

Lecture 28.

Relativistic geometry of 2-and-3-dimensional waves

(Ch. 4-5 of Unit 2 4.09.12)

Plane wave 4-vector $(\omega_0, \omega_x, \omega_y, \omega_z)$ and space-time (x_0, x_1, x_2, x_3) geometry

Pattern recognition: “Occam’s Sword”

Reviewing the *stellar aberration angle* σ vs. *rapidity* ρ geometry

Reviewing “Sin-Tan Rosetta” geometry

Lorentz boost of *North-South-East-West* plane-wave 4-vectors $(\omega_0, \omega_x, \omega_y, \omega_z)$

Thales-like construction of Lorentz boost in 2D and 3D

The *spectral* ellipsoid

Combination and interference of 4-vector plane waves (Idealized polarization case)

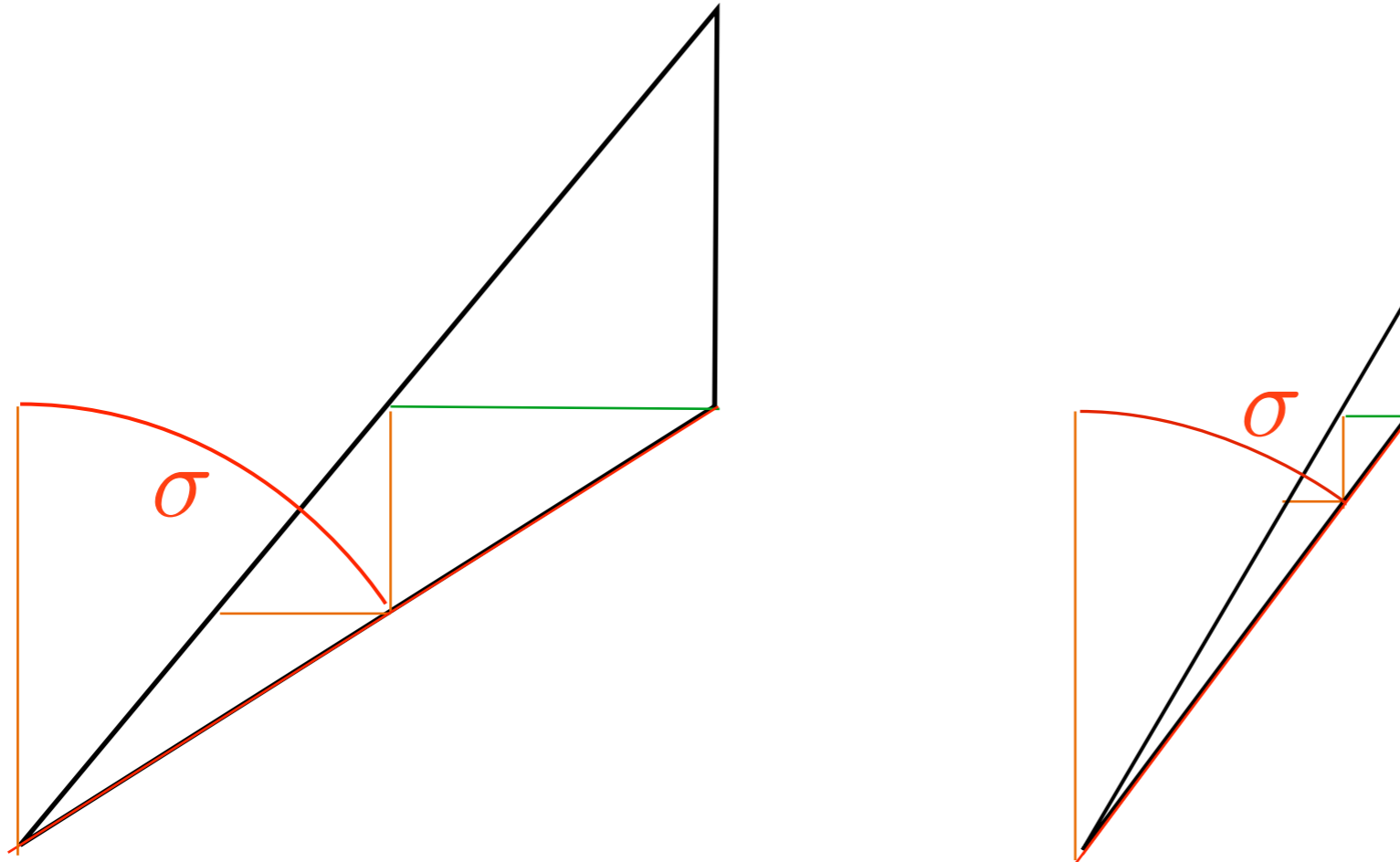
Combination *group* and phase waves define 4D Minkowski coordinates

Combination *group* and phase waves define wave guide dynamics

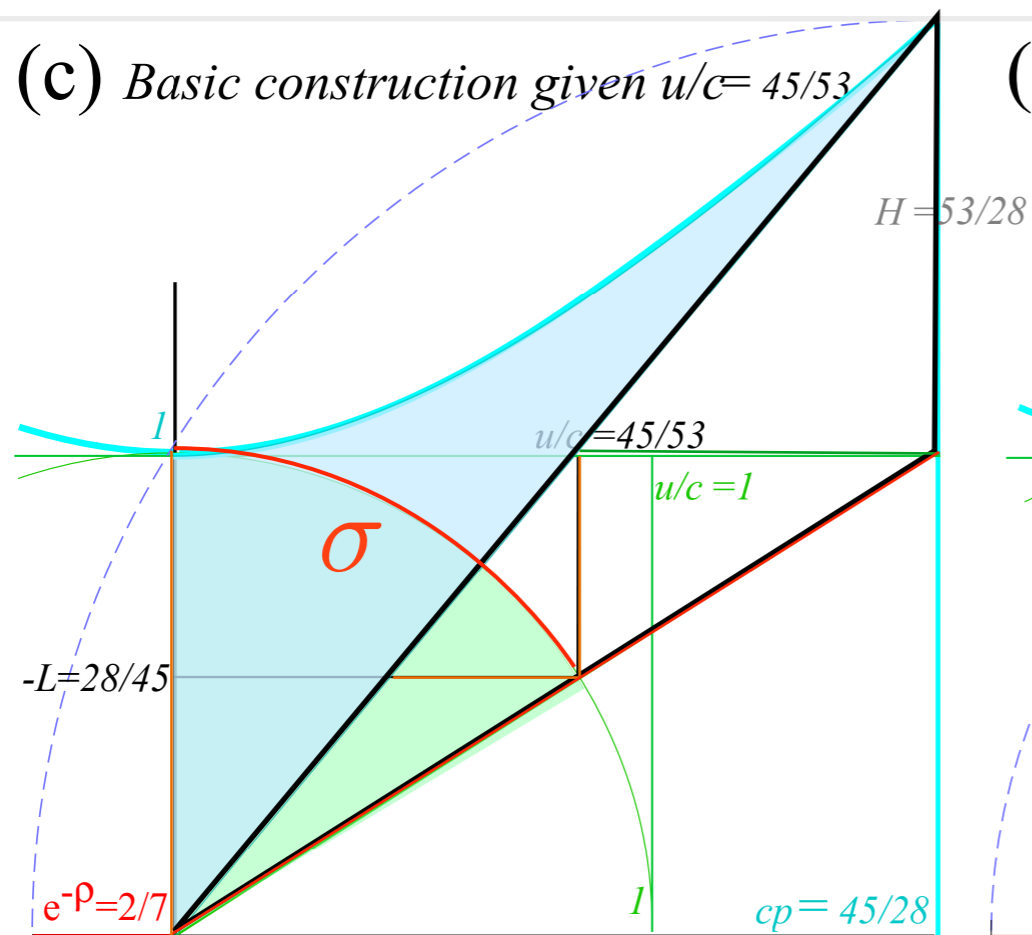
Waveguide dispersion and geometry

1st-quantized cavity modes

Pattern recognition: "Occam's Sword"



(c) Basic construction given $u/c = 45/53$



(d) $u/c = 3/5$

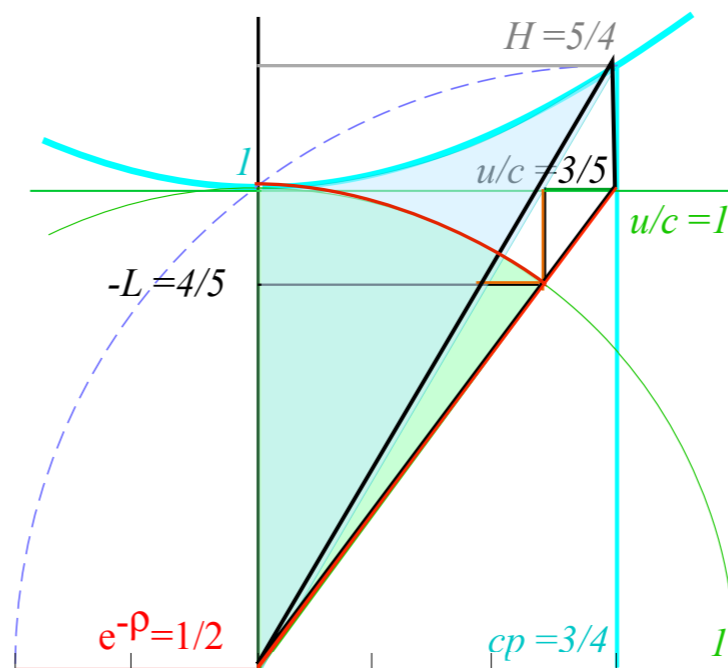


Fig. 5.5
Relativistic wave mechanics geometry.
(a) Overview.

(b-d) Details of contacting tangents.

(a) Geometry of relativistic transformation and wave based mechanics

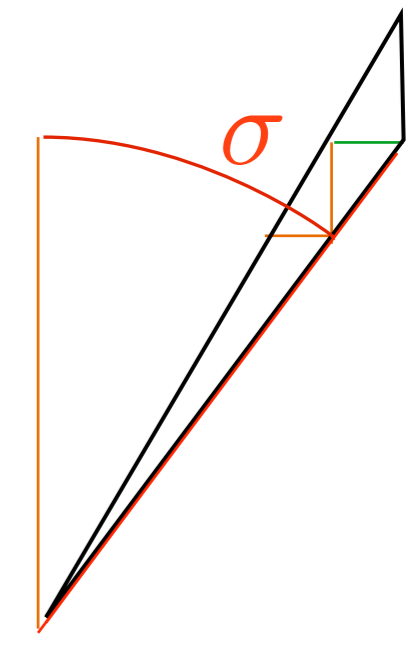
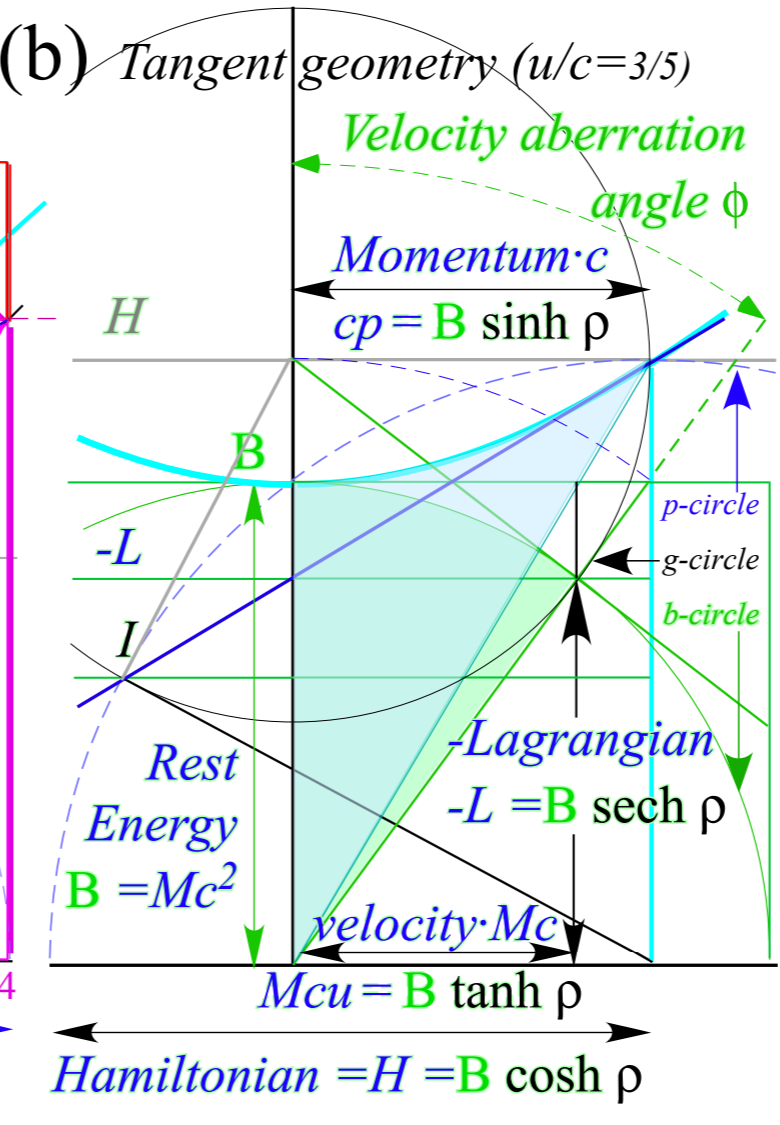
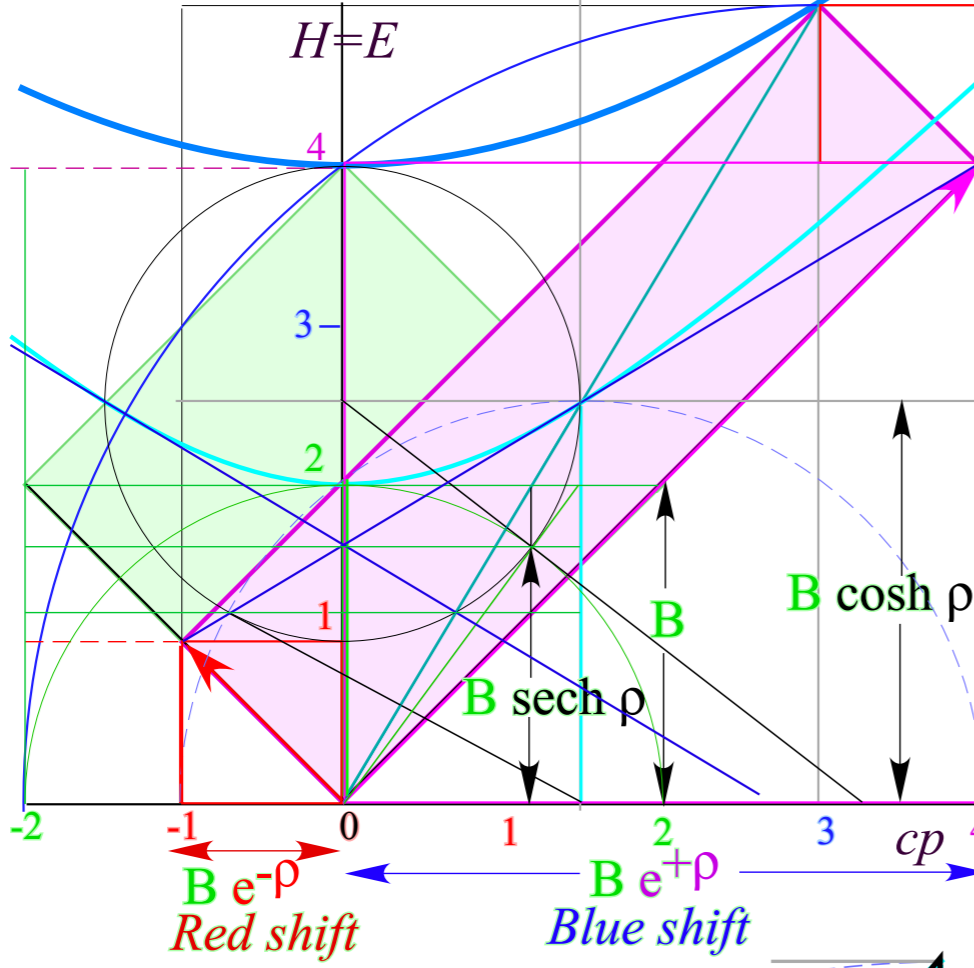
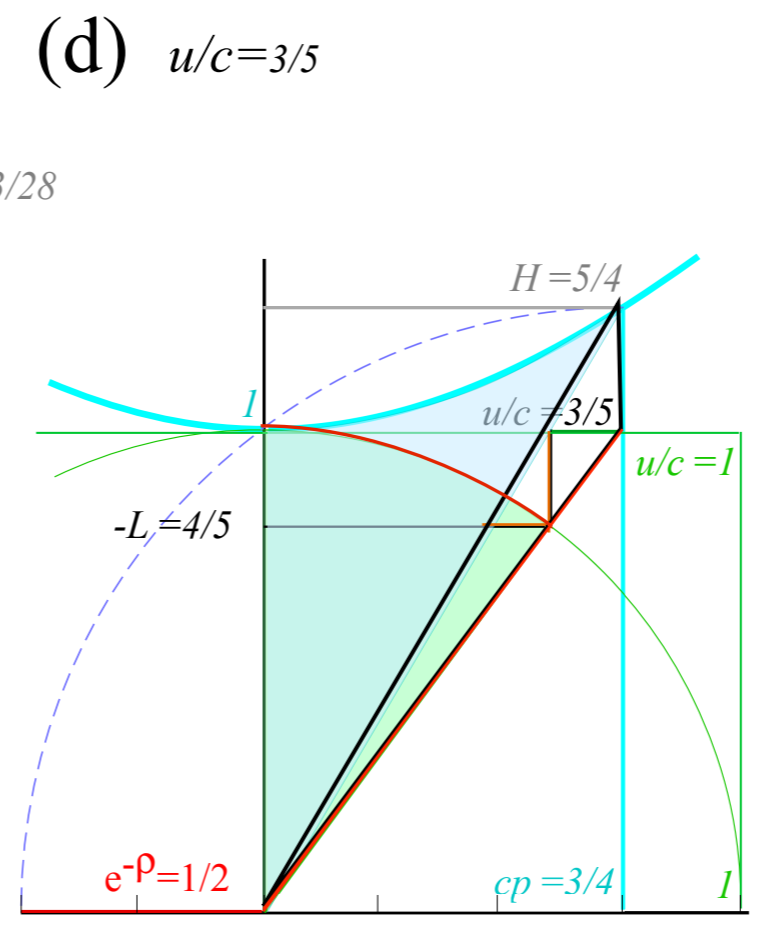
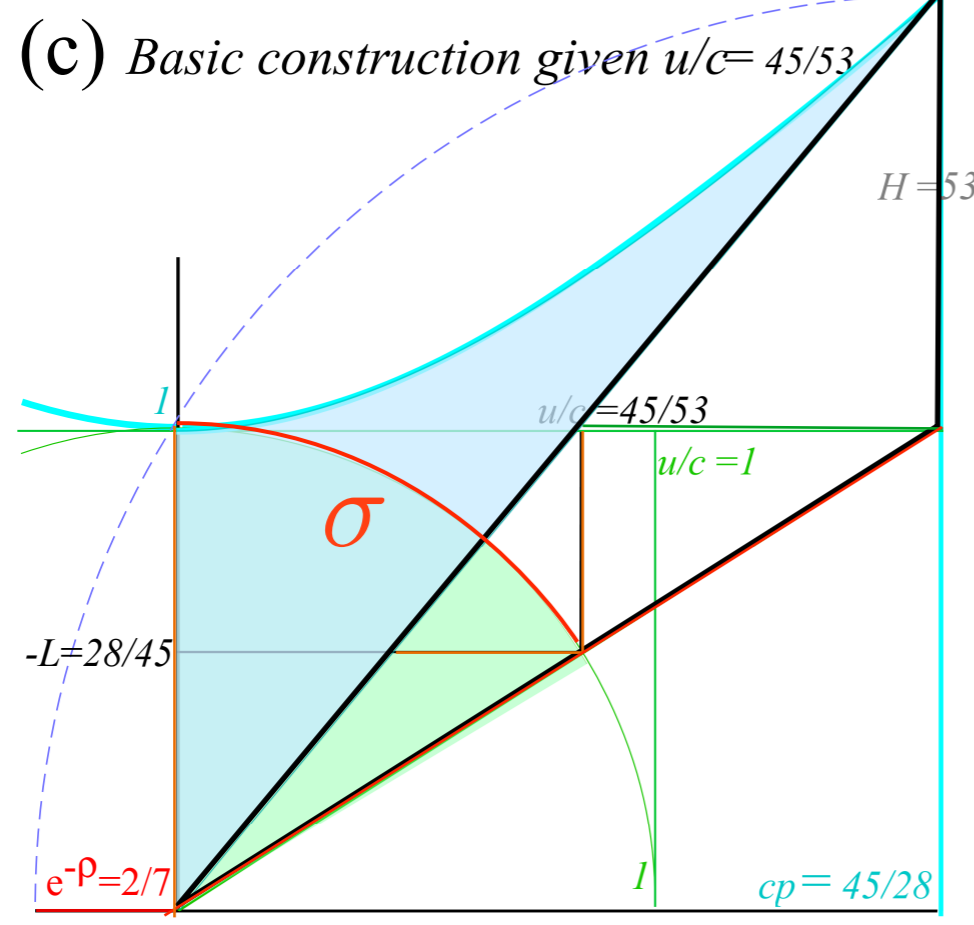


Fig. 5.5 Relativistic wave mechanics geometry. (a) Overview.



(b-d) Details of contacting tangents.

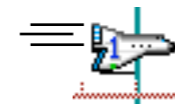
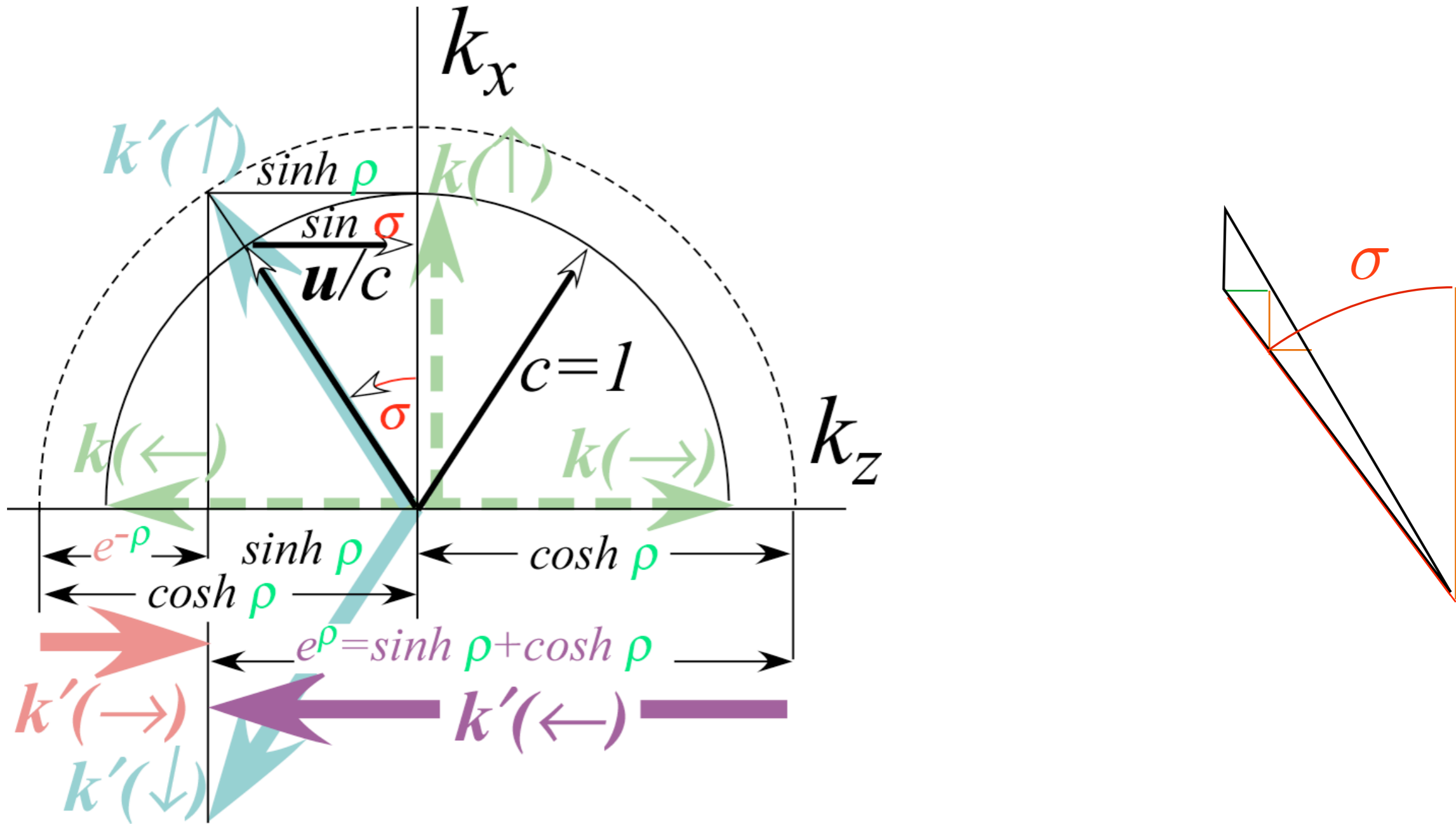


Fig. 5.10 CW cosmic speedometer.

Geometry of Lorentz boost of counter-propagating waves.



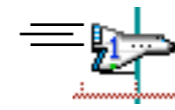
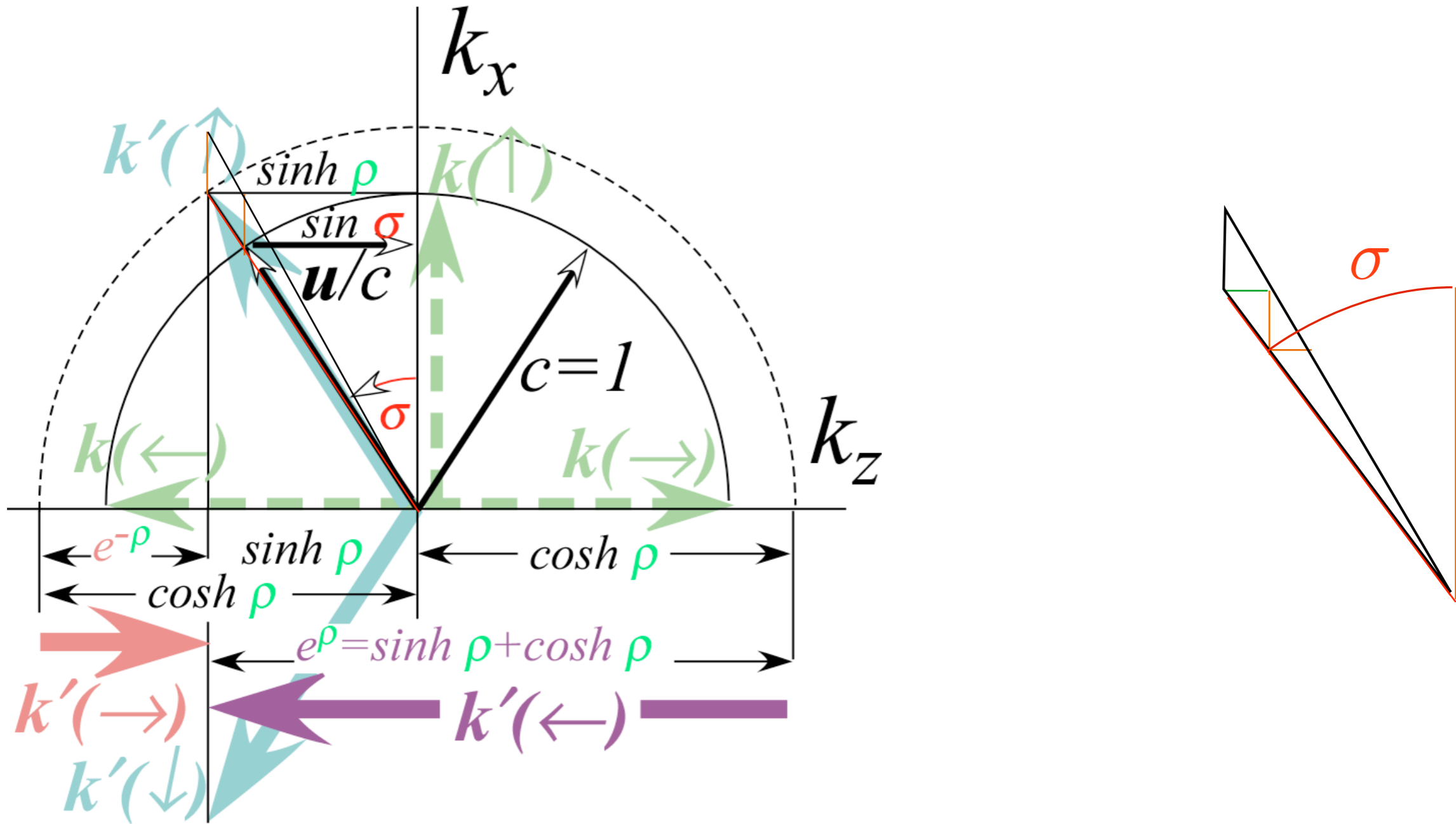
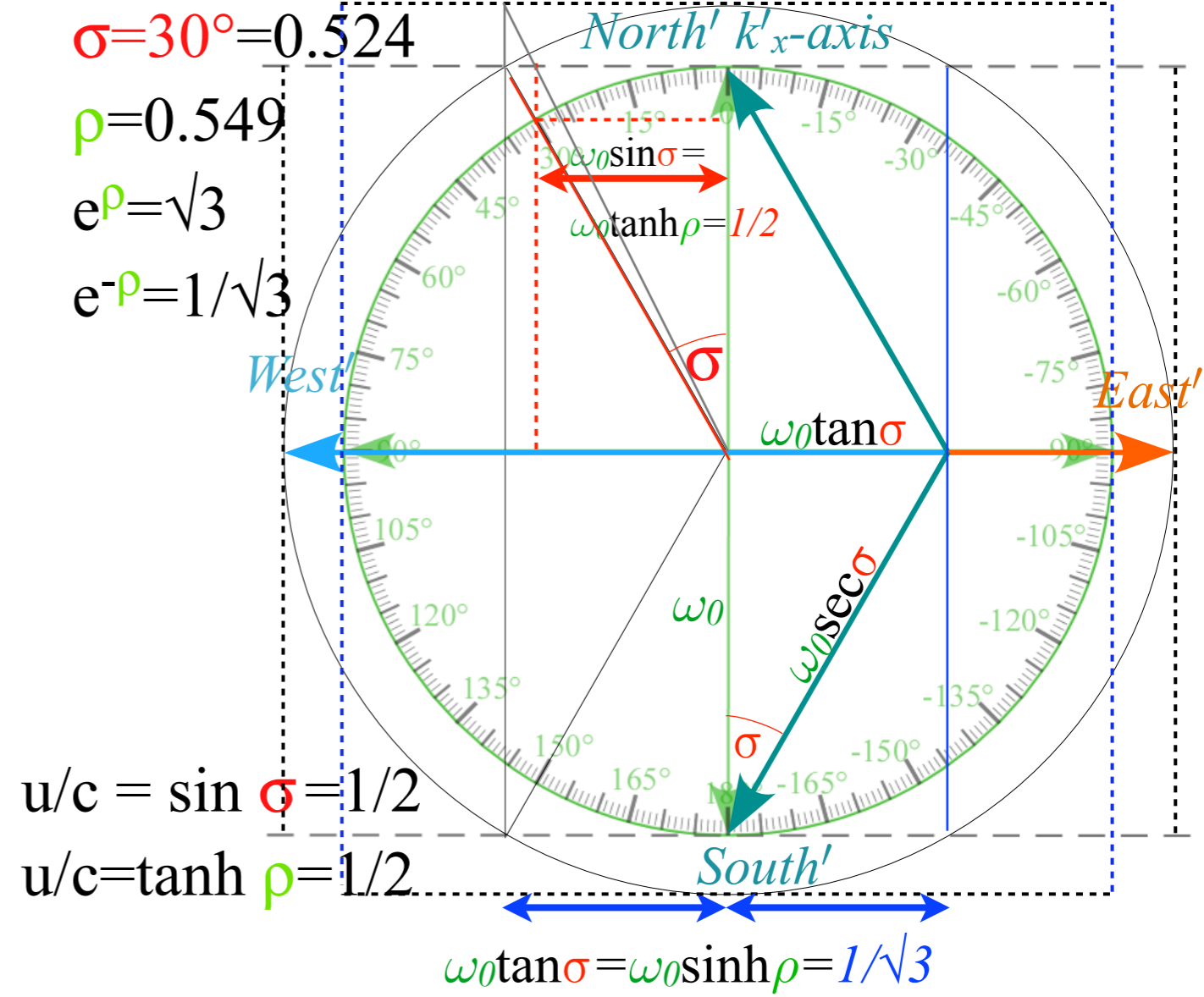
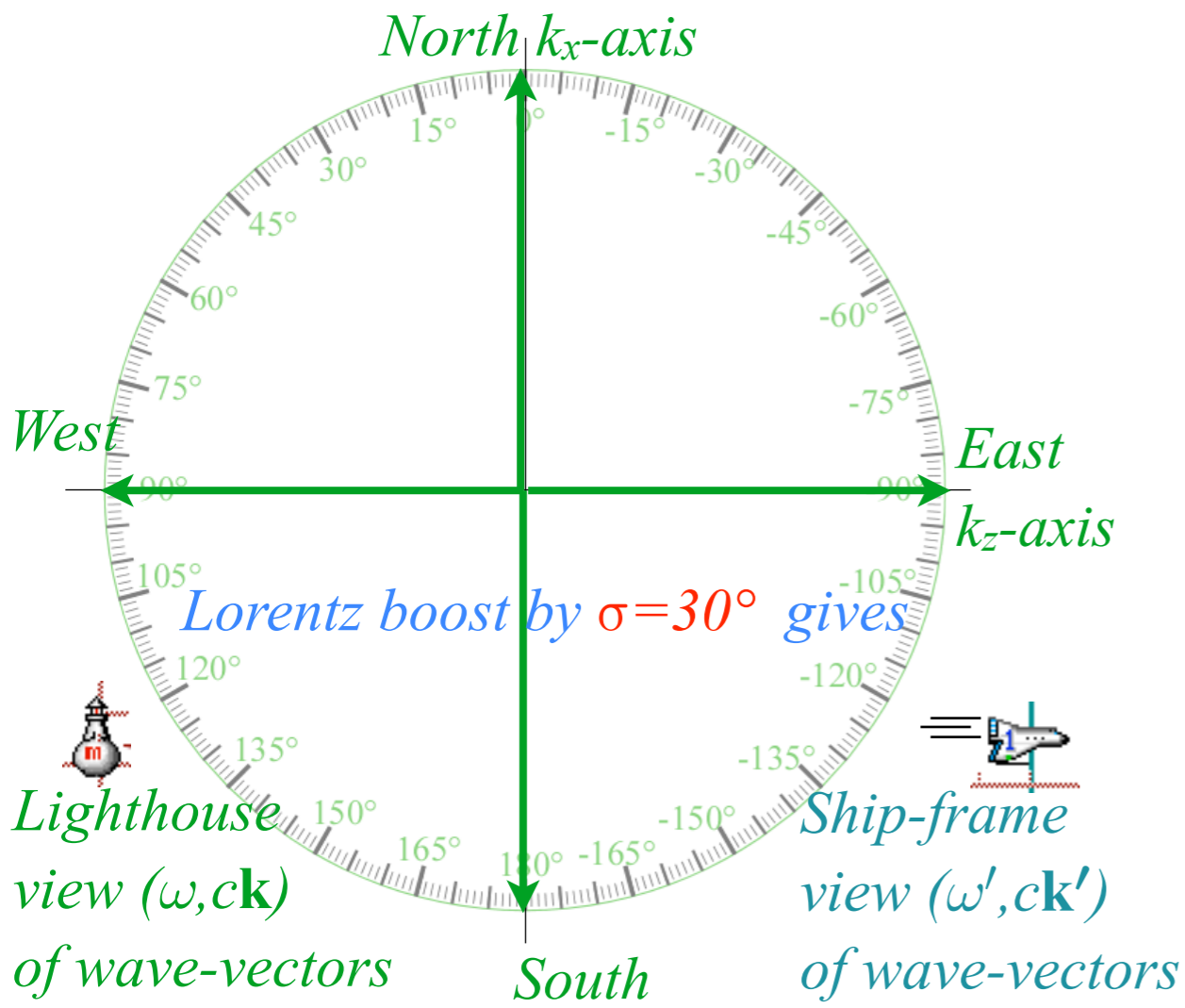


Fig. 5.10 CW cosmic speedometer.

Geometry of Lorentz boost of counter-propagating waves.



Lecture 27 discusses Lorentz boost of North-South-East-West plane-wave 4-vectors $(\omega_0, \omega_x, \omega_y, \omega_z)$

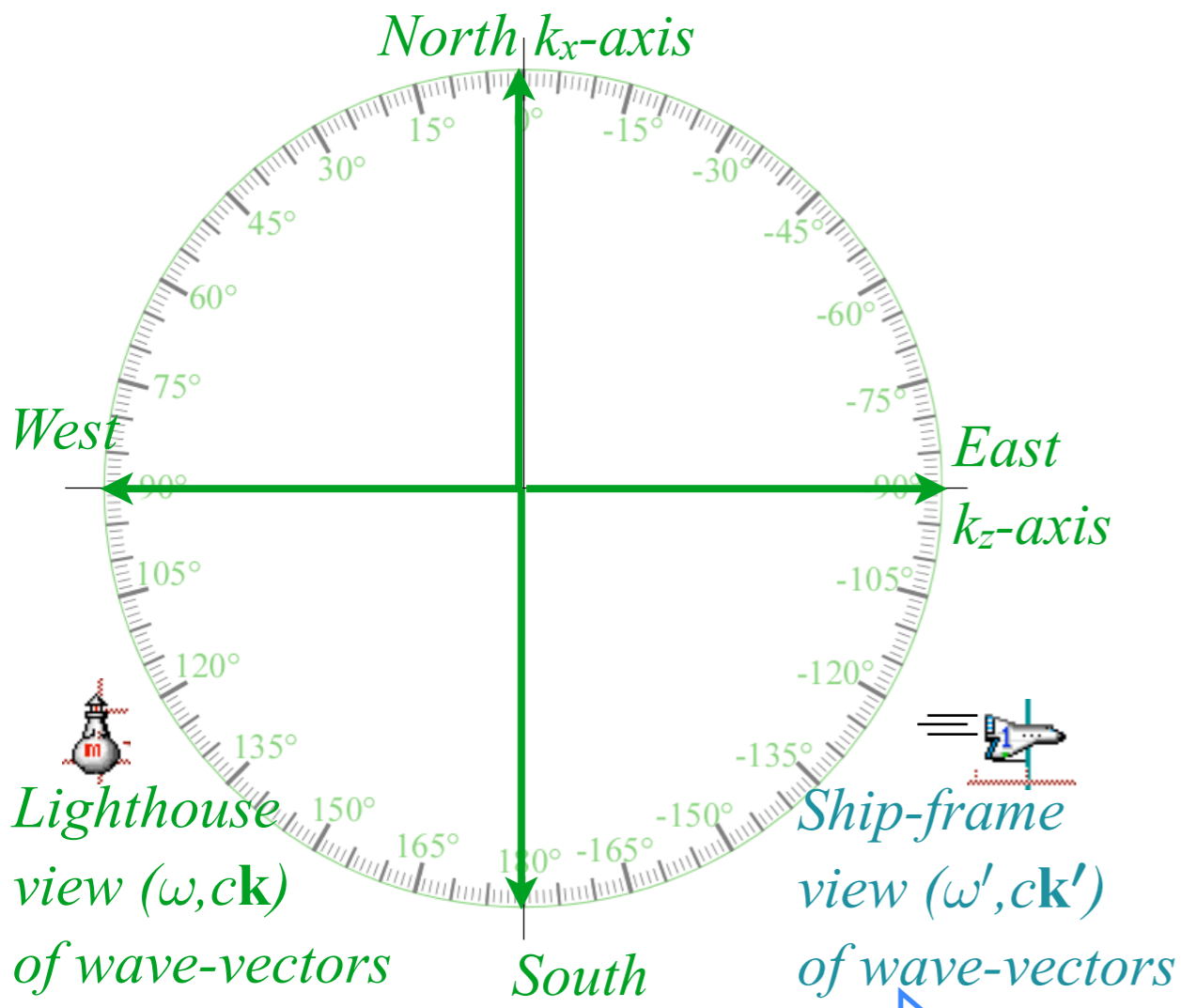


South starlight in lighthouse frame is straight down x-axis : $(\omega_{\downarrow}, ck_{x\downarrow}, ck_{y\downarrow}, ck_{z\downarrow}) = (\omega_0, -\omega_0, 0, 0)$

+ ρ_z -rapidity ship frame sees starlight Lorentz transformed to : $(\omega'_{\downarrow}, ck'_{x\downarrow}, ck'_{y\downarrow}, ck'_{z\downarrow}) = (\omega_0 \cosh \rho_z, -\omega_0, 0, -\omega_0 \sinh \rho_z)$

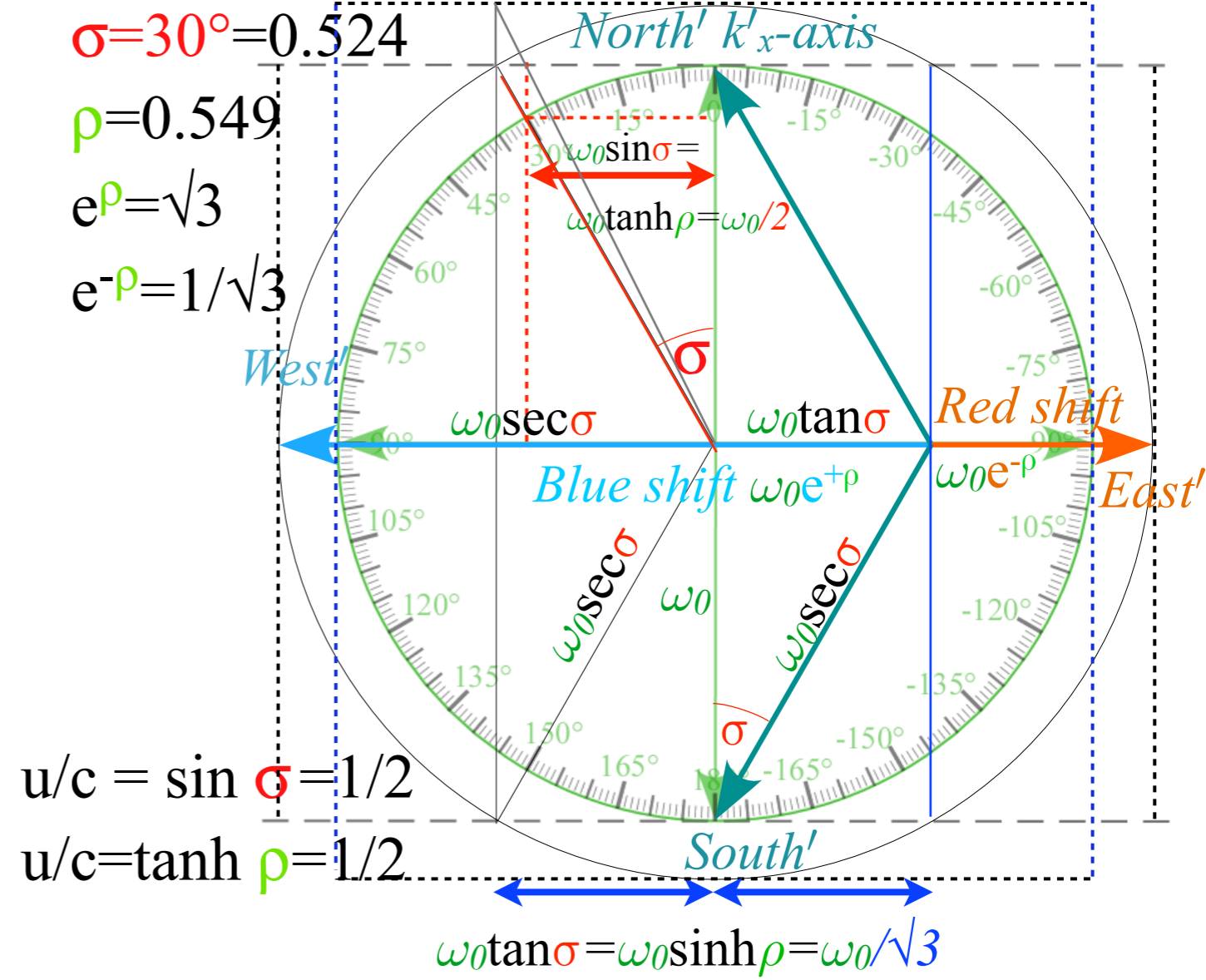
$$\begin{pmatrix} \omega'_{\downarrow} \\ ck'_{x\downarrow} \\ ck'_{y\downarrow} \\ ck'_{z\downarrow} \end{pmatrix} = \begin{pmatrix} \cosh \rho_z & \cdot & \cdot & -\sinh \rho_z \\ \cdot & 1 & \cdot & \cdot \\ \cdot & \cdot & 1 & \cdot \\ -\sinh \rho_z & \cdot & \cdot & \cosh \rho_z \end{pmatrix} \begin{pmatrix} \omega_{\downarrow} \\ ck_{x\downarrow} \\ ck_{y\downarrow} \\ ck_{z\downarrow} \end{pmatrix} = \begin{pmatrix} \cosh \rho_z & \cdot & \cdot & -\sinh \rho_z \\ \cdot & 1 & \cdot & \cdot \\ \cdot & \cdot & 1 & \cdot \\ -\sinh \rho_z & \cdot & \cdot & \cosh \rho_z \end{pmatrix} \begin{pmatrix} \omega_0 \\ -\omega_0 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} \omega_0 \cosh \rho_z \\ -\omega_0 \\ 0 \\ -\omega_0 \sinh \rho_z \end{pmatrix} = \begin{pmatrix} \omega_0 \sec \sigma \\ -\omega_0 \\ 0 \\ -\omega_0 \tan \sigma \end{pmatrix}$$

Lecture 27 discusses Lorentz boost of North-South-East-West plane-wave 4-vectors $(\omega_0, \omega_x, \omega_y, \omega_z)$



Lorentz boost by $\sigma=30^\circ$ or $e^{+\rho} = \sqrt{3}$

For ship going $u=c \tanh \rho$ along z-axis



West starlight $(\omega_0, 0, 0, -\omega_0)$ is blue shifted by $e^{+\rho} = \cosh \rho + \sinh \rho$

$$\begin{pmatrix} \omega'_{\leftarrow} \\ ck'_{x\leftarrow} \\ ck'_{y\leftarrow} \\ ck'_{z\leftarrow} \end{pmatrix} = \omega_0 \begin{pmatrix} \cosh \rho_z + \sinh \rho_z & & & \\ & 0 & & \\ & 0 & & \\ -\sinh \rho_z - \cosh \rho_z & & & \end{pmatrix} = \begin{pmatrix} \omega_0 e^{+\rho_z} \\ 0 \\ 0 \\ -\omega_0 e^{+\rho_z} \end{pmatrix}$$

and East starlight $(\omega_0, 0, 0, +\omega_0)$ is red shifted by $e^{-\rho} = \cosh \rho - \sinh \rho$

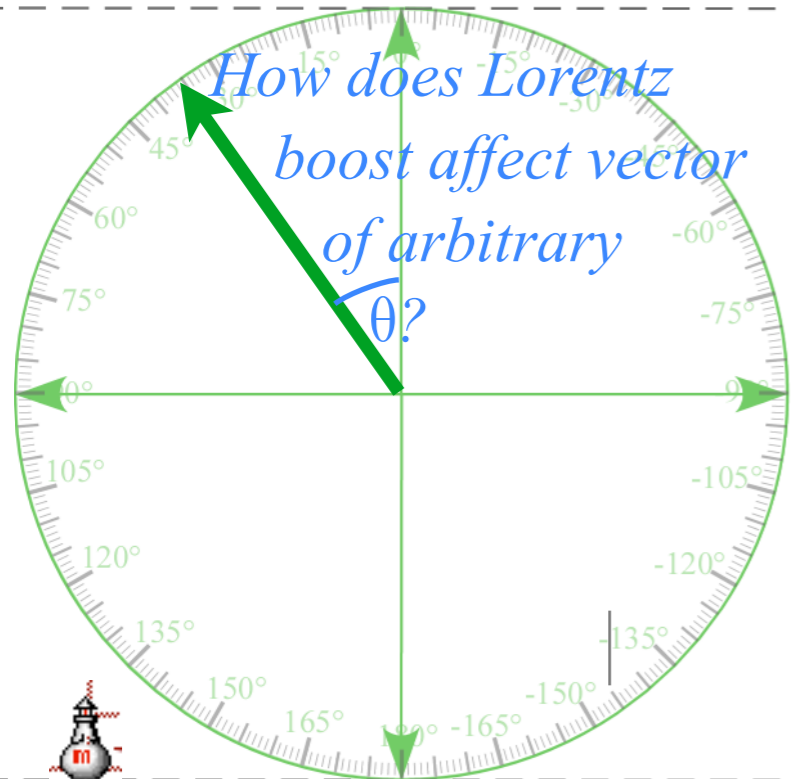
$$\begin{pmatrix} \omega'_{\rightarrow} \\ ck'_{x\rightarrow} \\ ck'_{y\rightarrow} \\ ck'_{z\rightarrow} \end{pmatrix} = \omega_0 \begin{pmatrix} \cosh \rho_z - \sinh \rho_z & & & \\ & 0 & & \\ & 0 & & \\ -\sinh \rho_z + \cosh \rho_z & & & \end{pmatrix} = \begin{pmatrix} \omega_0 e^{-\rho_z} \\ 0 \\ 0 \\ -\omega_0 e^{-\rho_z} \end{pmatrix}$$

Blue shift factor is $e^{+\rho} = \cosh \rho + \sinh \rho = \sec \sigma + \tan \sigma$

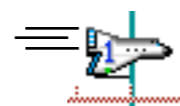
Red shift factor is $e^{-\rho} = \cosh \rho - \sinh \rho = \sec \sigma - \tan \sigma$

*Faster Lorentz boost of
North-South-East-West
plane-wave 4-vectors $(\omega_0, \omega_x, \omega_y, \omega_z)$*

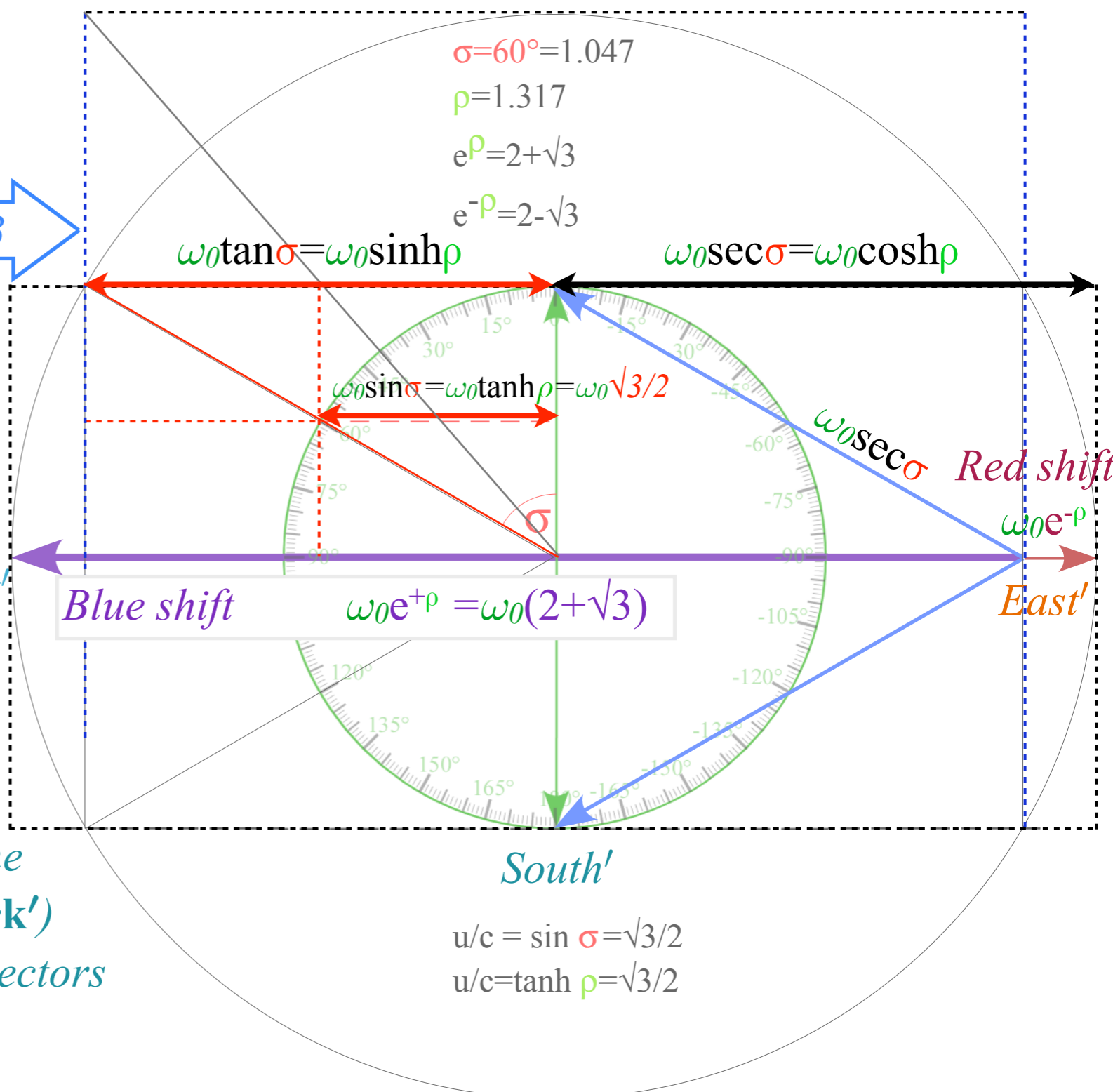
Lorentz boost by $\sigma=60^\circ$ or $e^{+\rho}=2+\sqrt{3}$



Lighthouse view $(\omega, c\mathbf{k})$ of wave-vectors

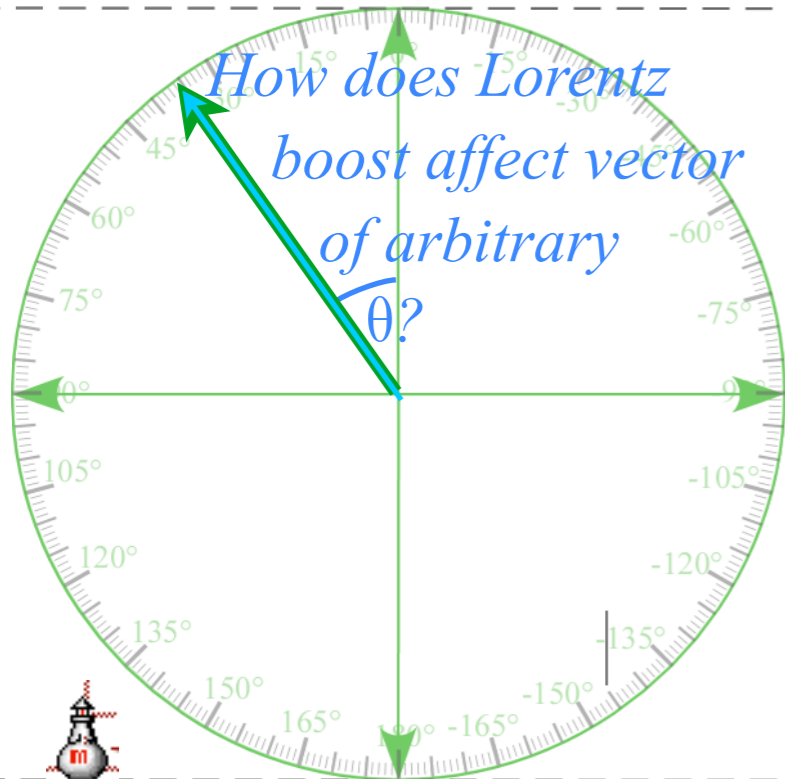


Ship-frame view $(\omega', c\mathbf{k}')$ of wave-vectors

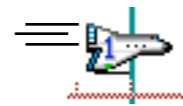


Faster Lorentz boost of North-South-East-West plane-wave 4-vectors $(\omega_0, \omega_x, \omega_y, \omega_z)$

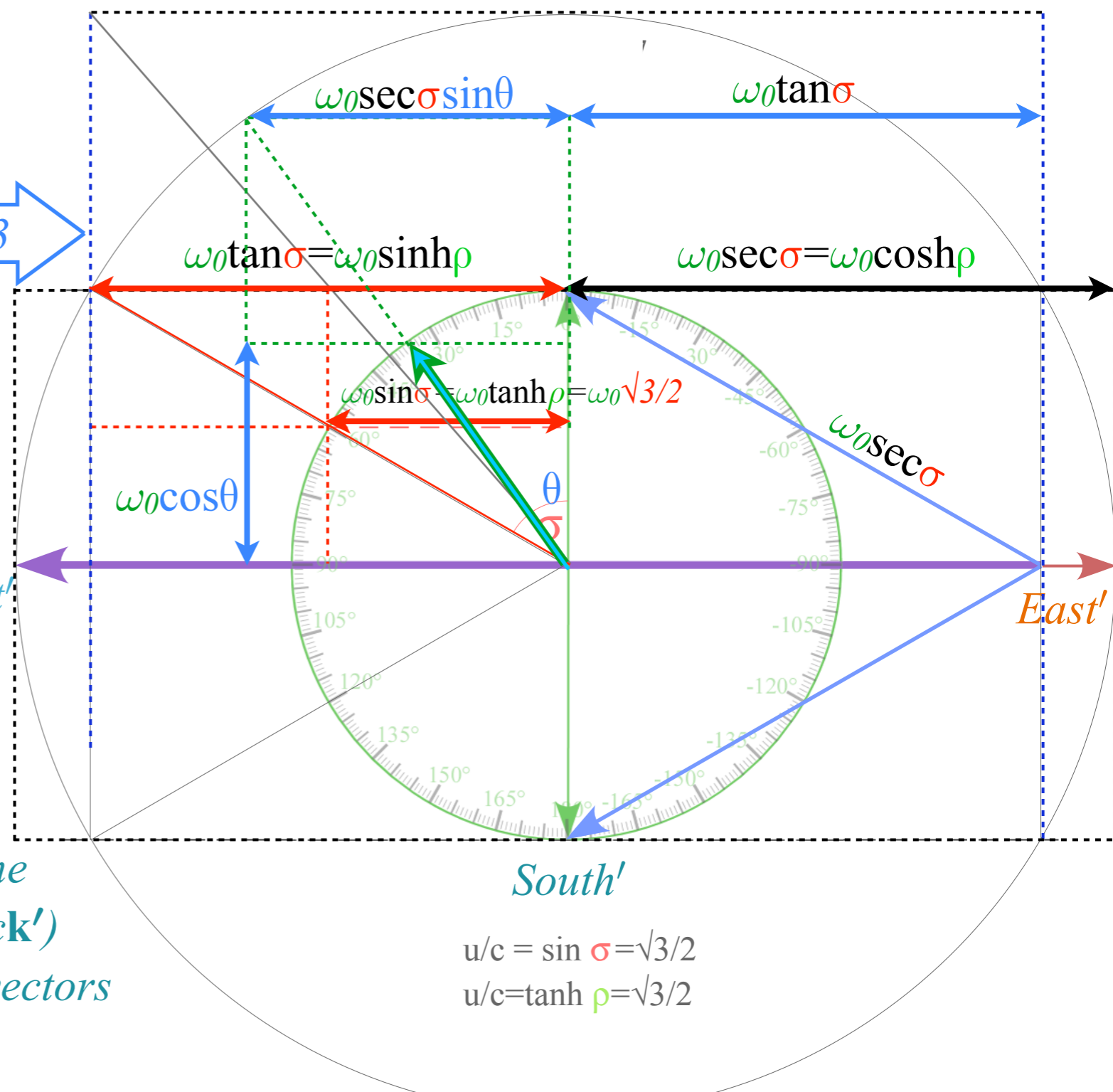
Lorentz boost by $\sigma = 60^\circ$ or $e^{+\rho} = 2 + \sqrt{3}$



Lighthouse view $(\omega, c\mathbf{k})$ of wave-vectors



Ship-frame view $(\omega', c\mathbf{k}')$ of wave-vectors

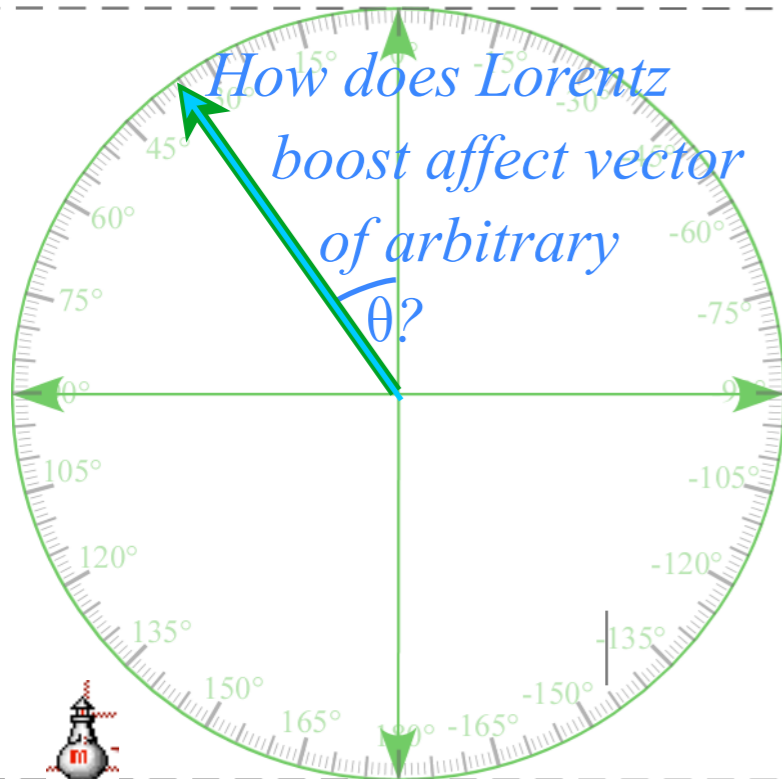


Let lab starlight ray at polar angle θ have $\mathbf{k} \uparrow \theta = \omega_0 (1, \cos \theta, 0, -\sin \theta)$. Then ship going u along z -axis sees :

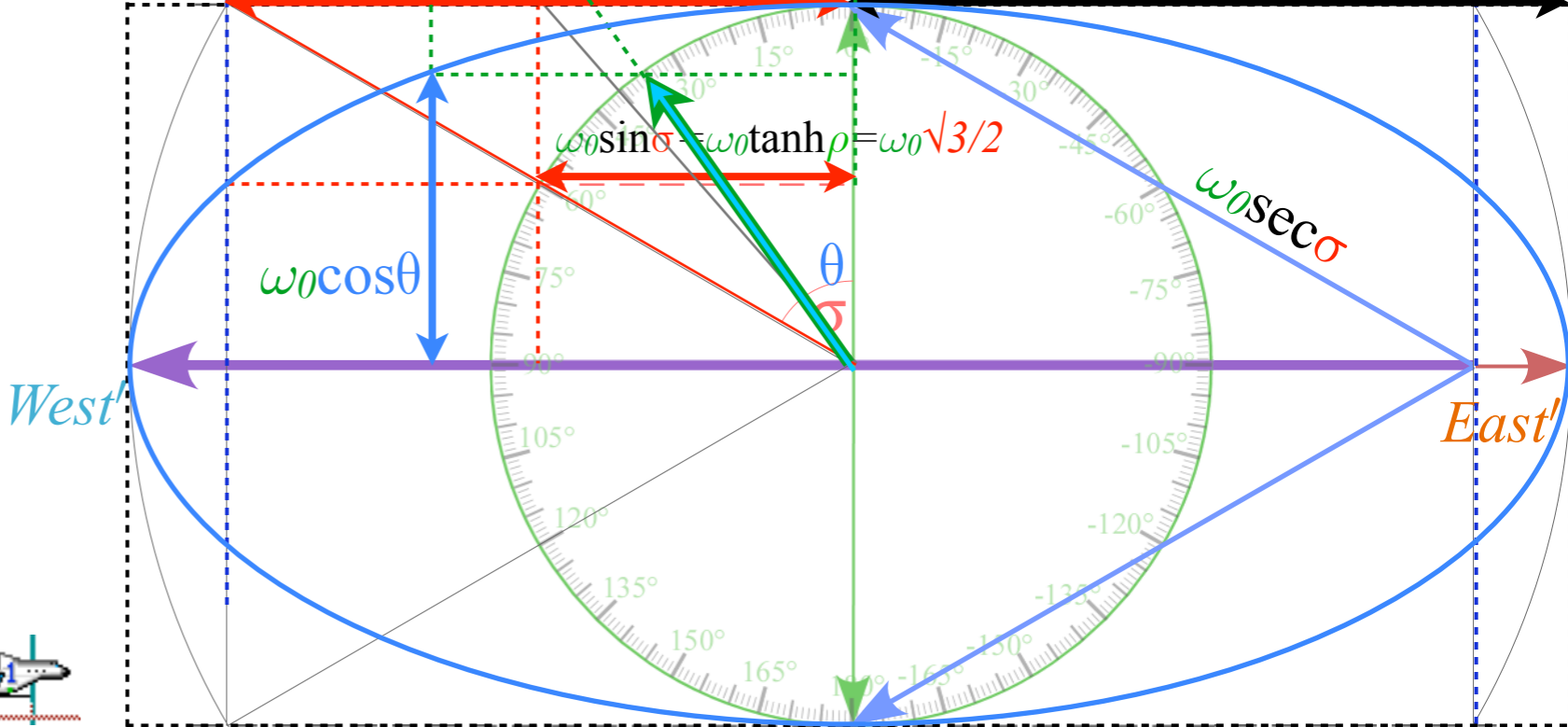
$$\begin{pmatrix} \omega'_{\uparrow \theta} \\ ck'_{x \uparrow \theta} \\ ck'_{y \uparrow \theta} \\ ck'_{z \uparrow \theta} \end{pmatrix} = \begin{pmatrix} \cosh \rho_z & \cdot & \cdot & -\sinh \rho_z \\ \cdot & 1 & \cdot & \cdot \\ \cdot & \cdot & 1 & \cdot \\ -\sinh \rho_z & \cdot & \cdot & \cosh \rho_z \end{pmatrix} \begin{pmatrix} \omega_0 \\ \omega_0 \cos \theta \\ 0 \\ -\omega_0 \sin \theta \end{pmatrix} = \omega_0 \begin{pmatrix} \cosh \rho_z + \sinh \rho_z \sin \theta \\ \cos \theta \\ 0 \\ -\sinh \rho_z - \cosh \rho_z \sin \theta \end{pmatrix} = \omega_0 \begin{pmatrix} \sec \sigma + \tan \sigma \sin \theta \\ \cos \theta \\ 0 \\ -\tan \sigma - \sec \sigma \sin \theta \end{pmatrix}$$

Faster Lorentz boost of North-South-East-West plane-wave 4-vectors $(\omega_0, \omega_x, \omega_y, \omega_z)$

Lorentz boost by $\sigma = 60^\circ$ or $e^{+\rho} = 2 + \sqrt{3}$



Lighthouse view $(\omega, c\mathbf{k})$ of wave-vectors



Ship-frame view $(\omega', c\mathbf{k}')$ of wave-vectors

$$u/c = \sin \sigma = \sqrt{3}/2$$

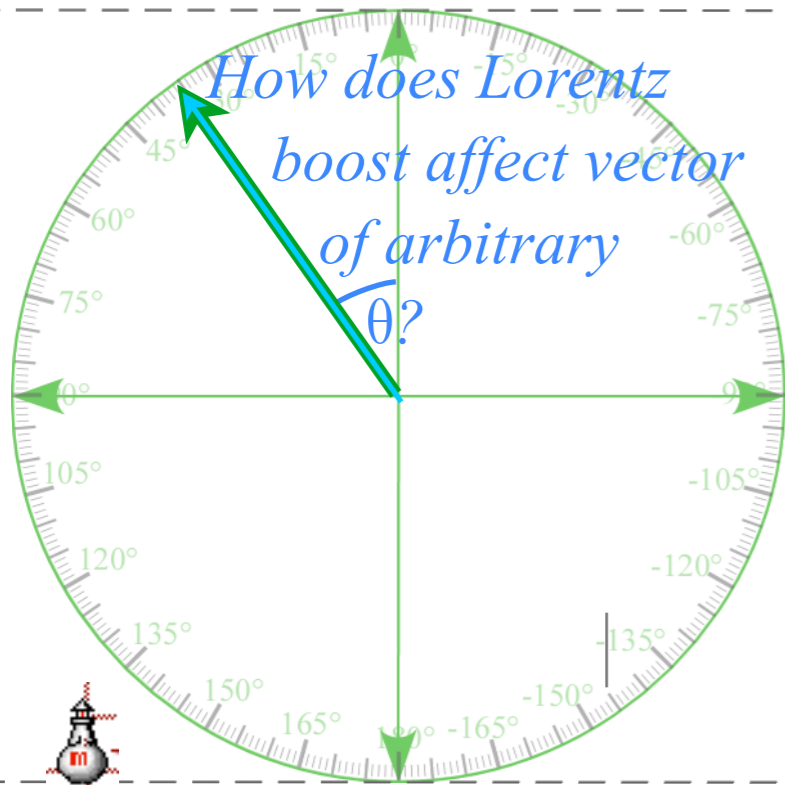
$$u/c = \tanh \rho = \sqrt{3}/2$$

Let lab starlight ray at polar angle θ have $\mathbf{k} \uparrow \theta = \omega_0 (1, \cos \theta, 0, -\sin \theta)$. Then ship going \mathbf{u} along z -axis sees :

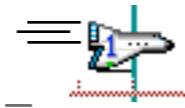
$$\begin{pmatrix} \omega'_{\uparrow\theta} \\ ck'_{x\uparrow\theta} \\ ck'_{y\uparrow\theta} \\ ck'_{z\uparrow\theta} \end{pmatrix} = \begin{pmatrix} \cosh \rho_z & \cdot & \cdot & -\sinh \rho_z \\ \cdot & 1 & \cdot & \cdot \\ \cdot & \cdot & 1 & \cdot \\ -\sinh \rho_z & \cdot & \cdot & \cosh \rho_z \end{pmatrix} \begin{pmatrix} \omega_0 \\ \omega_0 \cos \theta \\ 0 \\ -\omega_0 \sin \theta \end{pmatrix} = \omega_0 \begin{pmatrix} \cosh \rho_z + \sinh \rho_z \sin \theta \\ \cos \theta \\ 0 \\ -\sinh \rho_z - \cosh \rho_z \sin \theta \end{pmatrix} = \omega_0 \begin{pmatrix} \sec \sigma + \tan \sigma \sin \theta \\ \cos \theta \\ 0 \\ -\tan \sigma - \sec \sigma \sin \theta \end{pmatrix}$$

Faster Lorentz boost of North-South-East-West plane-wave 4-vectors $(\omega_0, \omega_x, \omega_y, \omega_z)$

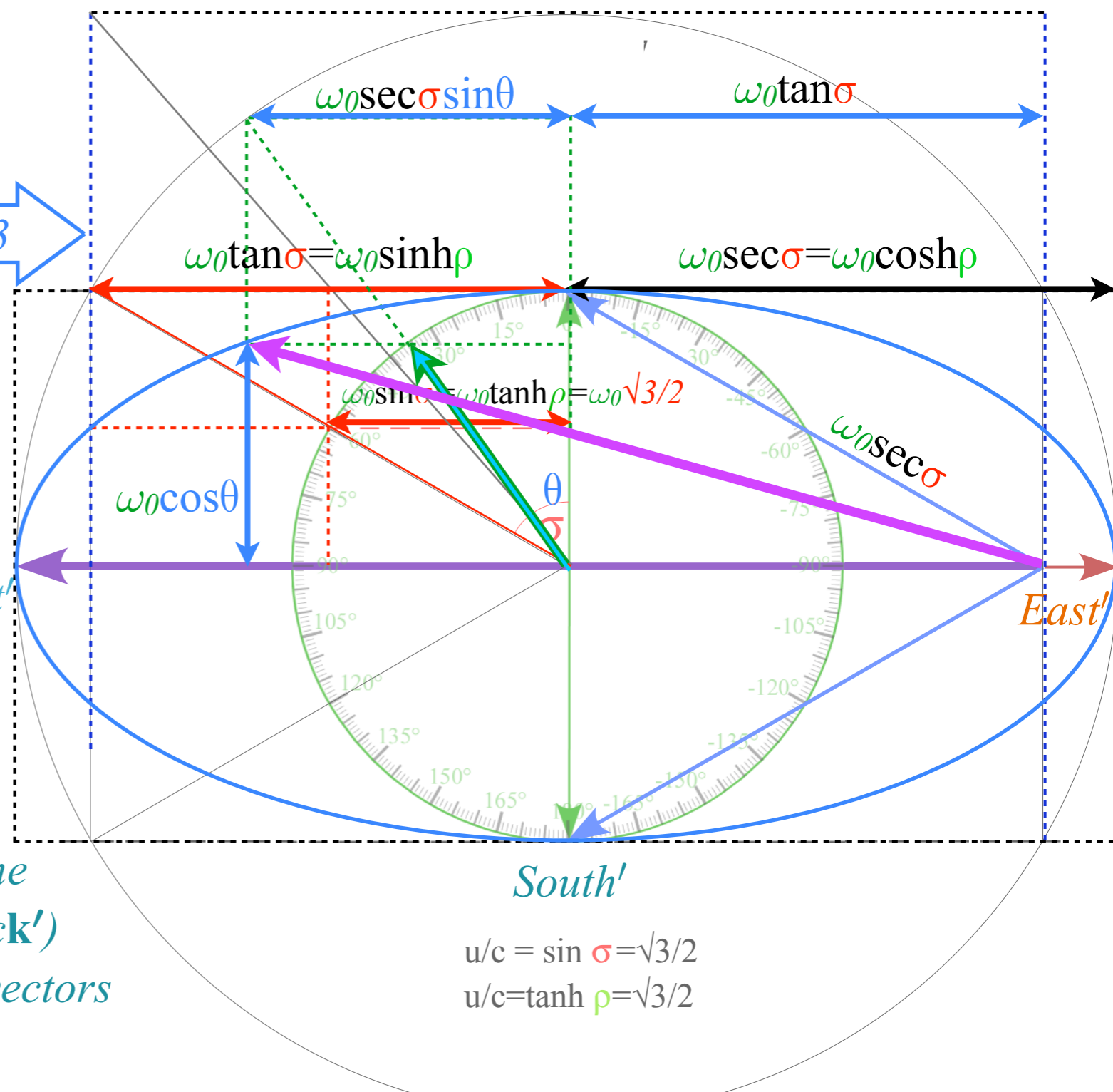
Lorentz boost by $\sigma = 60^\circ$ or $e^{+\rho} = 2 + \sqrt{3}$



Lighthouse view $(\omega, c\mathbf{k})$ of wave-vectors



Ship-frame view $(\omega', c\mathbf{k}')$ of wave-vectors



$$u/c = \sin \sigma = \sqrt{3}/2$$

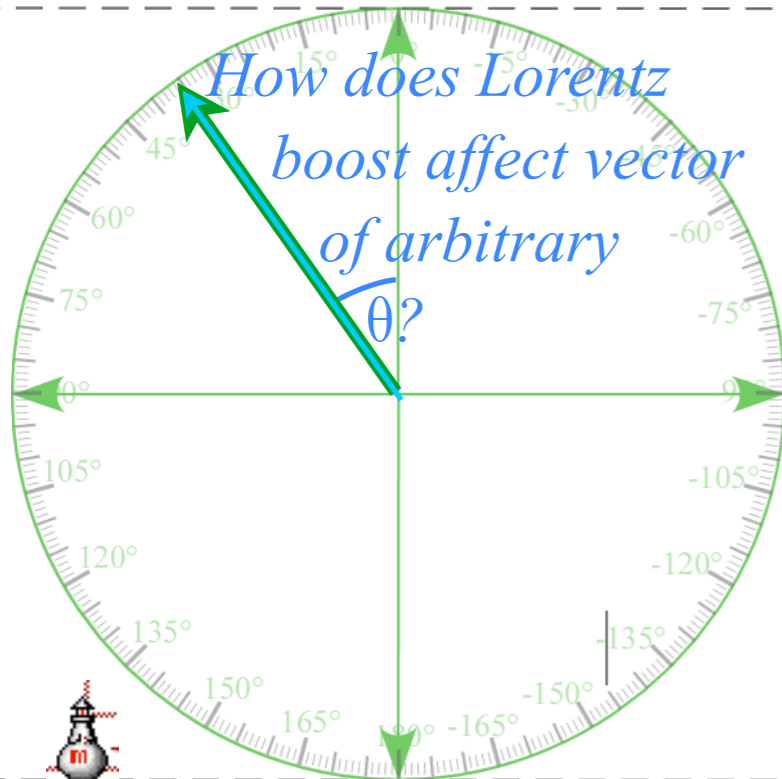
$$u/c = \tanh \rho = \sqrt{3}/2$$

Let lab starlight ray at polar angle θ have $\mathbf{k} \uparrow \theta = \omega_0 (1, \cos \theta, 0, -\sin \theta)$. Then ship going u along z -axis sees :

$$\begin{pmatrix} \omega'_{\uparrow\theta} \\ ck'_{x\uparrow\theta} \\ ck'_{y\uparrow\theta} \\ ck'_{z\uparrow\theta} \end{pmatrix} = \begin{pmatrix} \cosh \rho_z & \cdot & \cdot & -\sinh \rho_z \\ \cdot & 1 & \cdot & \cdot \\ \cdot & \cdot & 1 & \cdot \\ -\sinh \rho_z & \cdot & \cdot & \cosh \rho_z \end{pmatrix} \begin{pmatrix} \omega_0 \\ \omega_0 \cos \theta \\ 0 \\ -\omega_0 \sin \theta \end{pmatrix} = \omega_0 \begin{pmatrix} \cosh \rho_z + \sinh \rho_z \sin \theta \\ \cos \theta \\ 0 \\ -\sinh \rho_z - \cosh \rho_z \sin \theta \end{pmatrix} = \omega_0 \begin{pmatrix} \sec \sigma + \tan \sigma \sin \theta \\ \cos \theta \\ 0 \\ -\tan \sigma - \sec \sigma \sin \theta \end{pmatrix}$$

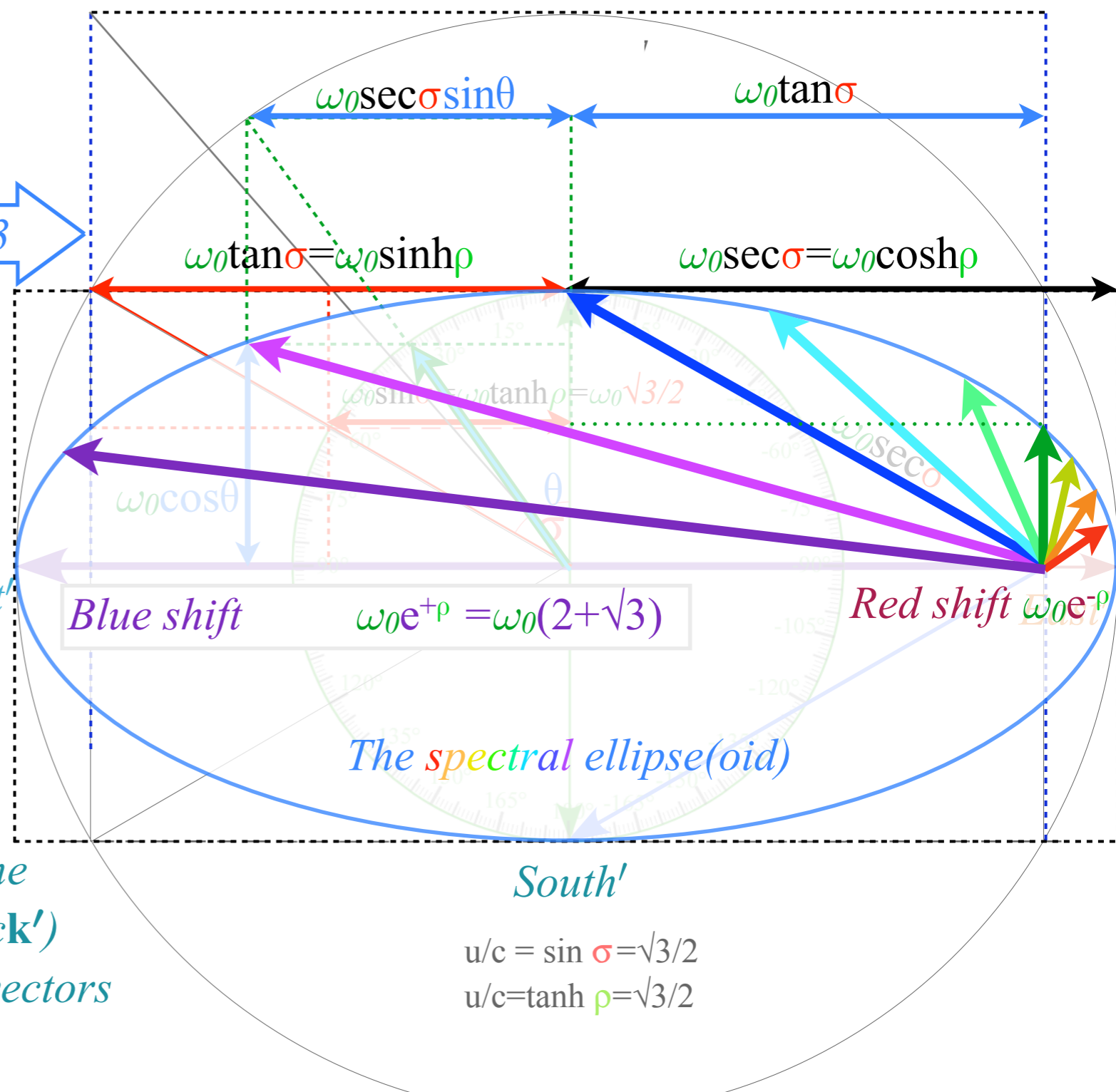
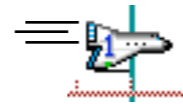
Faster Lorentz boost of
North-South-East-West
plane-wave 4-vectors $(\omega_0, \omega_x, \omega_y, \omega_z)$

Lorentz boost by $\sigma = 60^\circ$ or $e^{+\rho} = 2 + \sqrt{3}$



Lighthouse
view $(\omega, c\mathbf{k})$
of wave-vectors

Ship-frame
view $(\omega', c\mathbf{k}')$
of wave-vectors

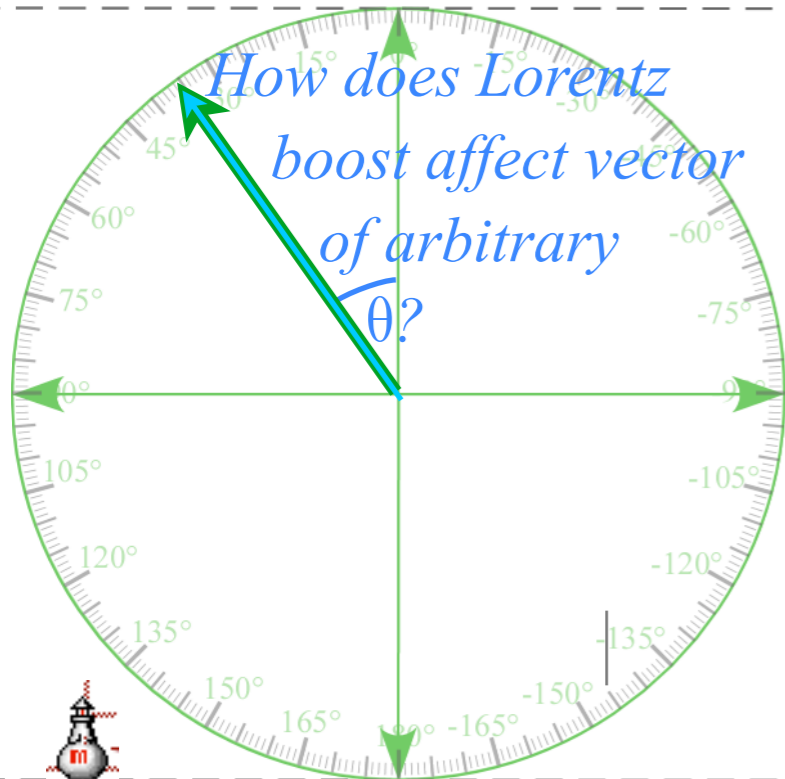


Let lab starlight ray at polar angle θ have $\mathbf{k} \uparrow \theta = \omega_0 (1, \cos \theta, 0, -\sin \theta)$. Then ship going \mathbf{u} along z -axis sees :

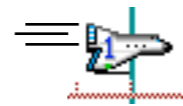
$$\begin{pmatrix} \omega'_{\uparrow \theta} \\ ck'_{x \uparrow \theta} \\ ck'_{y \uparrow \theta} \\ ck'_{z \uparrow \theta} \end{pmatrix} = \begin{pmatrix} \cosh \rho_z & \cdot & \cdot & -\sinh \rho_z \\ \cdot & 1 & \cdot & \cdot \\ \cdot & \cdot & 1 & \cdot \\ -\sinh \rho_z & \cdot & \cdot & \cosh \rho_z \end{pmatrix} \begin{pmatrix} \omega_0 \\ \omega_0 \cos \theta \\ 0 \\ -\omega_0 \sin \theta \end{pmatrix} = \omega_0 \begin{pmatrix} \cosh \rho_z + \sinh \rho_z \sin \theta \\ \cos \theta \\ 0 \\ -\sinh \rho_z - \cosh \rho_z \sin \theta \end{pmatrix} = \omega_0 \begin{pmatrix} \sec \sigma + \tan \sigma \sin \theta \\ \cos \theta \\ 0 \\ -\tan \sigma - \sec \sigma \sin \theta \end{pmatrix}$$

Faster Lorentz boost of North-South-East-West plane-wave 4-vectors $(\omega_0, \omega_x, \omega_y, \omega_z)$

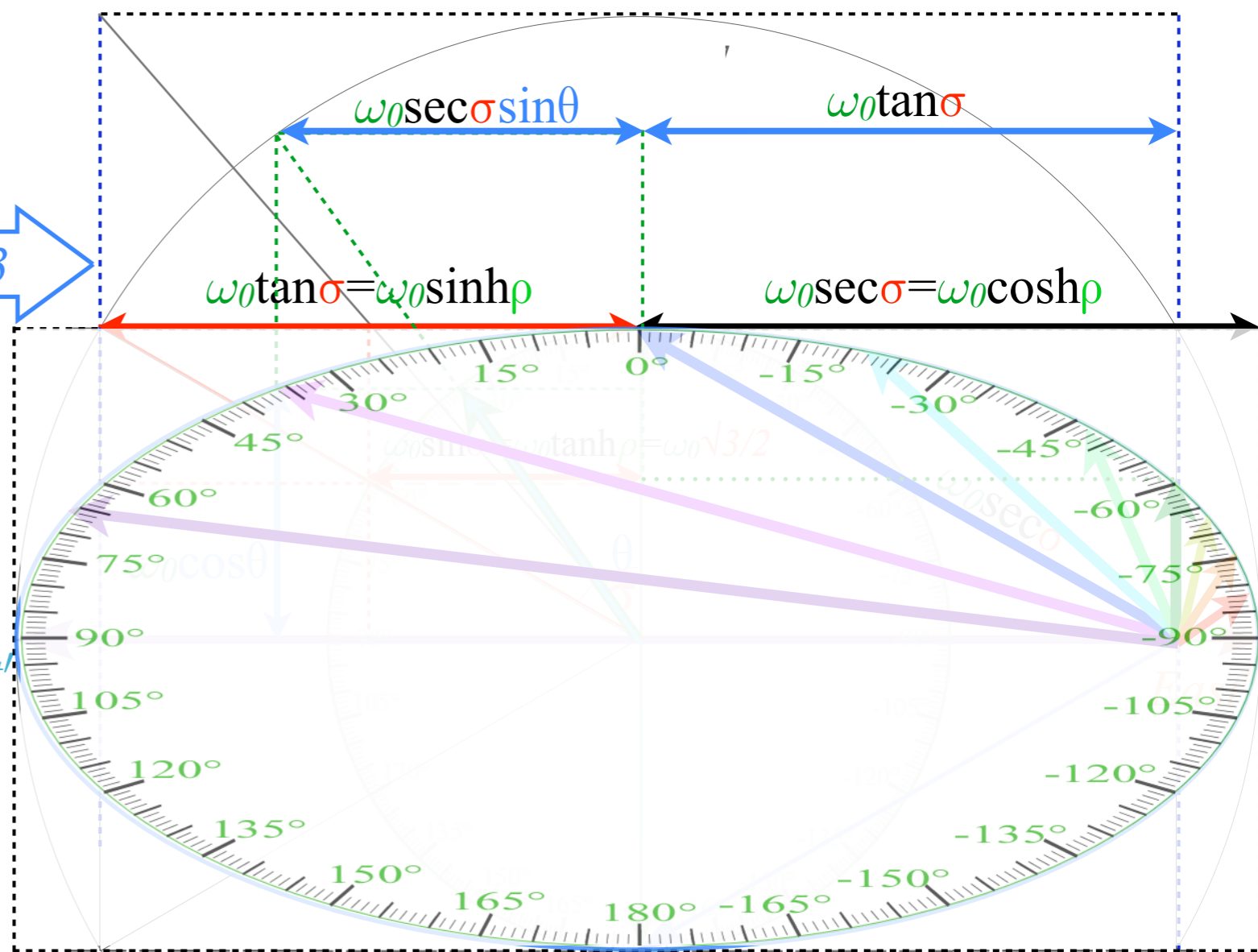
Lorentz boost by $\sigma = 60^\circ$ or $e^{+\rho} = 2 + \sqrt{3}$



Lighthouse view $(\omega, c\mathbf{k})$ of wave-vectors



Ship-frame view $(\omega', c\mathbf{k}')$ of wave-vectors



South'

$$u/c = \sin \sigma = \sqrt{3}/2$$

$$u/c = \tanh \rho = \sqrt{3}/2$$

Let lab starlight ray at polar angle θ have $\mathbf{k} \uparrow \theta = \omega_0 (1, \cos \theta, 0, -\sin \theta)$. Then ship going \mathbf{u} along z -axis sees :

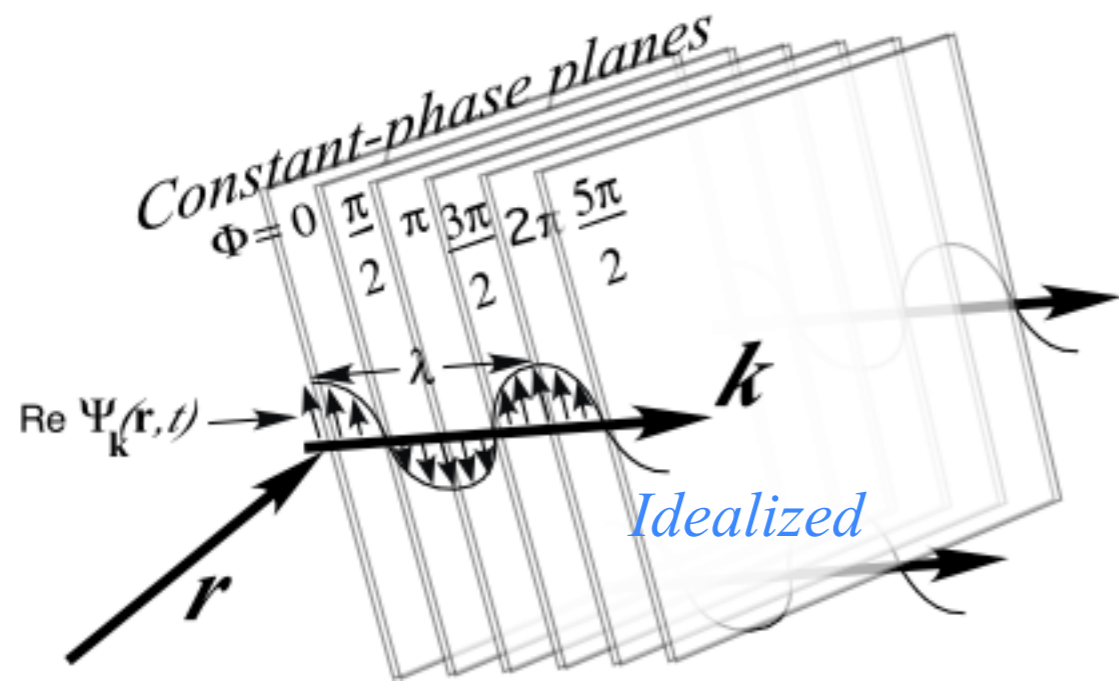
$$\begin{pmatrix} \omega'_{\uparrow \theta} \\ ck'_{x \uparrow \theta} \\ ck'_{y \uparrow \theta} \\ ck'_{z \uparrow \theta} \end{pmatrix} = \begin{pmatrix} \cosh \rho_z & \cdot & \cdot & -\sinh \rho_z \\ \cdot & 1 & \cdot & \cdot \\ \cdot & \cdot & 1 & \cdot \\ -\sinh \rho_z & \cdot & \cdot & \cosh \rho_z \end{pmatrix} \begin{pmatrix} \omega_0 \\ \omega_0 \cos \theta \\ 0 \\ -\omega_0 \sin \theta \end{pmatrix} = \omega_0 \begin{pmatrix} \cosh \rho_z + \sinh \rho_z \sin \theta \\ \cos \theta \\ 0 \\ -\sinh \rho_z - \cosh \rho_z \sin \theta \end{pmatrix} = \omega_0 \begin{pmatrix} \sec \sigma + \tan \sigma \sin \theta \\ \cos \theta \\ 0 \\ -\tan \sigma - \sec \sigma \sin \theta \end{pmatrix}$$

Combination and interference of 4-vector plane waves (Idealized amplitude case)

$$\Psi_{A_{\rightarrow}, \omega_{\rightarrow}, \mathbf{k}_{\rightarrow}; A_{\leftarrow}, \omega_{\leftarrow}, \mathbf{k}_{\leftarrow}}(\mathbf{r}, t) = A_{\rightarrow} e^{i(\mathbf{k}_{\rightarrow} \cdot \mathbf{r} - \omega_{\rightarrow} t)} + A_{\leftarrow} e^{i(\mathbf{k}_{\leftarrow} \cdot \mathbf{r} - \omega_{\leftarrow} t)}$$

2-CW-single-plane-polarized case: $\Psi_{\mathbf{k}}(\mathbf{r}, t) = e^{i(\mathbf{k}_{\rightarrow} \cdot \mathbf{r} - \omega_{\rightarrow} t)} + e^{i(\mathbf{k}_{\leftarrow} \cdot \mathbf{r} - \omega_{\leftarrow} t)}$ *Idealized: Equal amplitudes and single plane polarization*

Factored into *phase* and *group* factors:

$$= e^{i \frac{(\mathbf{k}_{\rightarrow} + \mathbf{k}_{\leftarrow}) \cdot \mathbf{r} - (\omega_{\rightarrow} + \omega_{\leftarrow}) t}{2}} 2 \cos \frac{(\mathbf{k}_{\rightarrow} - \mathbf{k}_{\leftarrow}) \cdot \mathbf{r} - (\omega_{\rightarrow} - \omega_{\leftarrow}) t}{2} = e^{i(\bar{\mathbf{K}} \cdot \mathbf{r} - \bar{\Omega} t)} 2 \cos(\bar{\mathbf{k}} \cdot \mathbf{r} - \bar{\omega} t)$$


Phase (k, ω)

$$\frac{(\mathbf{k}_{\rightarrow} + \mathbf{k}_{\leftarrow})}{2} = \bar{\mathbf{K}},$$

$$\frac{(\omega_{\rightarrow} + \omega_{\leftarrow})}{2} = \bar{\Omega},$$

Group (k, ω)

$$\bar{\mathbf{k}} = \frac{(\mathbf{k}_{\rightarrow} - \mathbf{k}_{\leftarrow})}{2},$$

$$\bar{\omega} = \frac{(\omega_{\rightarrow} - \omega_{\leftarrow})}{2}.$$

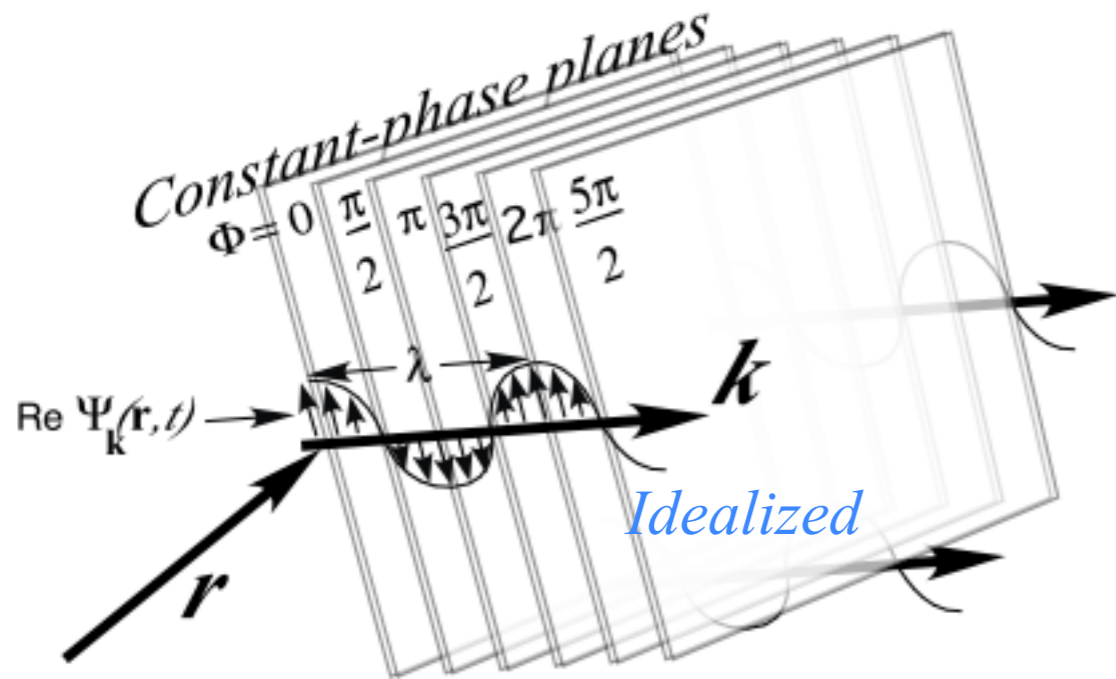
Fig. 6A.0 Sketch of a 1-CW-single-plane-polarized plane wavefunction $\Psi_{\mathbf{k}}(\mathbf{r}, t) = A e^{i\Phi} = A e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$ with wavevector \mathbf{k} .

Combination and interference of 4-vector plane waves (Idealized amplitude case)

$$\Psi_{A_{\rightarrow}, \omega_{\rightarrow}, \mathbf{k}_{\rightarrow}; A_{\leftarrow}, \omega_{\leftarrow}, \mathbf{k}_{\leftarrow}}(\mathbf{r}, t) = A_{\rightarrow} e^{i(\mathbf{k}_{\rightarrow} \cdot \mathbf{r} - \omega_{\rightarrow} t)} + A_{\leftarrow} e^{i(\mathbf{k}_{\leftarrow} \cdot \mathbf{r} - \omega_{\leftarrow} t)}$$

2-CW-single-plane-polarized case: $\Psi_{\mathbf{k}}(\mathbf{r}, t) = e^{i(\mathbf{k}_{\rightarrow} \cdot \mathbf{r} - \omega_{\rightarrow} t)} + e^{i(\mathbf{k}_{\leftarrow} \cdot \mathbf{r} - \omega_{\leftarrow} t)}$ *Idealized: Equal amplitudes and single plane polarization*

Factored into *phase* and *group* factors:

$$= e^{i \frac{(\mathbf{k}_{\rightarrow} + \mathbf{k}_{\leftarrow}) \cdot \mathbf{r} - (\omega_{\rightarrow} + \omega_{\leftarrow}) t}{2}} 2 \cos \frac{(\mathbf{k}_{\rightarrow} - \mathbf{k}_{\leftarrow}) \cdot \mathbf{r} - (\omega_{\rightarrow} - \omega_{\leftarrow}) t}{2} = e^{i(\bar{\mathbf{k}} \cdot \mathbf{r} - \bar{\omega} t)} 2 \cos(\bar{\mathbf{k}} \cdot \mathbf{r} - \bar{\omega} t)$$


Phase (k, ω)

$$\frac{(\mathbf{k}_{\rightarrow} + \mathbf{k}_{\leftarrow})}{2} = \bar{\mathbf{k}},$$

$$\frac{(\omega_{\rightarrow} + \omega_{\leftarrow})}{2} = \bar{\omega},$$

Group (k, ω)

$$\bar{\mathbf{k}} = \frac{(\mathbf{k}_{\rightarrow} - \mathbf{k}_{\leftarrow})}{2},$$

$$\bar{\omega} = \frac{(\omega_{\rightarrow} - \omega_{\leftarrow})}{2}.$$

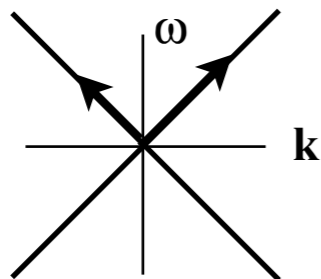
Fig. 6A.0 Sketch of a 1-CW-single-plane-polarized plane wavefunction $\Psi_{\mathbf{k}}(\mathbf{r}, t) = Ae^{i\Phi} = Ae^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$ with wavevector \mathbf{k} .

Individual laser 4-vectors reside on light cone or null-invariant.

Ship Lighthouse Laser lab

$$c^2 \mathbf{k}'_{\rightarrow} \cdot \mathbf{k}'_{\rightarrow} - \omega'^2_{\rightarrow} = c^2 \mathbf{k}_{\rightarrow} \cdot \mathbf{k}_{\rightarrow} - \omega^2_{\rightarrow} = c^2 k_0^2 - \omega_0^2 = 0$$

$$c^2 \mathbf{k}'_{\leftarrow} \cdot \mathbf{k}'_{\leftarrow} - \omega'^2_{\leftarrow} = c^2 \mathbf{k}_{\leftarrow} \cdot \mathbf{k}_{\leftarrow} - \omega^2_{\leftarrow} = c^2 k_0^2 - \omega_0^2 = 0$$

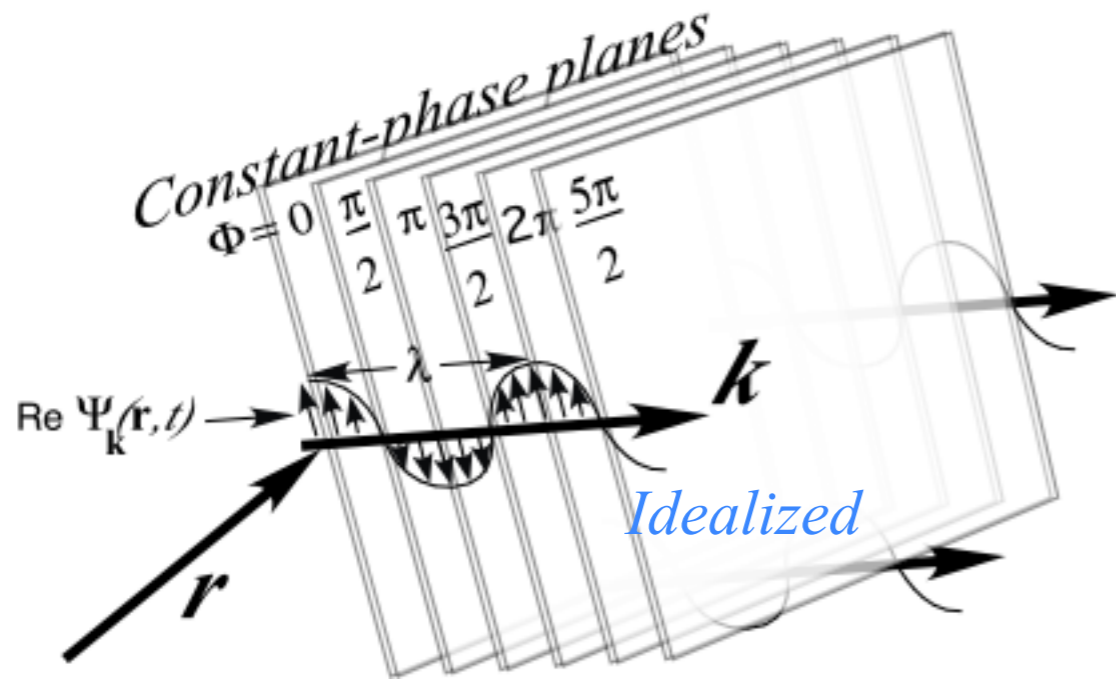


Combination and interference of 4-vector plane waves (Idealized amplitude case)

$$\Psi_{A_{\rightarrow}, \omega_{\rightarrow}, \mathbf{k}_{\rightarrow}; A_{\leftarrow}, \omega_{\leftarrow}, \mathbf{k}_{\leftarrow}}(\mathbf{r}, t) = A_{\rightarrow} e^{i(\mathbf{k}_{\rightarrow} \cdot \mathbf{r} - \omega_{\rightarrow} t)} + A_{\leftarrow} e^{i(\mathbf{k}_{\leftarrow} \cdot \mathbf{r} - \omega_{\leftarrow} t)}$$

2-CW-single-plane-polarized case: $\Psi_{\mathbf{k}}(\mathbf{r}, t) = e^{i(\mathbf{k}_{\rightarrow} \cdot \mathbf{r} - \omega_{\rightarrow} t)} + e^{i(\mathbf{k}_{\leftarrow} \cdot \mathbf{r} - \omega_{\leftarrow} t)}$ *Idealized: Equal amplitudes and single plane polarization*

Factored into *phase* and *group* factors:

$$= e^{i \frac{(\mathbf{k}_{\rightarrow} + \mathbf{k}_{\leftarrow}) \cdot \mathbf{r} - (\omega_{\rightarrow} + \omega_{\leftarrow}) t}{2}} 2 \cos \frac{(\mathbf{k}_{\rightarrow} - \mathbf{k}_{\leftarrow}) \cdot \mathbf{r} - (\omega_{\rightarrow} - \omega_{\leftarrow}) t}{2} = e^{i(\bar{\mathbf{K}} \cdot \mathbf{r} - \bar{\omega} t)} 2 \cos(\bar{\mathbf{k}} \cdot \mathbf{r} - \bar{\omega} t)$$


Phase (k, ω)

$$\frac{(\mathbf{k}_{\rightarrow} + \mathbf{k}_{\leftarrow})}{2} = \bar{\mathbf{K}},$$

$$\frac{(\omega_{\rightarrow} + \omega_{\leftarrow})}{2} = \bar{\omega},$$

Group (k, ω)

$$\bar{\mathbf{k}} = \frac{(\mathbf{k}_{\rightarrow} - \mathbf{k}_{\leftarrow})}{2},$$

$$\bar{\omega} = \frac{(\omega_{\rightarrow} - \omega_{\leftarrow})}{2}.$$

Fig. 6A.0 Sketch of a 1-CW-single-plane-polarized plane wavefunction $\Psi_{\mathbf{k}}(\mathbf{r}, t) = Ae^{i\Phi} = Ae^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$ with wavevector \mathbf{k} .

Individual laser 4-vectors reside on light cone or null-invariant.

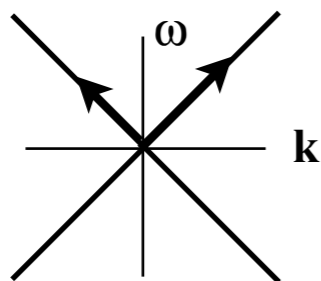
Ship

Lighthouse

Laser lab

$$c^2 \mathbf{k}'_{\rightarrow} \cdot \mathbf{k}'_{\rightarrow} - \omega'^2_{\rightarrow} = c^2 \mathbf{k}_{\rightarrow} \cdot \mathbf{k}_{\rightarrow} - \omega^2_{\rightarrow} = c^2 k_0^2 - \omega_0^2 = 0$$

$$c^2 \mathbf{k}'_{\leftarrow} \cdot \mathbf{k}'_{\leftarrow} - \omega'^2_{\leftarrow} = c^2 \mathbf{k}_{\leftarrow} \cdot \mathbf{k}_{\leftarrow} - \omega^2_{\leftarrow} = c^2 k_0^2 - \omega_0^2 = 0$$



Sum and difference vectors are not on the light cone.

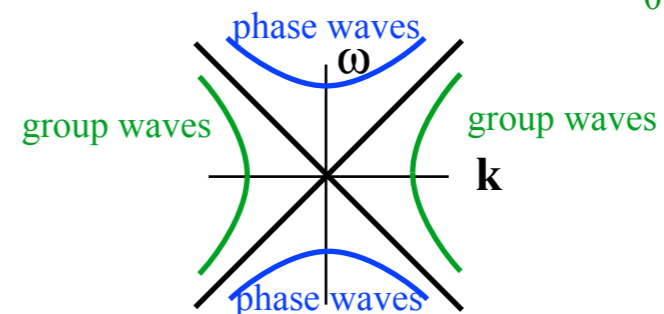
Ship

Lighthouse

Laser lab

$$\bar{\omega}'^2 - c^2 \bar{\mathbf{K}}' \cdot \bar{\mathbf{K}}' = \bar{\omega}^2 - c^2 \bar{\mathbf{K}} \cdot \bar{\mathbf{K}} = \omega_0^2 - 0 = c^2 k_0^2$$

$$\bar{\omega}'^2 - c^2 \bar{\mathbf{k}}' \cdot \bar{\mathbf{k}}' = \bar{\omega}^2 - c^2 \bar{\mathbf{k}} \cdot \bar{\mathbf{k}} = 0 - c^2 \mathbf{k}_0 \cdot \mathbf{k}_0 = -c^2 k_0^2$$



Combination *group* and phase define 4D Minkowski coordinates
 (Idealized amplitude case)

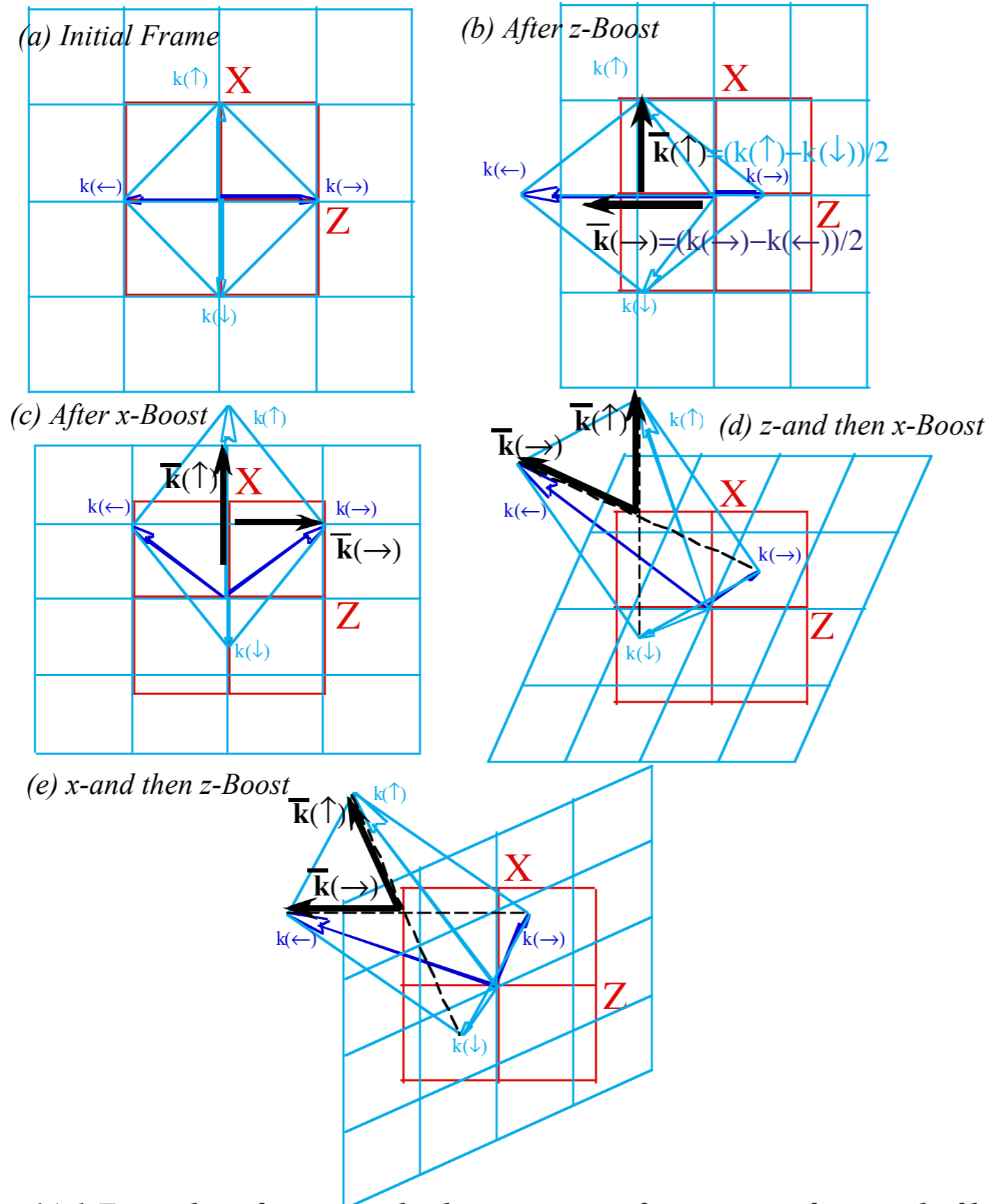


Fig. 6A.1 Examples of sequential relativistic transformations of a tetrad of light wavevectors.

2-Dimensional wave mechanics: guided waves and dispersion in the “Hall of Mirrors”

Any two or three-dimensional wave will be seen to exceed the c -limit when it approaches an axis obliquely. It happens for plane waves. The phase velocities along coordinate axes are given by

$$v_x = \omega / k_x, \quad v_y = \omega / k_y, \quad v_z = \omega / k_z.$$

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Each of the components (k_x, k_y, k_z) must be less than or equal to magnitude $k = \sqrt{(k_x^2 + k_y^2 + k_z^2)}$.

Thus, all the component phase velocities equal or exceed the phase velocity ω / k which is c for light!

A water waves exceeds c if it breaks parallel to shore so "break-line" moves infinitely fast with $k_x = 0$.

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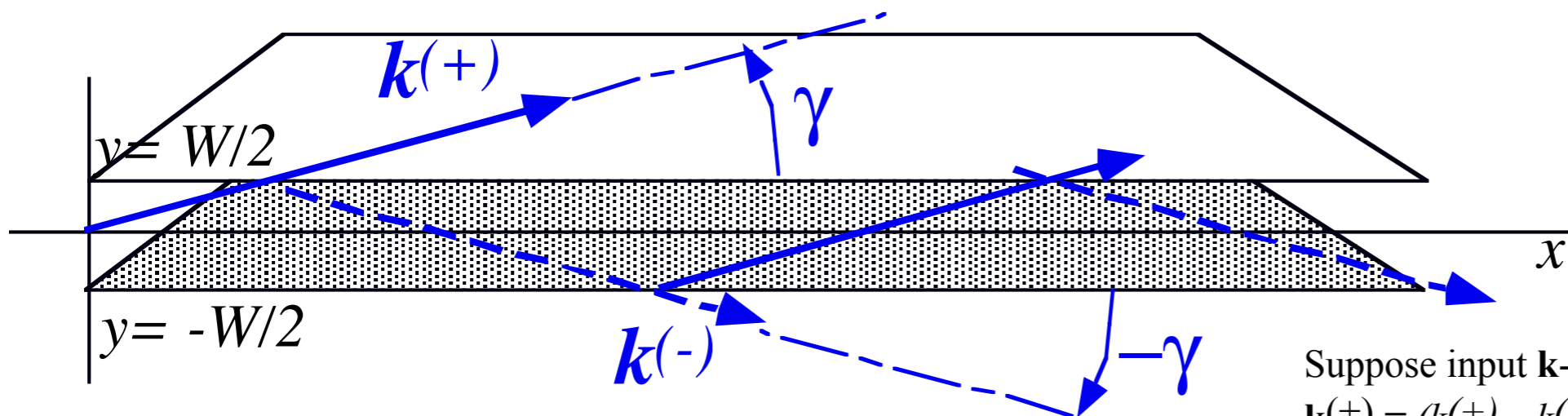
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Consider 'Hall of Mirrors' with two parallel mirrors on either side of the x -axis be separated by a distance $y=W$.

The South wall will be at $y=-W/2$ and the North wall at $y=W/2$. (z -axis or "up" is into the page here.)

The Hall should have a floor and ceiling at $z=\pm H/2$ as discussed later. Here waves move in xy -plane only.



Suppose input \mathbf{k} -vector $\mathbf{k}^{(+)}$ enters at angle $+\gamma$.
 $\mathbf{k}^{(+)} = (k^{(+)}_x, k^{(+)}_y, 0) = (k \cos \gamma, k \sin \gamma, 0)$

Fig. 6B.1 A "hall of mirrors" model for an optical wave guide of width W .

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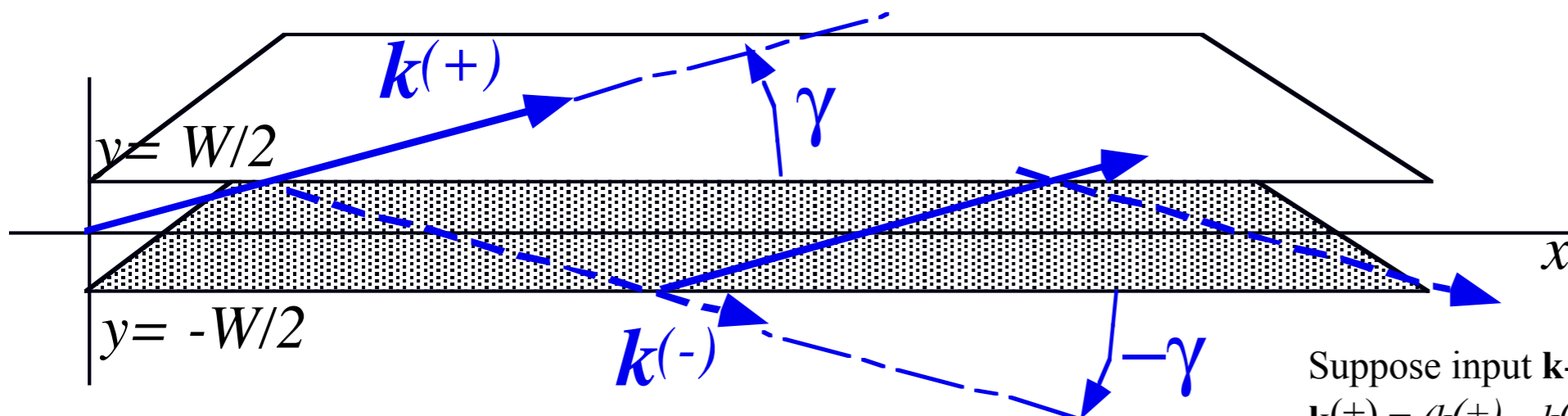


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 $\mathbf{k}^{(+)} = (k^{(+)}_x, k^{(+)}_y, 0) = (k \cos \gamma, k \sin \gamma, 0)$

$$\begin{aligned} \mathbf{E}(\mathbf{r}, t) &= \exp i(\mathbf{k}^{(+)} \cdot \mathbf{r} - \omega t) + \exp i(\mathbf{k}^{(-)} \cdot \mathbf{r} - \omega t) \\ &= \exp i(kx \cos \gamma + ky \sin \gamma - \omega t) + \exp i(kx \cos \gamma - ky \sin \gamma - \omega t) \end{aligned}$$

y -reflected mirror image has \mathbf{k} -vector $\mathbf{k}^{(-)}$ at angle $-\gamma$.
 $\mathbf{k}^{(-)} = (k^{(-)}_x, k^{(-)}_y, 0) = (k \cos \gamma, -k \sin \gamma, 0)$.

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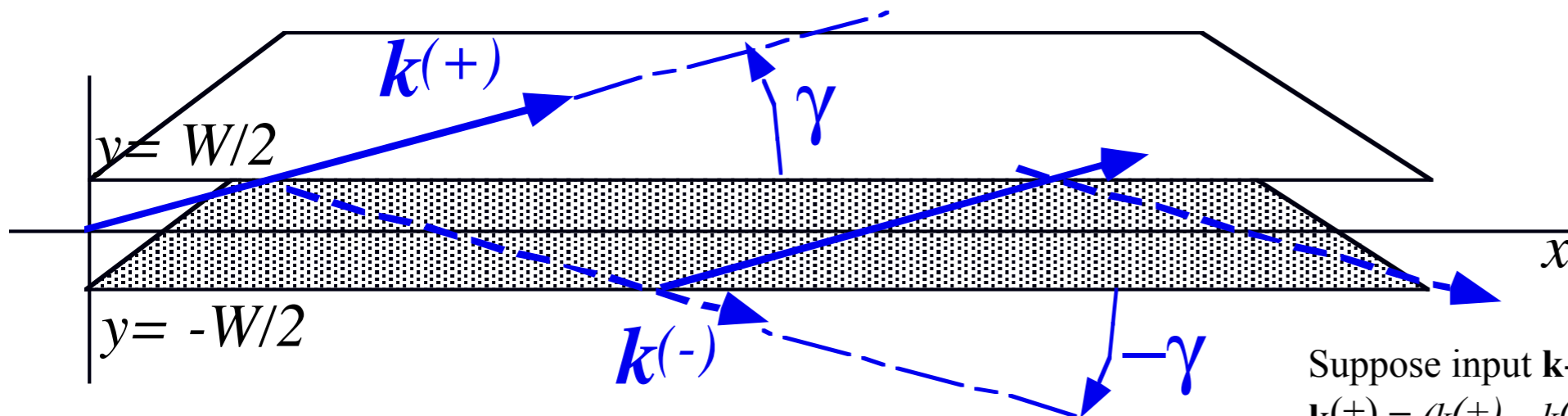


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Each of the components (k_x, k_y, k_z) must be less than or equal to magnitude $k = \sqrt{(k_x^2 + k_y^2 + k_z^2)}$.

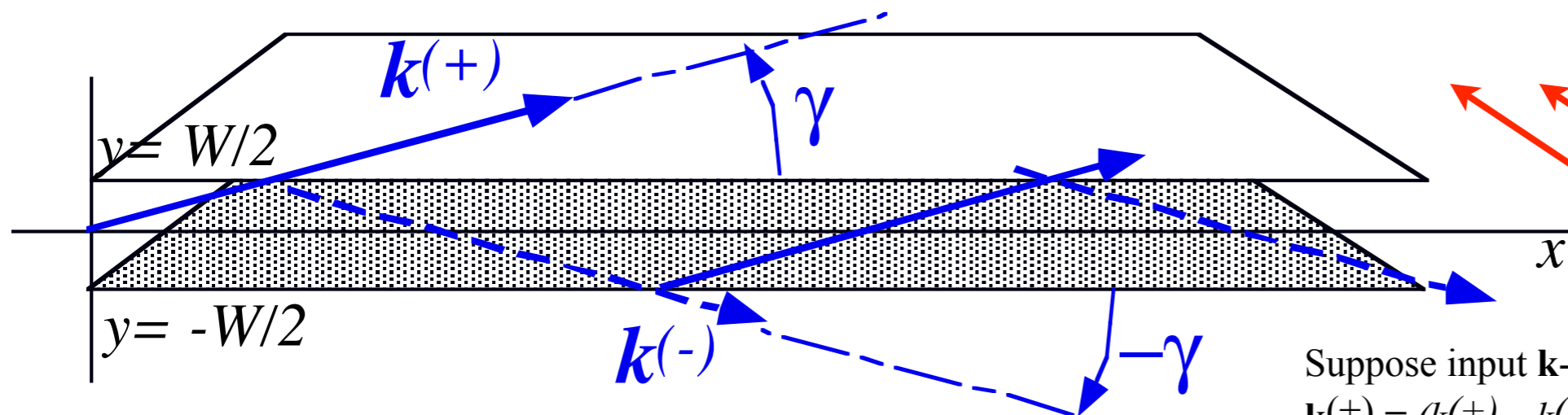
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Assume $T_{\text{ransverse}}E_{\text{lectric}}$ -mode.
It always has \mathbf{E} polarized parallel to xz plane

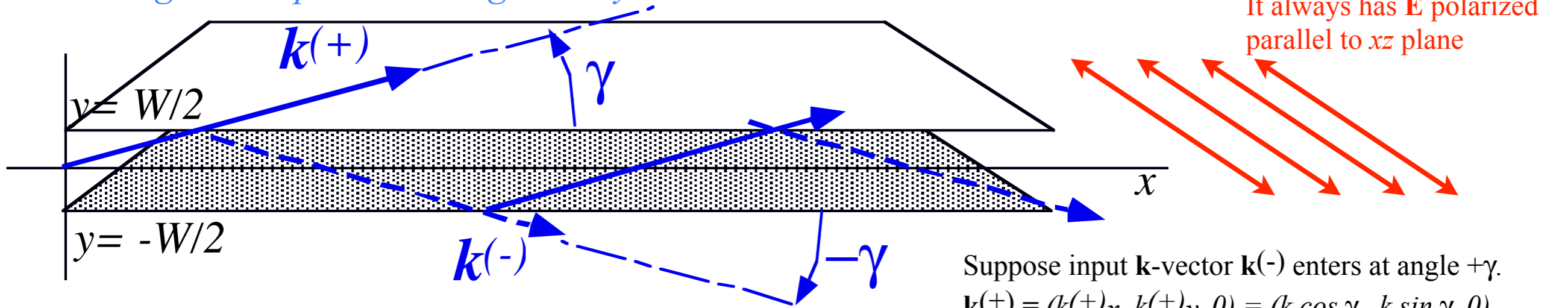
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TE boundary conditions make **group** be **zero** on metal walls $y = \pm W/2$.
 $0 = 2 \cos(k(W/2) \sin \gamma)$, or: $k(W/2) \sin \gamma = \pi/2$, or: $\sin \gamma = \pi/(kW)$

Waveguide dispersion and geometry



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Fig. 6B.1 A "hall of mirrors" model for an optical wave guide of width W .

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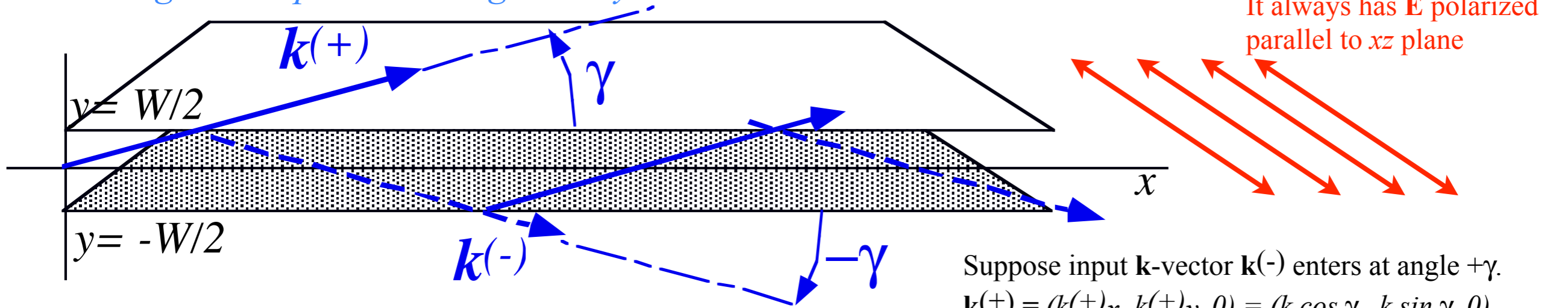
$$\begin{aligned}
 \mathbf{E}(\mathbf{r}, t) &= \exp i(\mathbf{k}^{(+)} \cdot \mathbf{r} - \omega t) + \exp i(\mathbf{k}^{(-)} \cdot \mathbf{r} - \omega t) \\
 &= \exp i(kx \cos \gamma + ky \sin \gamma - \omega t) + \exp i(kx \cos \gamma - ky \sin \gamma - \omega t) \\
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Condition $k^{(+)}_y = k \sin \gamma = \pi/W$ gives dispersion function $\omega(k_x)$ or ω vs. k_x relation

$$\omega = kc = c(k_x^2 + k_y^2 + k_z^2)^{1/2}$$

Waveguide dispersion and geometry



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guide phase wave and group wave

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$$\omega = kc = c(k_x^2 + k_y^2 + \cancel{k_z^2})^{1/2} = c(k_x^2 + \pi^2/W^2)^{1/2} = \sqrt{c^2 k_x^2 + \omega_{cut}^2} \quad \text{where: } \omega_{cut} = \pi c/W.$$

Waveguide dispersion and geometry

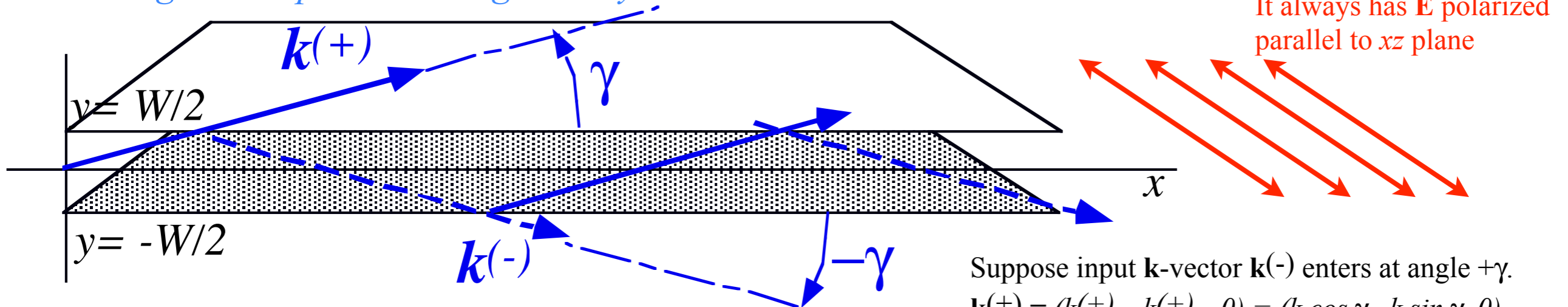


Fig. 6B.1 A "hall of mirrors" model for an optical wave guide of width W.

Suppose input \mathbf{k} -vector $\mathbf{k}(-)$ enters at angle $+\gamma$.
 $\mathbf{k}(+) = (k(+)_x, k(+)_y, 0) = (k \cos \gamma, k \sin \gamma, 0)$

y -reflected mirror image has \mathbf{k} -vector $\mathbf{k}(-)$ at angle $-\gamma$.
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$$\begin{aligned} \mathbf{E}(\mathbf{r}, t) &= \exp i(\mathbf{k}(+) \cdot \mathbf{r} - \omega t) + \exp i(\mathbf{k}(-) \cdot \mathbf{r} - \omega t) \\ &= \exp i(kx \cos \gamma + ky \sin \gamma - \omega t) + \exp i(kx \cos \gamma - ky \sin \gamma - \omega t) \\ &= \exp i(kx \cos \gamma - \omega t) [\exp i(ky \sin \gamma) + \exp i(-ky \sin \gamma)] \\ &= e^{i(kx \cos \gamma - \omega t)} [2 \cos(ky \sin \gamma)] \end{aligned}$$

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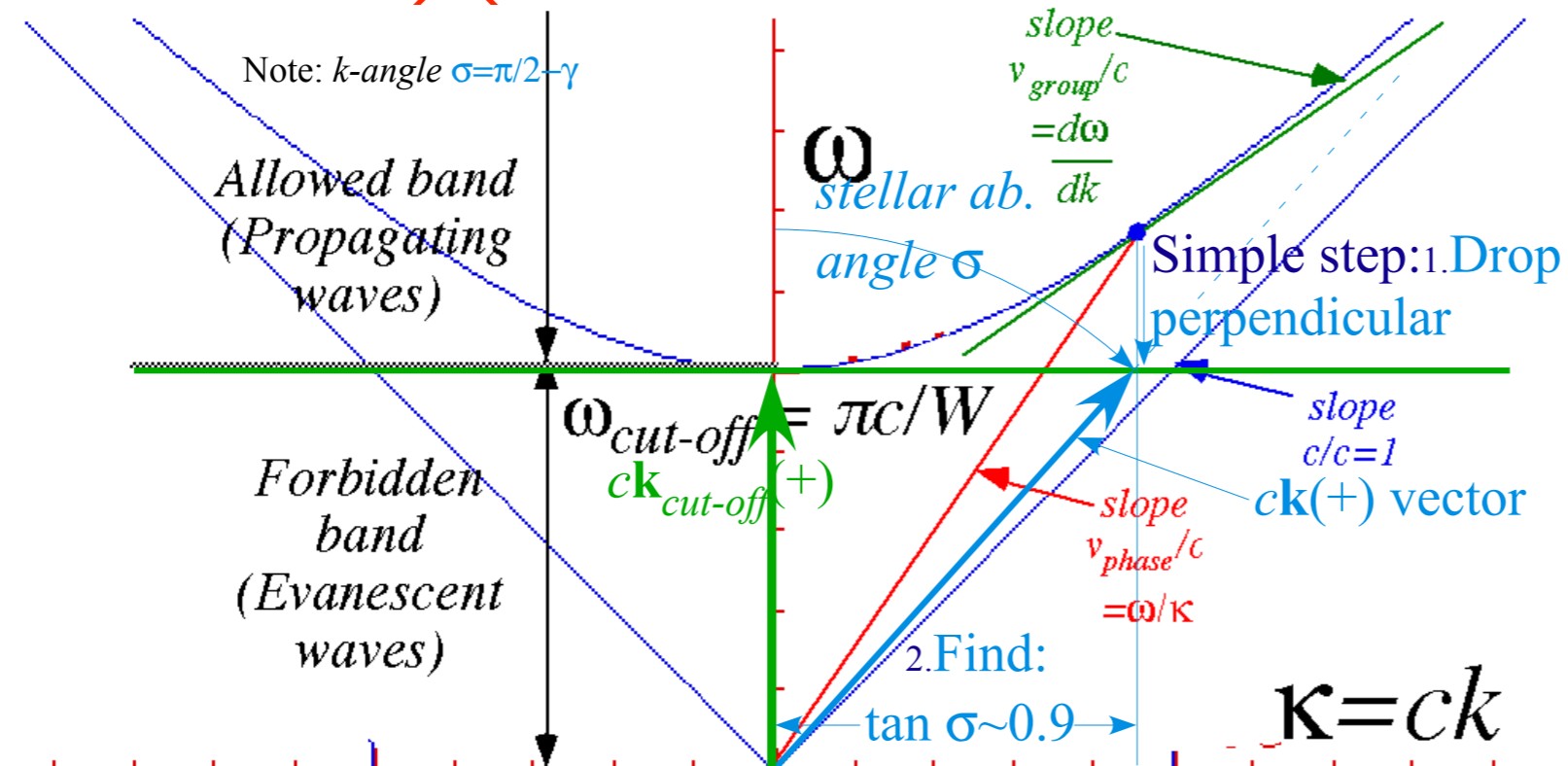


Fig. 6B.2 Dispersion function for a fundamental TE wave guide mode

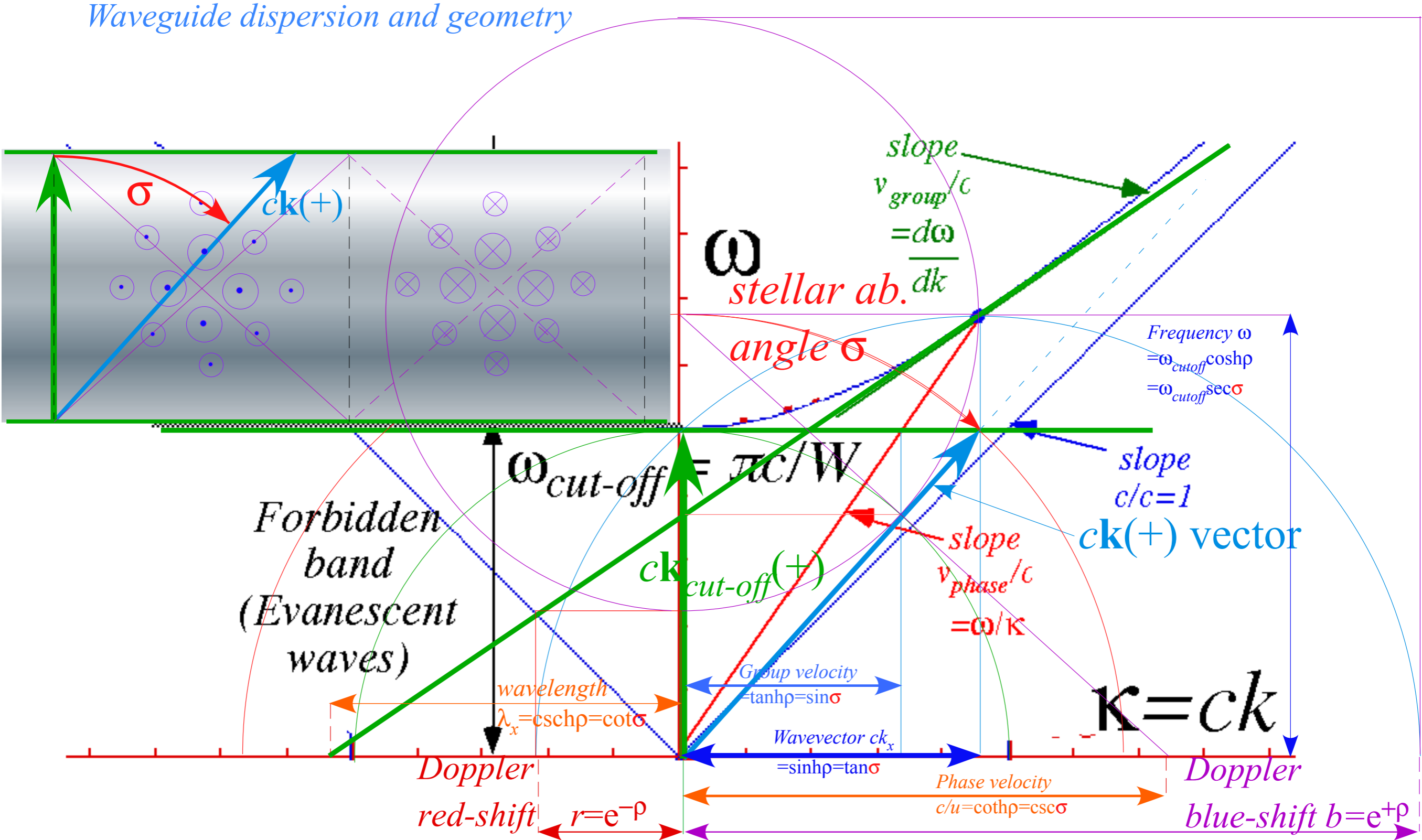


Fig. 6B.8 Thales geometry of cavity or waveguide mode

(Lecture 28 ends here)

Waveguide dispersion and geometry

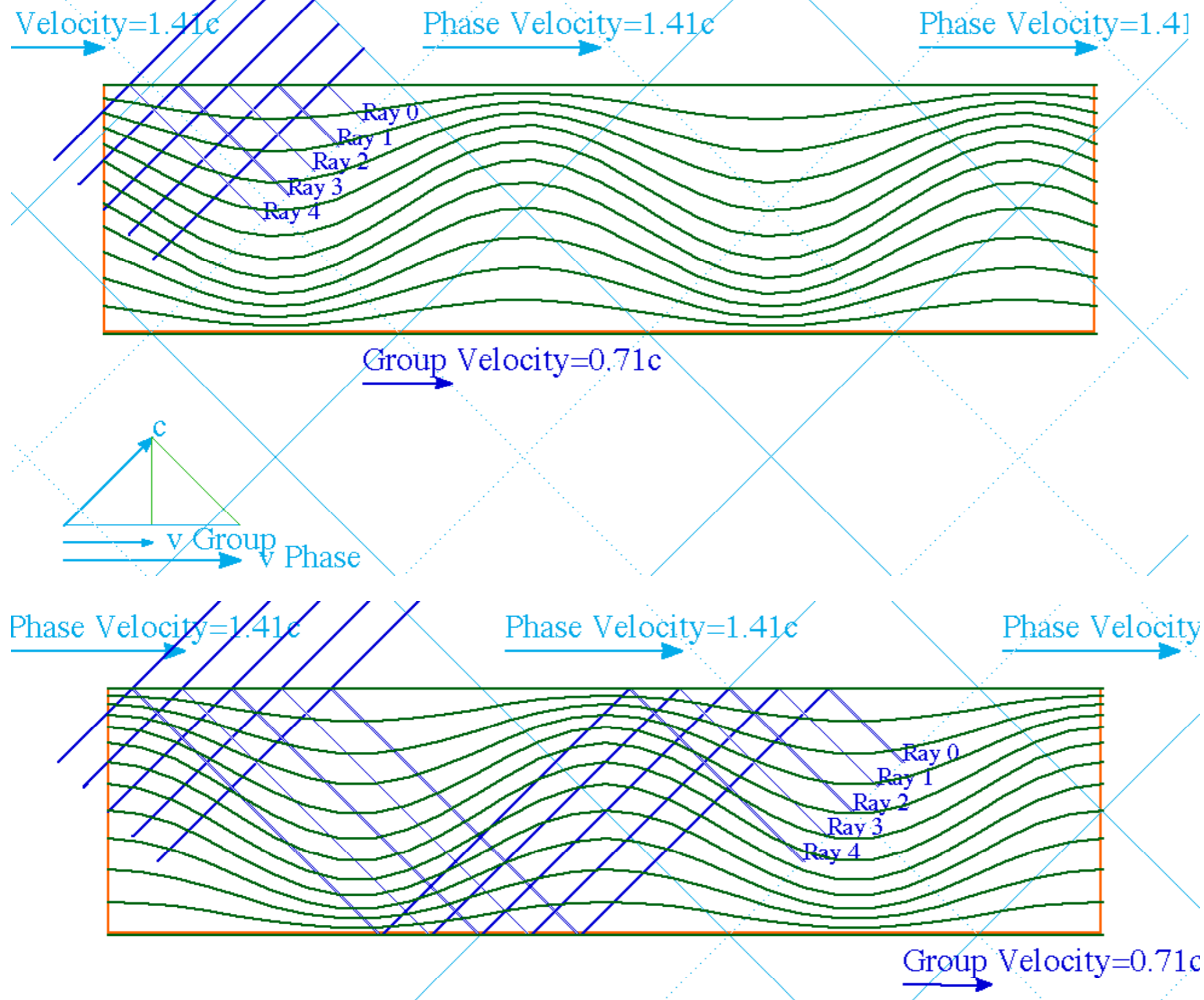


Fig. 6B.3 Right moving guide wave with $\gamma = 45^\circ$, $V_{\text{phase}} = \sqrt{2}c$, $V_{\text{group}} = c/\sqrt{2}$.

Waveguide dispersion and geometry

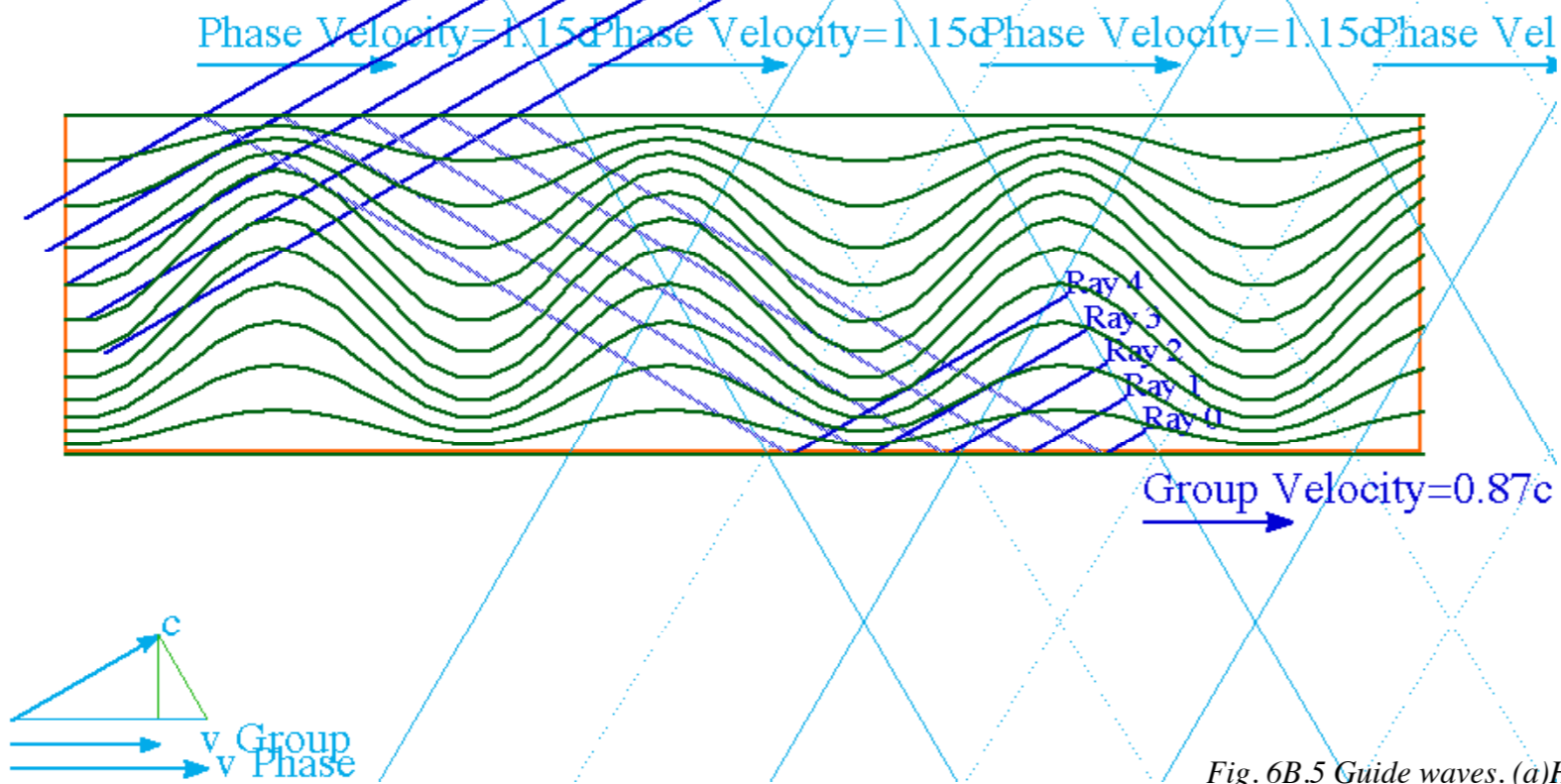
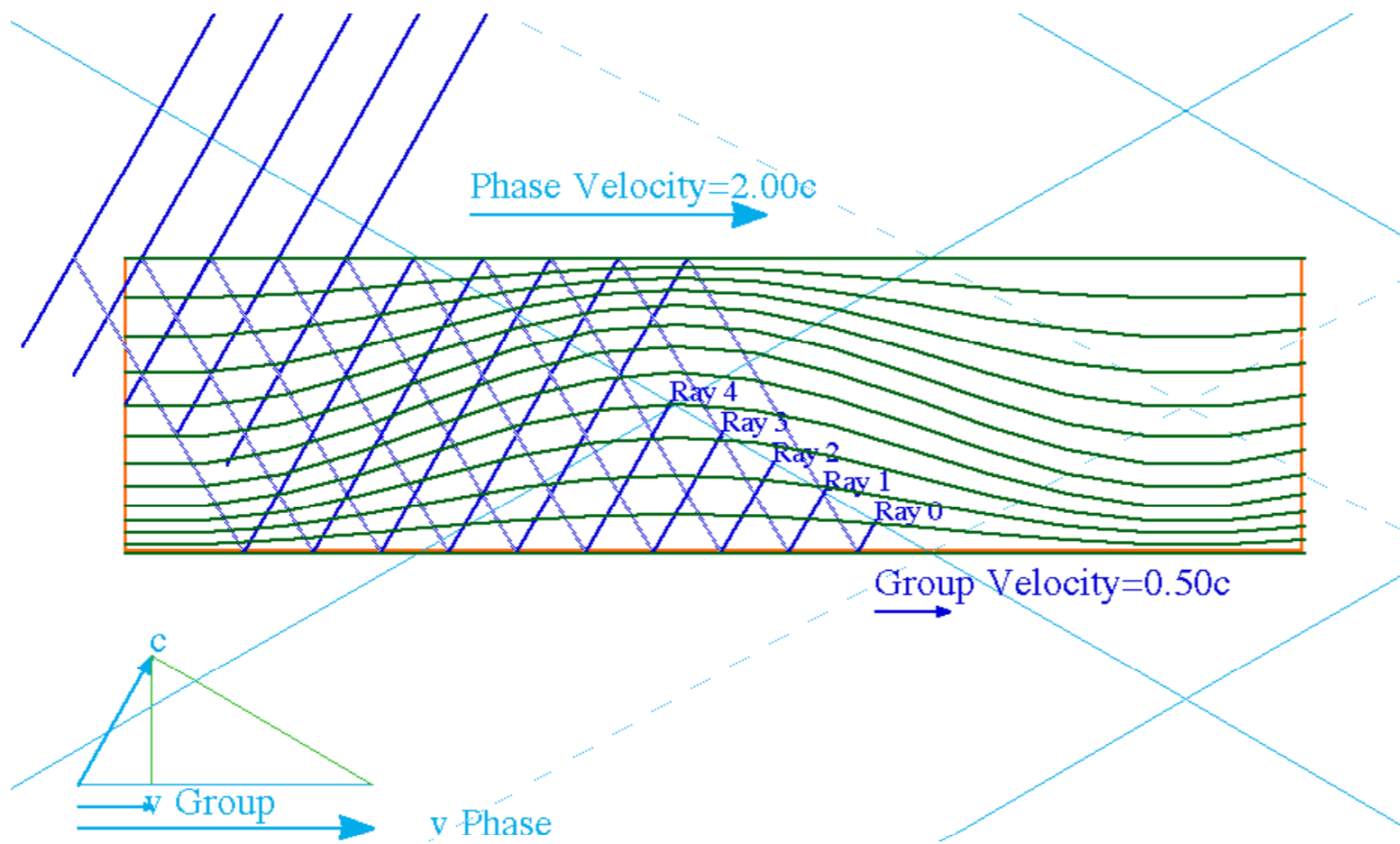


Fig. 6B.5 Guide waves. (a) Higher frequency case: $\gamma = 30^\circ$, $v_x(\text{phase}) = c\sqrt{3}/2c$, $v_x(\text{group}) = c2/\sqrt{3}$.
 (b) Lower frequency case: $\gamma = 60^\circ$, $v_x(\text{phase}) = 2c$, $v_x(\text{group}) =$



Waveguide dispersion and geometry

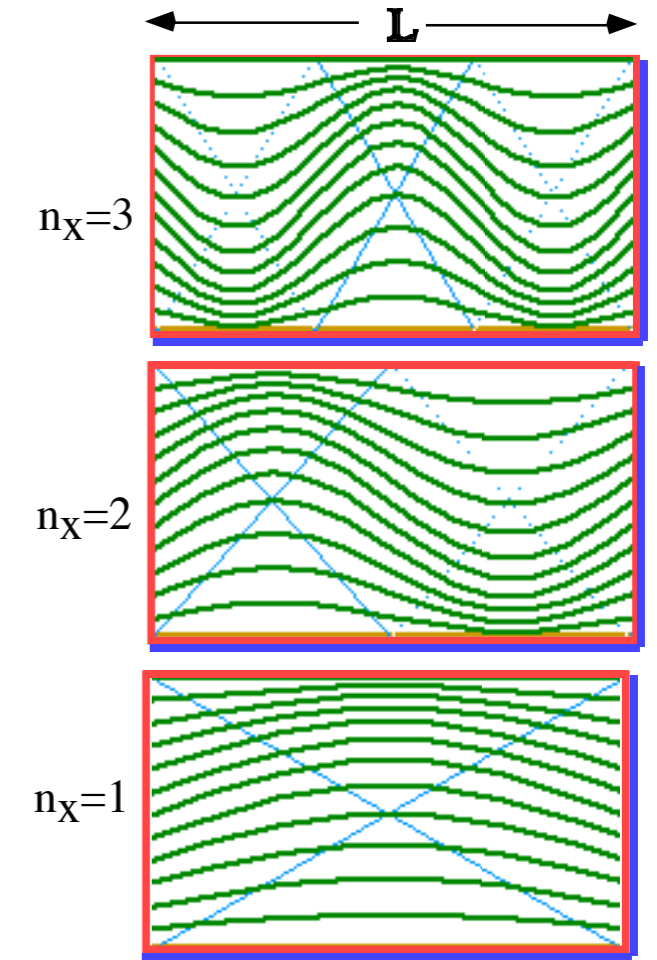
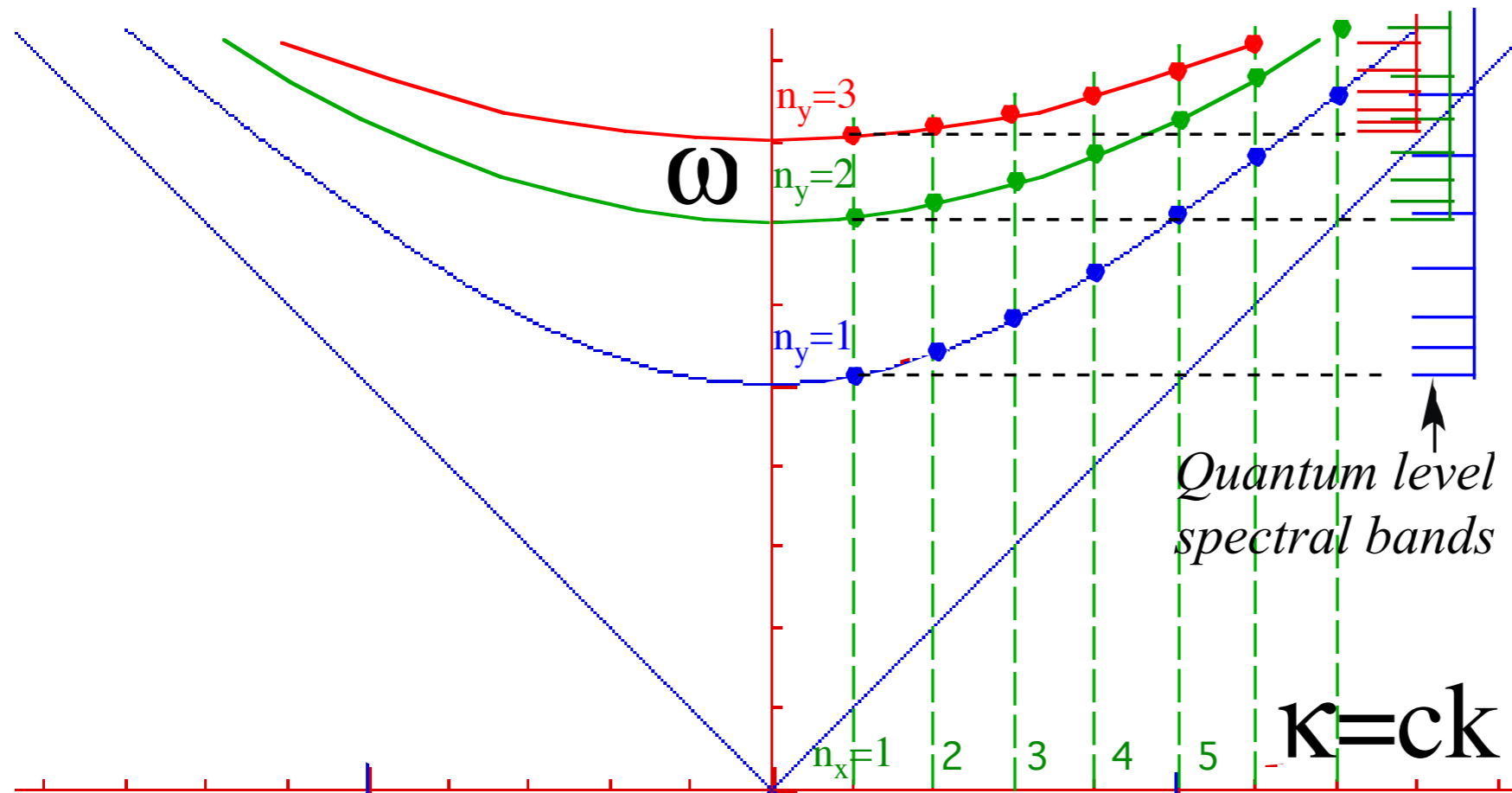


Fig. 6B.7 Cavity modes for three lowest quantum numbers

Fig. 6B.6 Cavity mode dispersion diagram showing overlapping and discrete ω and k values.

$$\Phi = -\mu\tau = \mathbf{k} \cdot \mathbf{r} - \omega t = \mathbf{k} \cdot \mathbf{r} - (\omega/c)(ct) = \mathbf{k}' \cdot \mathbf{r}' - (\omega'/c)(ct').$$

$$\Phi_{\leftarrow} = \mathbf{k}'_{\leftarrow} \cdot \mathbf{r}' - \omega'_{\leftarrow} t' = \mathbf{k}_{\leftarrow} \cdot \mathbf{r} - \omega_{\leftarrow} t = -\mathbf{k}_0 \cdot \mathbf{r}_0 - \omega_0 t_0$$

$$\Phi_{\rightarrow} = \mathbf{k}'_{\rightarrow} \cdot \mathbf{r}' - \omega'_{\rightarrow} t' = \mathbf{k}_{\rightarrow} \cdot \mathbf{r} - \omega_{\rightarrow} t = \mathbf{k}_0 \cdot \mathbf{r}_0 - \omega_0 t_0$$

$$c^2 \mathbf{k}'_{\leftarrow} \cdot \mathbf{k}'_{\leftarrow} - \omega'_{\leftarrow}{}^2 = c^2 \mathbf{k}_{\leftarrow} \cdot \mathbf{k}_{\leftarrow} - \omega_{\leftarrow}{}^2 = c^2 k_0^2 - \omega_0^2 = 0$$

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