problem: Set bumper height H so ball does not skid.



Practical poolhall application of center of percussion formula $I/M = p \cdot h$

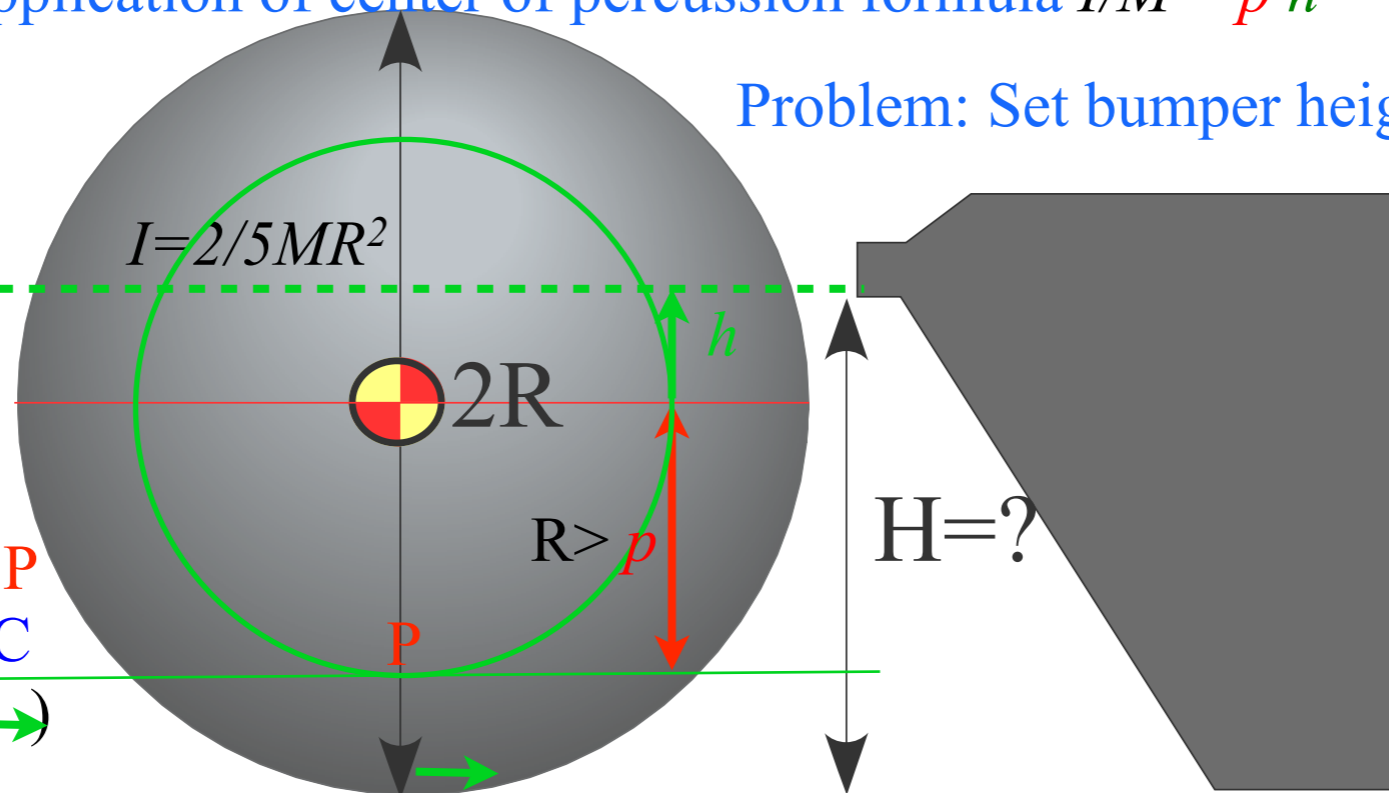


Practical poolhall application of center of percussion formula $I/M = p \cdot h$

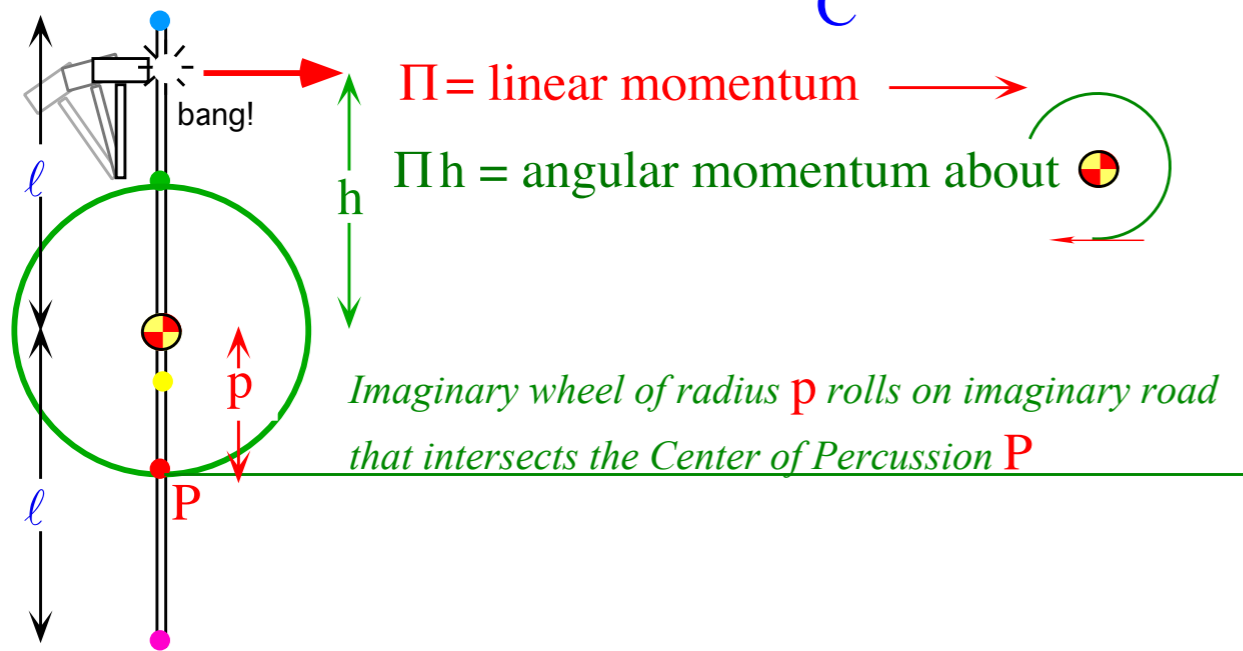
Problem: Set bumper height H so ball does not skid.

Where should bumper height H be set to make ball contact point C at the center of percussion P ?

center of percussion P
above contact point C
(Ball skids to right \rightarrow)



$$I/M = p \cdot h$$

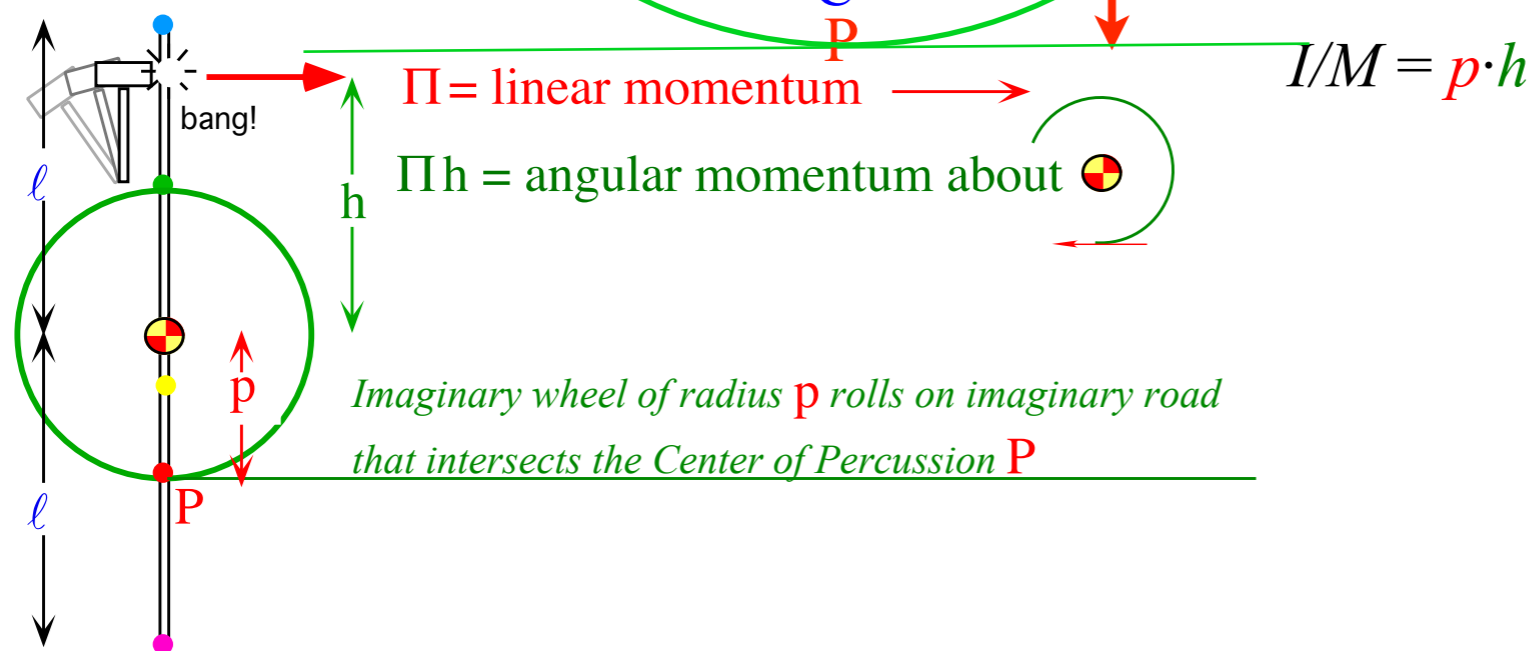
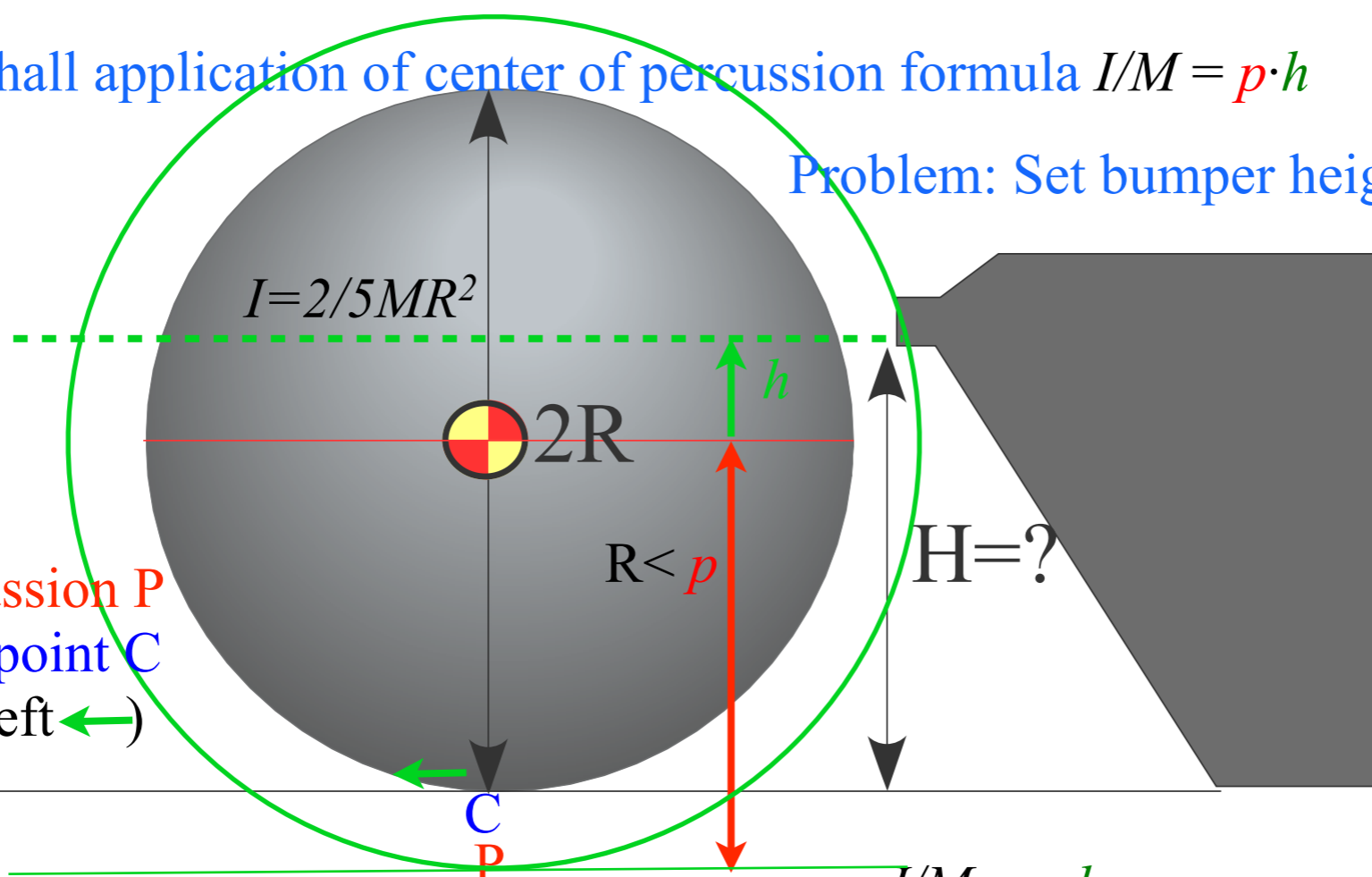


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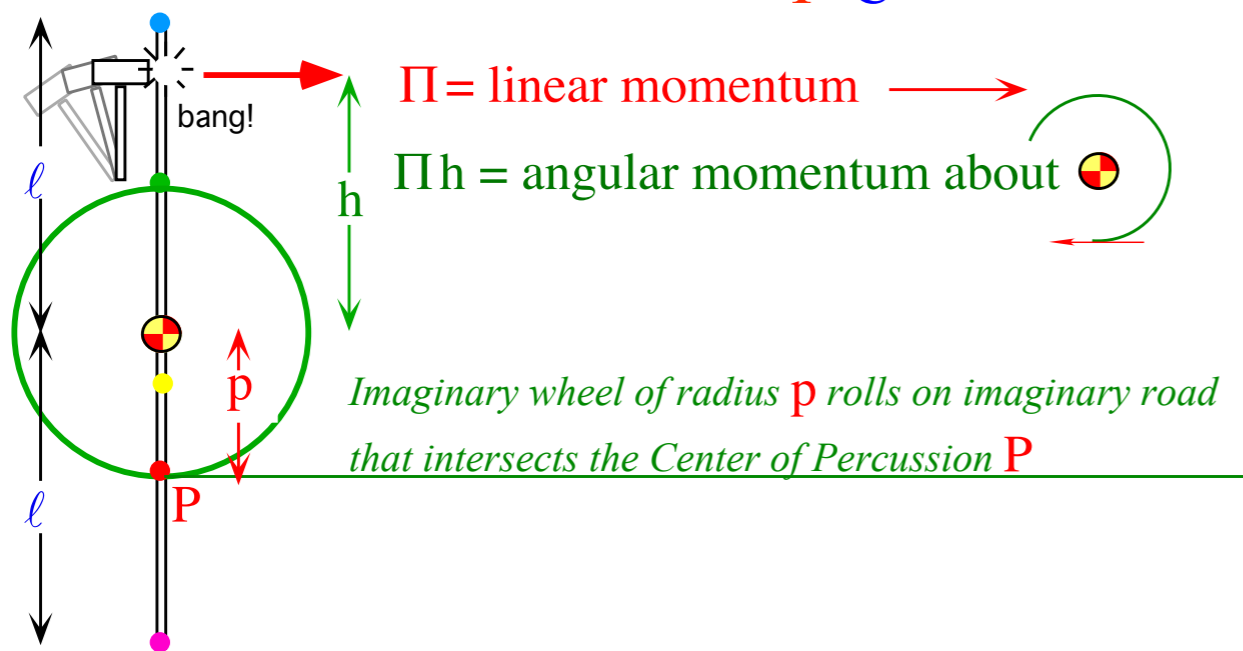
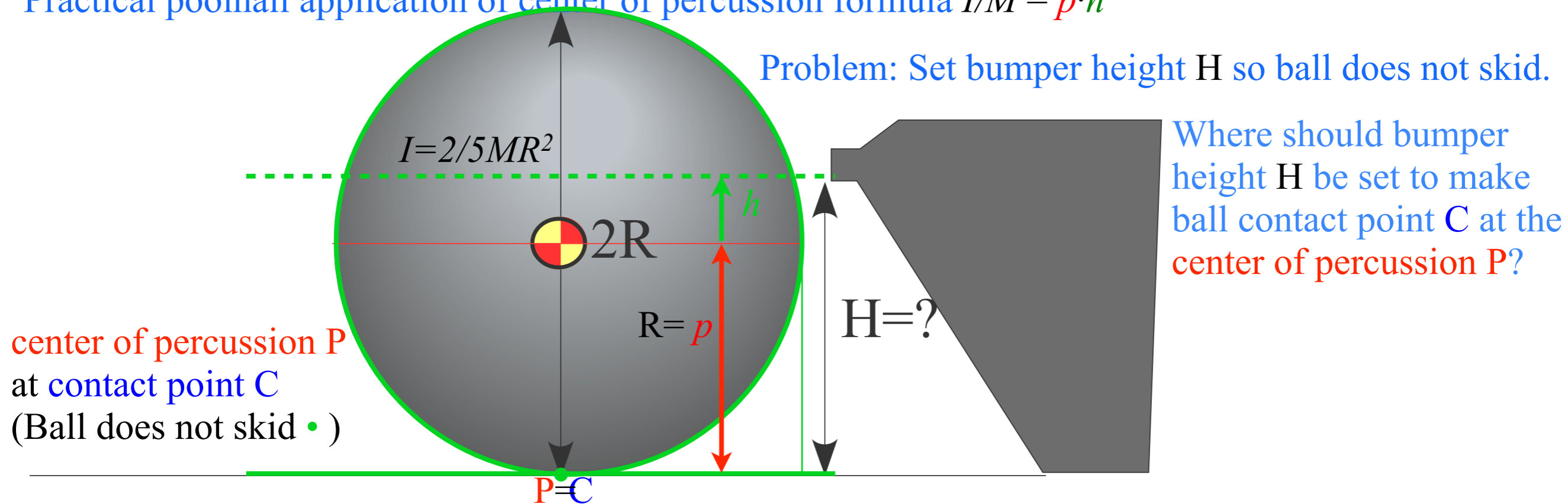
Problem: Set bumper height H so ball does not skid.

Where should bumper height H be set to make ball contact point C at the center of percussion P ?

center of percussion P
below contact point C
(Ball skids to left \leftarrow)



Practical poolhall application of center of percussion formula $I/M = p \cdot h$

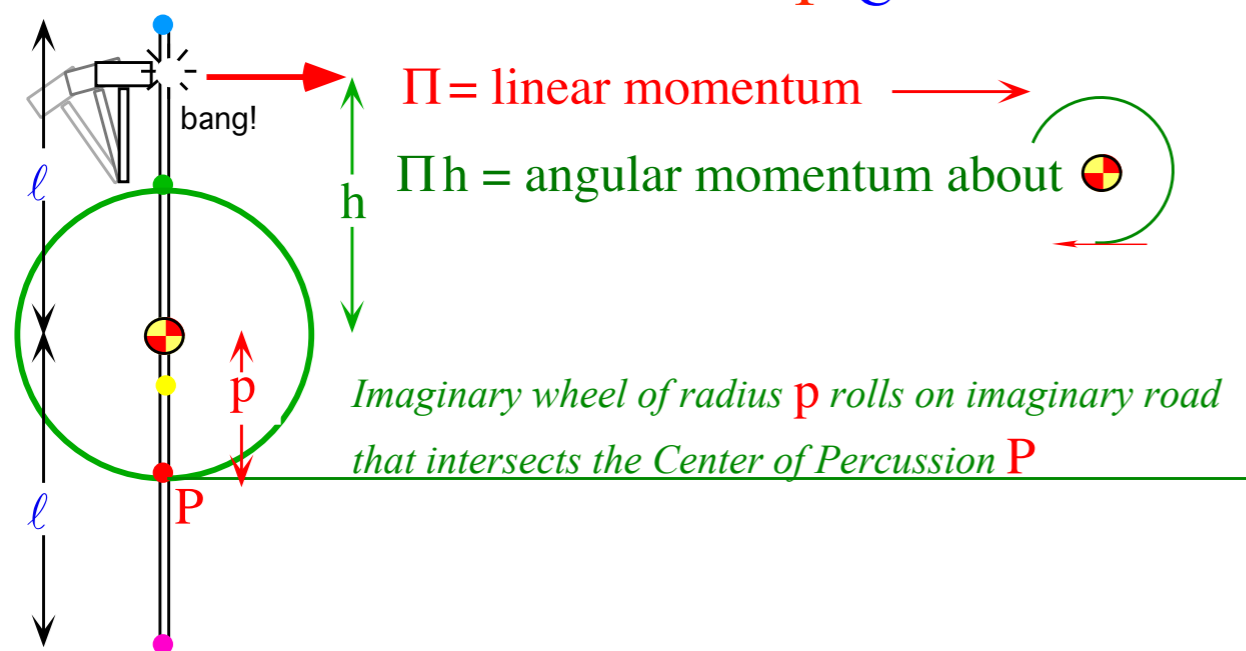
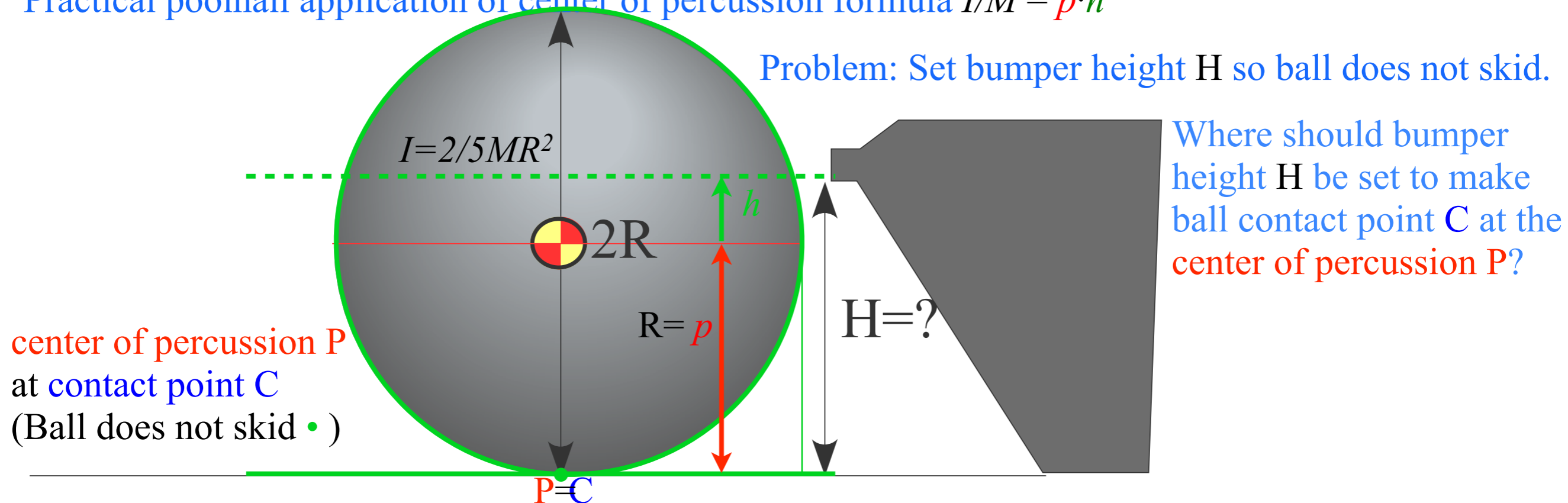


$$I/M = p \cdot h$$

$$h = I/Mp = I/MR$$

(For $R = p$)

Practical poolhall application of center of percussion formula $I/M = p \cdot h$



$$I/M = p \cdot h$$

$$h = I/Mp = I/MR \quad (\text{For } R = p)$$

$$= 2/5 MR^2 / MR$$

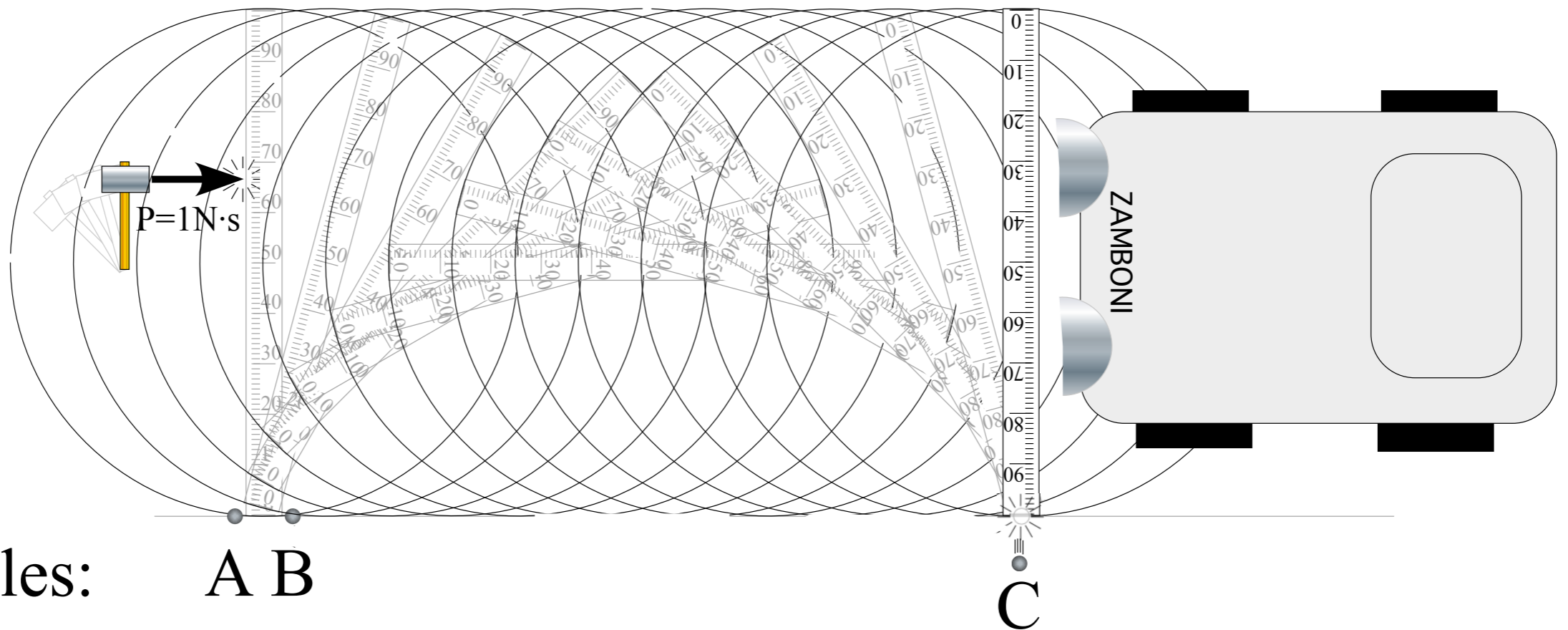
$$= 2/5 (R)$$

For: $H = R + h = 7/5 (R)$ ball does not skid.

$$= R + h = 7/10 (2R)$$

The Zamboni-Ice-Shot problem

(Assumes frictionless ice rink)



Marbles: A B

Where on a meter-stick do you hit it
so as to not disturb marbles A or B
and...

...knock marble C down as shown.